

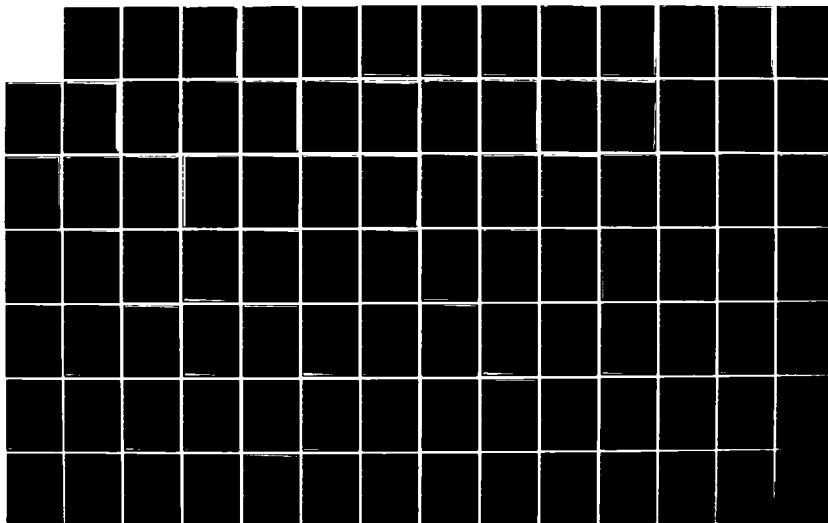
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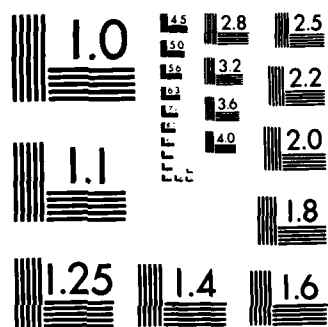
ESTIMATION OF F-15 PERCENTAGE MAINTENANCE MANPOWER
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ESTIMATION OF F-15 PEACETIME
MAINTENANCE MANPOWER REQUIREMENTS
USING THE LOGISTICS COMPOSITE MODEL

THESIS

GOR/SM/76D-5

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Wright

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Abstract

Estimates of the maintenance manpower requirements of a planned F-15 Tactical Fighter Training Wing operating in a peacetime environment were requested by Tactical Air Command. The Logistics Composite Model (LCOM), a computer simulation, was used in conjunction with the Moody Regression and Moody Manpower programs to estimate these requirements. A more efficient method, using statistical tests of hypothesis, was developed for determining steady state in the simulation model. Using this method, steady state conditions were found to exist, in most cases, at the end of the first simulated day. An estimate was made of the autocorrelation present in each set of simulation output data. Then, correcting for this autocorrelation, statistical confidence intervals were constructed for the manpower estimates. By simulating at various levels of flying activity and with various constraints on resource availability, manpower requirements were found to be relatively insensitive to these constraints at low sortie rates and more sensitive at higher sortie rates. The authors suggest that the construction of statistical confidence intervals and the methodology developed in this study for determining steady state should be given serious consideration in future LCOM manpower studies. *... and keywords include: no 1473*

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ESTIMATION OF F-15 PEACETIME
MAINTENANCE MANPOWER REQUIREMENTS
USING THE LOGISTICS COMPOSITE MODEL

THESIS

Presented to the Faculty of the School of Engineering
of the Air Force Institute of Technology
Air University

in Partial Fulfillment of the
Requirements for the Degree of
Master of Science

by

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Graduate Operations Research

December 1976

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Preface

This thesis represents the first detailed Logistics Composite Model (LCOM) analysis of United States Air Force (USAF) peacetime flying operations. In the study, we have attempted to shed light on the statistical and sensitivity inferences of the manpower estimation process. Hopefully, our efforts will allow the LCOM community to achieve greater statistical accuracy with LCOM.

We would like to thank our advisor, Colonel Ronald A. Luhks, and reader, Lieutenant Colonel Jon R. Hobbs, for their guidance during these past six months. We especially thank Lieutenant James R. Lowell for his ceaseless efforts and expert technical advice throughout our thesis effort. We also would like to thank Lieutenant Colonel Donald C. Tetmeyer, William D. Moody, and Wayne Jansen for their help with LCOM procedures. Finally, we would like to thank our wives, Mary and Bobbi, without whose help and encouragement this thesis would not have been possible.

George DeGiovanni

Donald M. Douglas

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Symbols and Abbreviations

AFB	Air Force Base
AFIT	Air Force Institute of Technology
AFM	Air Force Manual
AFSC	Air Force Specialty Code
AGE	Aerospace Ground Equipment
α	Type I Error
ASD	Aeronautical Systems Division
ASR	Accomplished Sortie Rate
ATS	Avionic Test Station
AUTO	Automatic
β	Type II Error
COM	Communications
E	Mutually Exclusive Probability
$E()$	Expected Value
ECM	Electronic Counter Measures
$E(U)$	Mean Value of Mann-Whitney
FC	Functional Code
FHPM	Flying Hours per Month
G	Nonmutually Exclusive Probability
H_a	Statistical Alternate Hypothesis
H_0	Statistical Null Hypothesis
INS	Inertial Navigation System
L	Interval or Lag Between Data Points
LCOM	Logistics Composite Model

Symbols and Abbreviations (continued)

LRU	Line Replaceable Unit
M	Direct Manning in Number of Men
MPIP	Maintenance Posture Improvement Program
M_s	Manpower Constraint in Number of Men
MSBMA	Mean Sorties Between Maintenance Action
N	Sample Size
NAV	Navigations
NRTS	Not Repairable This Station
P(R)	Probability That R Equals Some Integer Valued Number of Runs
PSR	Performance Summary Report
R	Number of Runs
ρ	Autocorrelation Coefficient
$\hat{\rho}$	Estimated Autocorrelation Coefficient
$\hat{\rho}(L)$	Estimated Autocorrelation Coefficient at Lag (L)
$\rho(L)$	Autocorrelation Coefficient at Lag (L)
RPV	Remotely Piloted Vehicle
σ^2	Population Variance
S_μ	Standard Deviation of the Mean
S_μ^2	Sample Variance of the Mean
TAC	Tactical Air Command
TFTW	Tactical Fighter Training Wing
U	Mann-Whitney Statistic
μ	Population Mean
U.E.	Unit Equipment

Symbols and Abbreviations (continued)

UHF	Ultra High Frequency
USAF	United States Air Force
V(U)	Variance of Mann-Whitney Statistic
W	Mann-Whitney Rank Value
WUC	Work Unit Code
\bar{X}	Sample Mean
X_t	Output Data Value at Time (t)
Z	Standard Normal Random Variable

I. INTRODUCTION

Estimation of the maintenance manpower necessary to support desired flying activities in various United States Air Force (USAF) organizations is a continuing problem. As new aircraft enter the inventory and as procedures change, there exists a recurring need for reliable estimates of the maintenance manpower necessary to support desired levels of flying activity efficiently. These estimates aid USAF managers in allocating maintenance manpower to new or existing flying units and insuring combat readiness.

Background

One method which has been used successfully to estimate these maintenance manpower requirements involves the use of the Logistics Composite Model (LCOM). The LCOM is a USAF computer simulation language designed to model USAF base level aircraft, maintenance, and support functions (Ref 33). Specifically, the model can be used to estimate maintenance manpower requirements for a USAF flying wing at specified levels of flying activity.

Two previous Air Force Institute of Technology (AFIT) theses have addressed LCOM estimation of maintenance manpower requirements: Green and Rumple constructed an LCOM simulation to evaluate the effects of alternative operational, maintenance, and supply policies on remotely piloted vehicle (RPV) maintenance manning (Ref 14:ii). Fritz and Yates used LCOM to simulate the interaction of the RPV, the launch aircraft, and the recovery helicopter (Ref 13:ii).

Tactical Air Command (TAC) used LCOM to estimate maintenance manpower requirements for their F-4, A-7, A-10, F-15, and F-16 aircraft

(Ref 23). However, TAC conducted the majority of these studies using a wartime operational environment and devoted little attention to a peacetime environment. Consequently, TAC suggested that AFIT students consider a peacetime LCOM study as a possible graduate thesis topic (Ref 29) and offered to make available an on-the-scene technical advisor to assist in making such a study meet TAC requirements.

Each of these previous LCOM studies simulated concurrent flying and maintenance activity. That is, aircraft maintenance was performed only on days of scheduled flying operations. In a wartime environment, this practice is acceptable since aircraft missions are scheduled seven days a week. However, this practice has one major drawback: if a high level of flying activity is scheduled, the aircraft maintenance organization may, at times, become overloaded with work. This causes a temporary decrease in flying activity until the maintenance organization clears out the backlogged work.

In a peacetime environment, flying operations are normally scheduled Monday through Friday. During high levels of flying activity, the maintenance organization continues to perform its functions on weekends in order to alleviate backlogged work. In this manner, the maintenance complex can usually keep stride with the weekly flying operations and the day to day level of flying activity remains fairly constant.

In this thesis, the authors use LCOM to model a peacetime flying environment. The model simulates a Monday through Friday flying schedule and a seven day maintenance work week.

Thesis Objectives

A need exists to expand F-15 LCOM estimation of maintenance manpower requirements to include the peacetime operational environment

(Ref 29). Furthermore, previous LCOM manpower studies have not emphasized statistical analysis of the output data.

In this thesis, the authors use LCOM to estimate the maintenance manpower requirements for an F-15 Tactical Fighter Training Wing (TFTW) with 72 unit equipment (U.E.) aircraft operating in a peacetime environment. In addition, they construct statistical confidence intervals around the resulting estimates of maintenance manpower requirements. Finally, the authors investigate the sensitivity of manpower requirements to variations in availability of aircraft parts and support equipment.

Thesis Scope

The LCOM peacetime environment is determined by TAC Training Syllabus Course Numbers F1500 B,I, and TX (Ref 30) requirements. These publications specify the flying training activity for F-15 pilot upgrade training which is the primary mission of a TFTW. The 58th TFTW located at Luke Air Force Base (AFB), Arizona currently uses these syllabi for all F-15 pilot upgrade training and is the base case for determining the peacetime F-15 LCOM operation and maintenance procedures.

Overview

The remainder of the thesis consists of five chapters. The LCOM chapter describes the Logistics Composite Model and Moody Manpower/Regression Programs. The Data Base chapter describes the maintenance and operations data base. The Methodology chapter lays the groundwork for this study's estimation of manpower requirements. The Analysis and Results chapter contains the manpower estimations and describes their sensitivity to variations in aircraft spare parts and support equipment.

Finally, the Conclusions and Recommendations chapter summarizes the thesis findings.

II. LCOM MANPOWER ESTIMATION

Rather than present a detailed description of the LCOM process, this chapter introduces simplified LCOM concepts which form a basis for the remainder of the thesis. Further detail concerning LCOM can be found in Drake (Ref 7 and 8) and Tetmeyer (Ref 33). The LCOM manpower estimation process uses the Logistics Composite Model, the Moody Regression Program, and the Moody Manpower Program (Ref 7, 8, and 33). The interaction of these computer programs produces a complete basic manning document for a USAF maintenance organization.

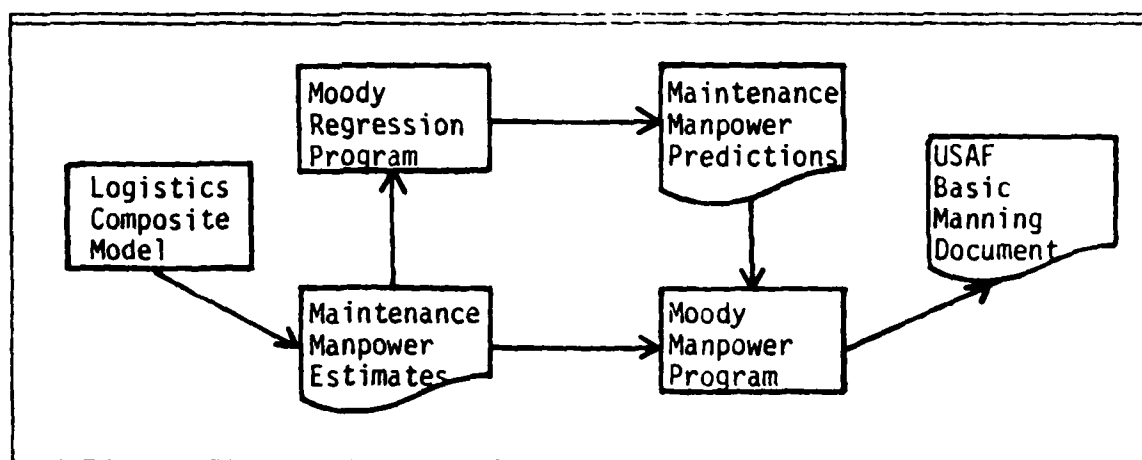


Figure 1. LCOM and Moody Regression/Manpower Program Relationship

Figure 1 depicts the interrelationship of LCOM and the Moody Regression/Manpower Programs. The Logistic Composite Model estimates maintenance manpower requirements for specified levels of flying activity. The Moody Regression Program uses these estimates and regression techniques to predict maintenance manpower requirements for a wide range of flying activity. The Moody Manpower Program uses the LCOM estimates and Regression predictions to produce a complete basic manning document for a USAF

maintenance organization. The following paragraphs describe each program in greater detail.

Logistics Composite Model

The LCOM uses three major computer programs to model aircraft flying operations, maintenance functions, and resource constraints. These programs are the preprocessor, main, and postprocessor programs (Ref 7: Chap. 1, p.2). The preprocessor program prepares aircraft operations and maintenance data for the main program. The main program simulates the interaction of aircraft operations, maintenance functions, and resource constraints and provides a statistical summary of the simulation results. The postprocessor program offers additional statistical output data.

Figure 2 illustrates the relationship between the three LCOM programs and the input/output data.

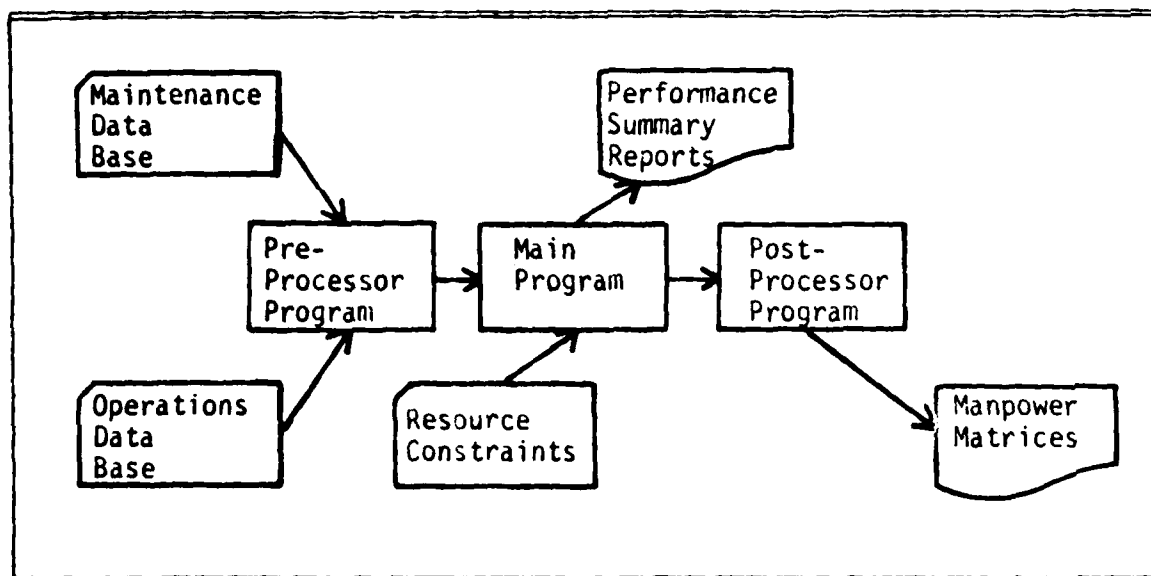


Figure 2. LCOM Program and Data Relationship

The operations and maintenance data bases represent the respective aircraft flying operations and maintenance characteristics. Resource

constraints consist of specified quantities of men by Air Force Specialty Code (AFSC), aircraft spare parts, and support equipment. The performance summary reports depict statistical summaries of the simulation results. Finally, the manpower matrices illustrate the daily distribution of manpower requirements (by AFSC).

Figure 3 shows how LCOM uses the flying operations schedule, maintenance functions, and resource constraints to simulate a sequence of maintenance activities. When the flying schedule calls for aircraft to start mission preparation, LCOM designates aircraft from the available aircraft pool for the mission. Each aircraft then processes through the preflight to postflight check blocks.

During this processing, LCOM uses men, spare parts, and support equipment as needed to perform maintenance functions. If all available manpower is already performing aircraft maintenance, LCOM delays the next mission until maintenance manpower is available. If the aircraft are ready for launch at their scheduled takeoff time, the missions fly for the specified mission length and then return for processing through the postflight check block. After postflight, LCOM places the aircraft in the available aircraft pool.

The LCOM also maintains a failure clock on each aircraft subsystem. These clocks use an exponential failure distribution to determine the number of sorties flown until corrective maintenance for their respective subsystems. Since LCOM does not simulate in-flight activity, it checks the failure clocks only during preflight and postflight. If the number of sorties flown equals a particular subsystem's clock value, LCOM lists that component as failed and ceases mission processing. The failed component then processes through the corrective maintenance block and uses

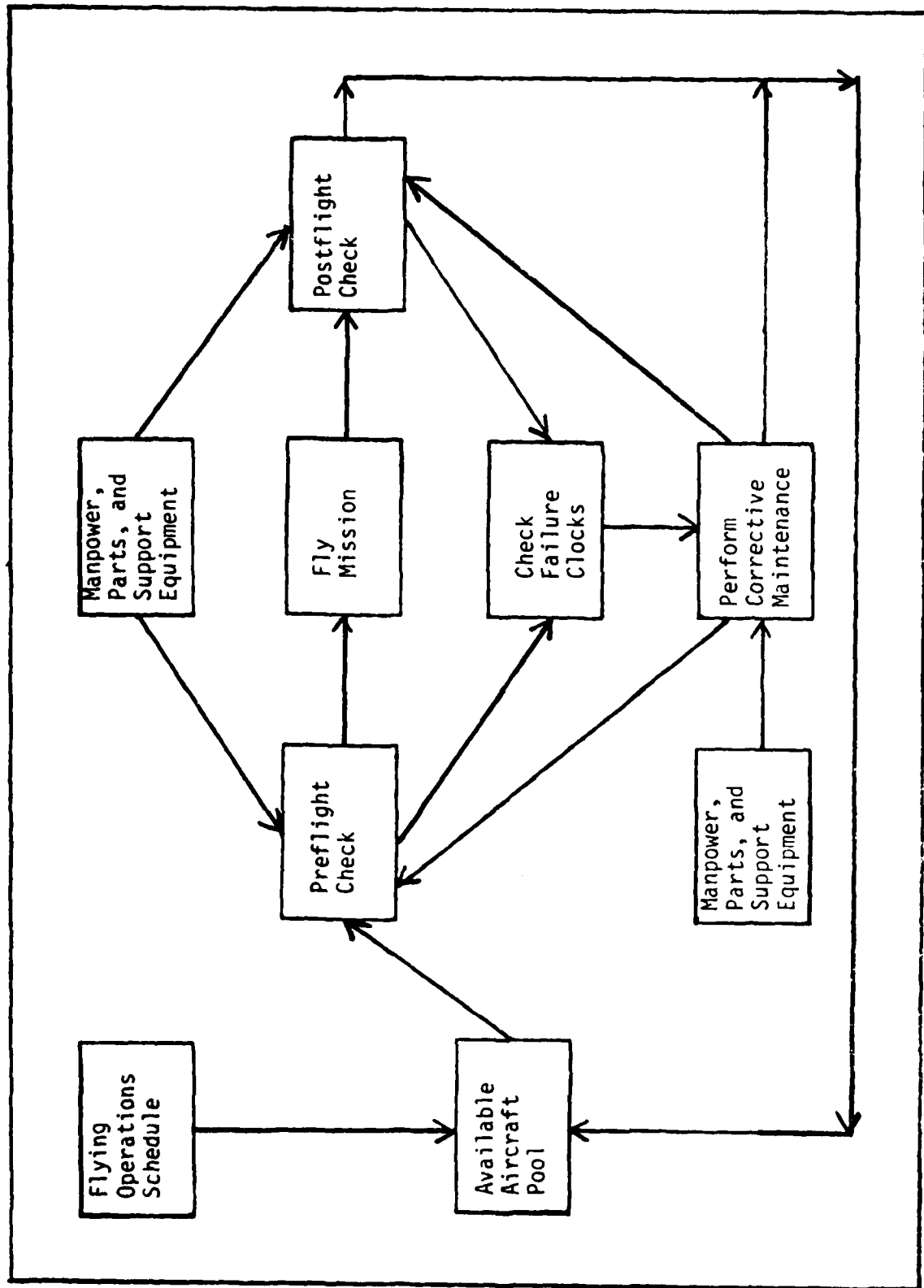


Figure 3. LCOM Simulation of Maintenance Activities

men, spare parts, and support equipment as necessary to perform the corrective maintenance. Upon completion of all corrective maintenance activity, LCOM allows the aircraft to continue with mission processing. However, if corrective maintenance delays an aircraft beyond its scheduled takeoff time, LCOM cancels the corresponding mission and returns the respective aircraft to the available aircraft pool.

The following description of LCOM's preprocessor, main, and post-processor programs more clearly defines the simulation process.

Preprocessor Program. The preprocessor program translates and organizes the maintenance and operations data bases for the main program. During data translation, the program scans the data base for inconsistencies and provides error diagnostic messages for data ambiguities (Ref 7: Chap. II, p.1). In some cases, the program makes computer logic assumptions when it finds minor data errors concerning user intentions and provides a message specifying the data ambiguity and corresponding program assumption. This feature prevents an unnecessary computer abort for minor data errors.

The LCOM maintenance data base consists of a weapon system's scheduled and unscheduled maintenance procedures, major components (parts), component failure frequencies, mean service and repair times, and resource (men, part, support equipment) requirements. This data represents the maintenance environment of an LCOM simulation (Ref 33:30).

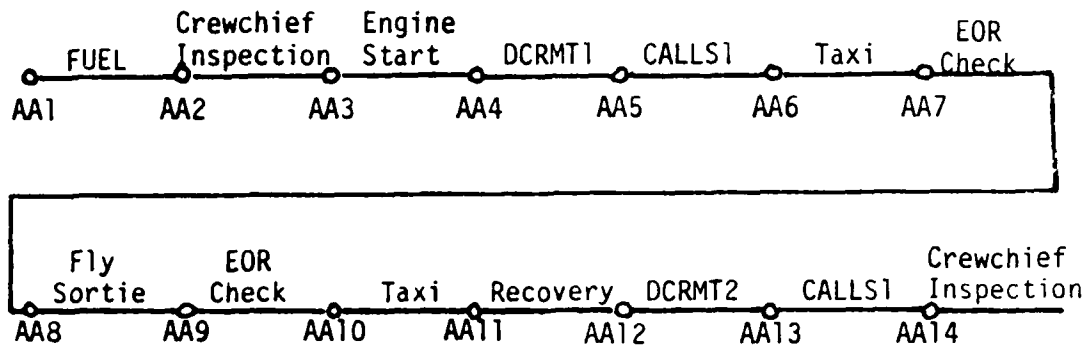
During data base formulation, the user graphically depicts the maintenance environment using LCOM networks (Ref 33:28). These networks define maintenance relationships within the data base. Figure 4 illustrates a simplified LCOM main network and corrective maintenance network for an aircraft mission.

In an LCOM network, tasks represent the scheduled and unscheduled maintenance procedures. These tasks are connected by network nodes (Ref 33:32). For example, nodes AA1/AA2, in Figure 4, define a FUEL task. The user also specifies the men (by Air Force Specialty Code), support equipment, and service or repair time necessary to complete a task. If a task resource is not available, LCOM will delay processing the aircraft mission beyond the guilty task until the constraining resource becomes available. For example, the FUEL task requires two men (AFSC 431X1), one fuel truck, and five minutes.

Every weapon system is composed of many major components or parts. The work unit code (WUC) manual for the particular weapon system numerically defines each of these parts. The LCOM maintains a failure clock for each major component in the maintenance network (Ref 33:36). For example, nodes M1/M2, in Figure 4, define the failure clock for the UHF radio (F63A00). The user assigns each failure clock a failure frequency parameter. He determines this parameter by analyzing failure rates of corresponding real life weapon system components. Mean sorties between maintenance action (MSBMA) is the most common parameter (Ref 33:56). In Figure 4, F63A00 has a MSBMA equal to 10 sorties. At the completion of an aircraft mission, the failure clock for each component in that mission main network advances one sortie.

The LCOM allows the user to specify the percent of time a major component fails before or after mission launch through the use of a clock decrement task (Ref 33:37). Nodes AA4/AA5, in Figure 4, define the clock decrement task prior to launch (DCRMT1) while nodes AA12/AA13 define the clock decrement task after launch (DCRMT2) for the UHF radio.

Main Mission Network:



UHF Radio Corrective Maintenance Network:

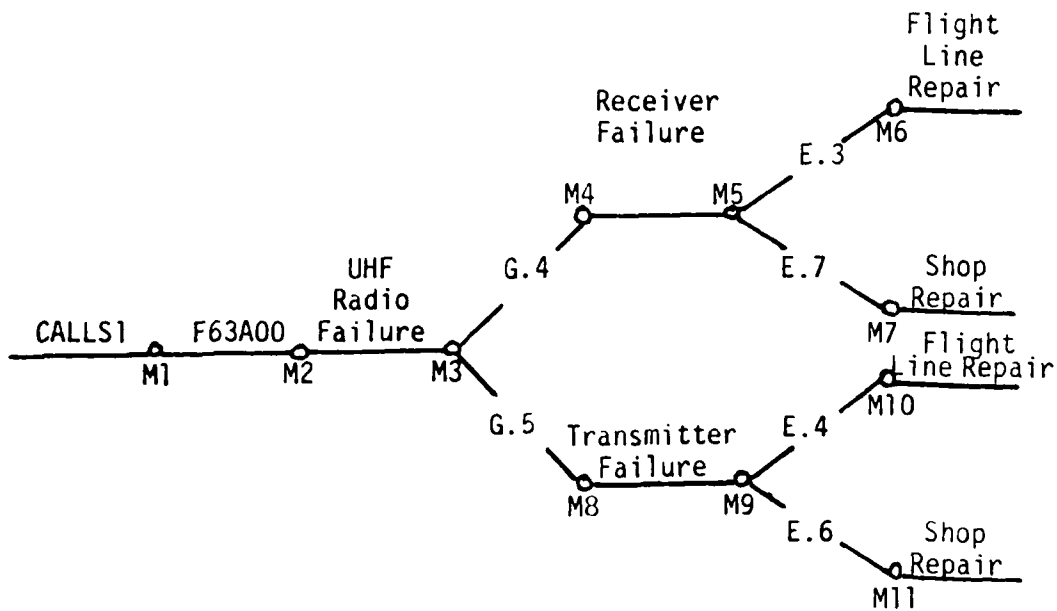


Figure 4. LCOM Maintenance Network

For example, DCRMT1 advances F63A00 three-fourth sortie and DCRMT2 advances F63A00 one-fourth sortie for a one sortie advance of the UHF radio clock by the completion of a processed aircraft mission.

Certain component failures in an LCOM network are not sortie related. In these cases, the failure clock uses a parameter other than MSBMA and the decrement task advances the failure clock by an adjusted amount independent of a sortie. One example is the gun on a tactical aircraft. Periodic gun maintenance is usually based on number of expended ammunition rounds. In this case, the failure clock uses rounds fired as a parameter and the decrement task advances the clock a certain number of rounds each mission sortie.

The LCOM interrogates a failure clock via a Call task (Ref 33:36). Nodes AA5/AA6 and AA13/AA14, in Figure 4, define the Call task (CALLS1) for the UHF radio failure clock (F63A00). Each time LCOM processes a mission through a Call task, the Model checks the corresponding clock to see if it has advanced to its MSBMA parameter. If the clock has advanced to this parameter, LCOM marks that component as failed and stops processing the aircraft mission. At the same time, the model begins processing the failed component through its respective corrective maintenance network. In Figure 4, LCOM processes the UHF radio through the UHF radio corrective maintenance network after F63A00 advances 10 sorties.

Within the corrective maintenance network, LCOM allows the user to specify which subsystem(s) caused the component failure and who fixes the subsystem(s). The model accomplishes this function with G and E probability distributions (Ref 33:62-65).

A G probability is a nonmutually exclusive probability that determines which subsystem(s) caused the component failure. Since the G

probability is nonmutually exclusive, either one or more than one subsystem can cause a component failure. In Figure 4, there exists a .4 probability that the receiver (nodes M4/M5) caused the radio failure, a .5 probability that the transmitter (nodes M8/M9) caused the radio failure, and an inferred .1 probability that both the receiver and transmitter caused the radio failure.

An E probability is a mutually exclusive probability that determines who fixes the broken subsystem(s). Since the E probability is mutually exclusive, Flight Line Repair (node M6) or Shop Repair (node M7), but not both, can fix the receiver. In Figure 4, there exists a .7 probability that Shop Repair fixes the receiver and a .3 probability that Flight Line Repair fixes the receiver.

If Shop Repair fixes the receiver, LCOM immediately generates a new part from supply stock and allows the aircraft mission to continue processing through its main network. After Shop Repair fixes the receiver, LCOM returns the repaired receiver to supply stock.

After constructing the LCOM networks, the user transcribes this information onto LCOM Extended Forms 11 (Ref 33:32-36). He then transfers this data to a computer card deck. This card deck is the completed maintenance data base. Figure A-1 in Appendix A contains a sample LCOM Extended Form 11.

The operations data base consists of the aircraft daily flying and maintenance schedules. These schedules form the operational scenario for an LCOM simulation.

The flying schedule contains the aircraft mission type, number of primary aircraft for each mission, mission takeoff time, mission cancel time, and flight duration. Missions with similar configurations, flight

time, preflight and postflight servicing, and maintenance crew requirements are grouped under a single LCOM mission type (Ref 33:16), since LCOM only simulates ground activity. As far as LCOM is concerned, flight time is that time which an aircraft is unavailable for maintenance.

The maintenance schedule specifies the number of spare aircraft per mission type, missions that fly more than once during the day (preflight to thru-flight), and number of phase inspections and aircraft washes.

The user designs the operational scenario for a specified level of flying activity. This level of activity is usually designated as aircraft sortie rate. Equation (1) defines sortie rate.

$$\text{sortie rate} = \frac{\text{sorties/day}}{\text{aircraft U.E. size}} \quad (1)$$

The U.E. size is the number of authorized aircraft assigned to a unit. Sorties per day may be either scheduled sorties or accomplished sorties. During the planning stage, the user bases the operational scenario on a scheduled aircraft sortie rate. After an LCOM simulation, the user computes an accomplished aircraft sortie rate.

The user records the completed operational scenario onto LCOM Forms 20 (Ref 33:17) prior to transferring the information to a computer card deck. The punched card deck represents the operational data base. Appendix B contains three operational scenarios based on scheduled sortie rates of .43, .74, and 1.0.

Main Program. The main program simulates maintenance and operations data base interaction. During this interaction, the main program uses available resources to prepare scheduled maintenance and flying

activity. The program processes each mission type through its respective main network while simulating all required maintenance tasks.

The preprocessor translated maintenance data base contains unconstrained maintenance manpower, aircraft spare parts, and support equipment. When these resources are left unconstrained, the main program has little difficulty complying with the operations data base's scheduled sortie rate provided sufficient time is allowed between scheduled missions for postflight and preflight maintenance tasks. If resources are constrained, the main program delays mission types, as necessary, when men, spare parts, and/or support equipment are unavailable. If a mission delay exceeds its cancel time, the program cancels the guilty mission. To constrain these resources, the user submits a series of computer cards to the main program prior to simulation. Each card specifies the number of maintenance men by AFSC and work shift, quantity of spare parts by WUC, and/or quantity of support equipment available during the LCOM simulation (Ref 33:123).

After simulation, the main program provides statistical data in the form of Performance Summary Report (PSR). These reports include the number of flying hours, number of sorties requested, number of sorties accomplished, manhours (by AFSC) used, manhour utilization rate (by AFSC), and parts (by WUC) consumed, generated, or backordered (Ref 7, Chap. II, p. 3). The user specifies the interval and number of PSR's desired prior to simulation. Figures C-1 and C-4 in Appendix C contain sample PSR's. The PSR's are used to evaluate the effects of main program simulation. For example, the user can compare scheduled and accomplished sortie rates to determine the effect of resource constraints on the simulation.

Postprocessor Program. The postprocessor program produces manpower matrices for each AFSC. These manpower matrices depict how an AFSC workload varies with the time of day (Ref 33:121). Figures C-2, C-3, C-5, and C-6 in Appendix C contain examples of on-equipment, off-equipment, and backorder matrix printouts for various AFSC's.

These on/off equipment printouts display the number of times during a simulated period that the number of people shown in the leftmost vertical axis are working at the time of day shown on the horizontal axis. This time is in half hour increments.

For instance, the on-equipment matrix for AFSC 326C2, in Appendix C, shows 11 cases in which two people are needed between 0330 and 0400.

The backorder matrices indicate which work shifts require additional personnel in order to increase sorties accomplished.

Moody Regression Program

The Moody Regression Program allows the user to estimate maintenance manning requirements for a wide range of flying activity (Ref 33:126). The user provides the program with three sets of LCOM estimated manning requirements (by AFSC) for an operational scenario based on three different scheduled sortie rates. The Moody Regression Program uses this data to compute first and second order regression equations for maintenance manning (by AFSC) as a function of flying hours per month. The program compares these ordered equations for goodness of fit and chooses that equation, for each AFSC, with the best fit. These equations can be used to graphically depict the information as shown in Figure 5.

Moody Manpower Program

The Moody Manpower Program produces a complete basic authorization document for a maintenance organization (Ref 33:129). The program

requires a unit's aircraft U.E. size and flying hours per month from the LCOM simulation, regression equations from the Moody Regression Program, the minimum crew size for each AFSC, and the organization's Major Command supervision and overhead requirements. The resultant document defines the organization structure by Air Force Functional Code (FC) and provides manning requirements by AFSC grade level, for each FC.

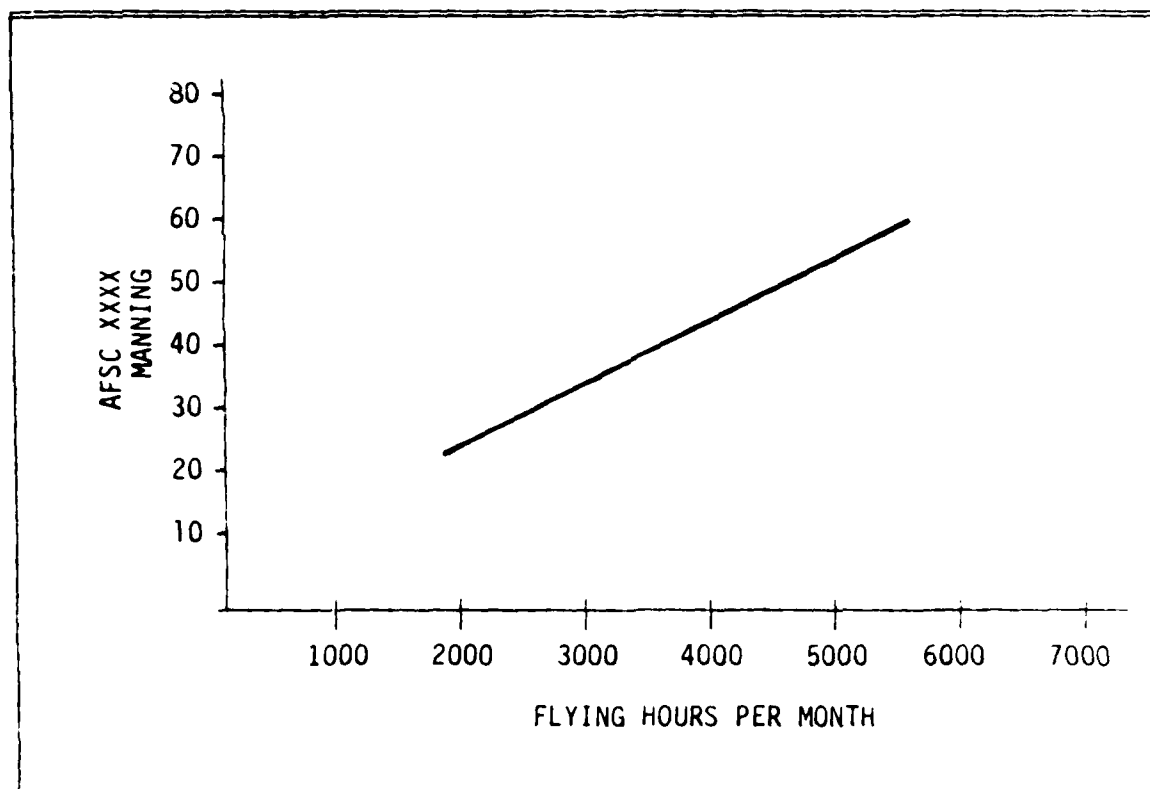


Figure 5. Moody Regression Graph

Summary

This chapter established the basic concepts used in the LCOM manpower estimation process. These concepts included the three LCOM programs, the Moody Regression Program, and the Moody Manpower Program. The next

chapter uses these concepts to describe the F-15 peacetime maintenance data base, operations data base, and resource constraints used in this study.

III. DATA BASE

This chapter contains a discussion of the maintenance and operations data bases and resource constraints used in the F-15 TFTW peacetime Logistics Composite Model. The description includes pertinent assumptions and the maintenance organization structure.

Maintenance Data Base

The maintenance data base is a modified version of maintenance data used in the ASD F-15/F-16 Wartime Study (Ref 5). Revisions include maintenance of TF-15 aircraft and simplified flight line maintenance networks with reduced armament and electronic counter measure requirements. Pages 107 through 149 in Appendix A contain a computer listing of the revised data base. The following paragraphs discuss these revisions in terms of the maintenance organization structure, scheduled and unscheduled maintenance procedures, repair/service times, weapon system components, and failure parameters.

Maintenance Organization Structure. Figure 6 illustrates the maintenance organization structure that supports the LCOM F-15 TFTW. This structure is similar to the 58th TFTW maintenance operation. The LCOM estimates those functional codes (FC's) designated by an "L" in Figure 6; the Moody Manpower Program produces a basic authorization document for all FC's depicted in the organization structure. Table I translates these FC's into AFSC's for LCOM estimated manpower and gives their work descriptions.

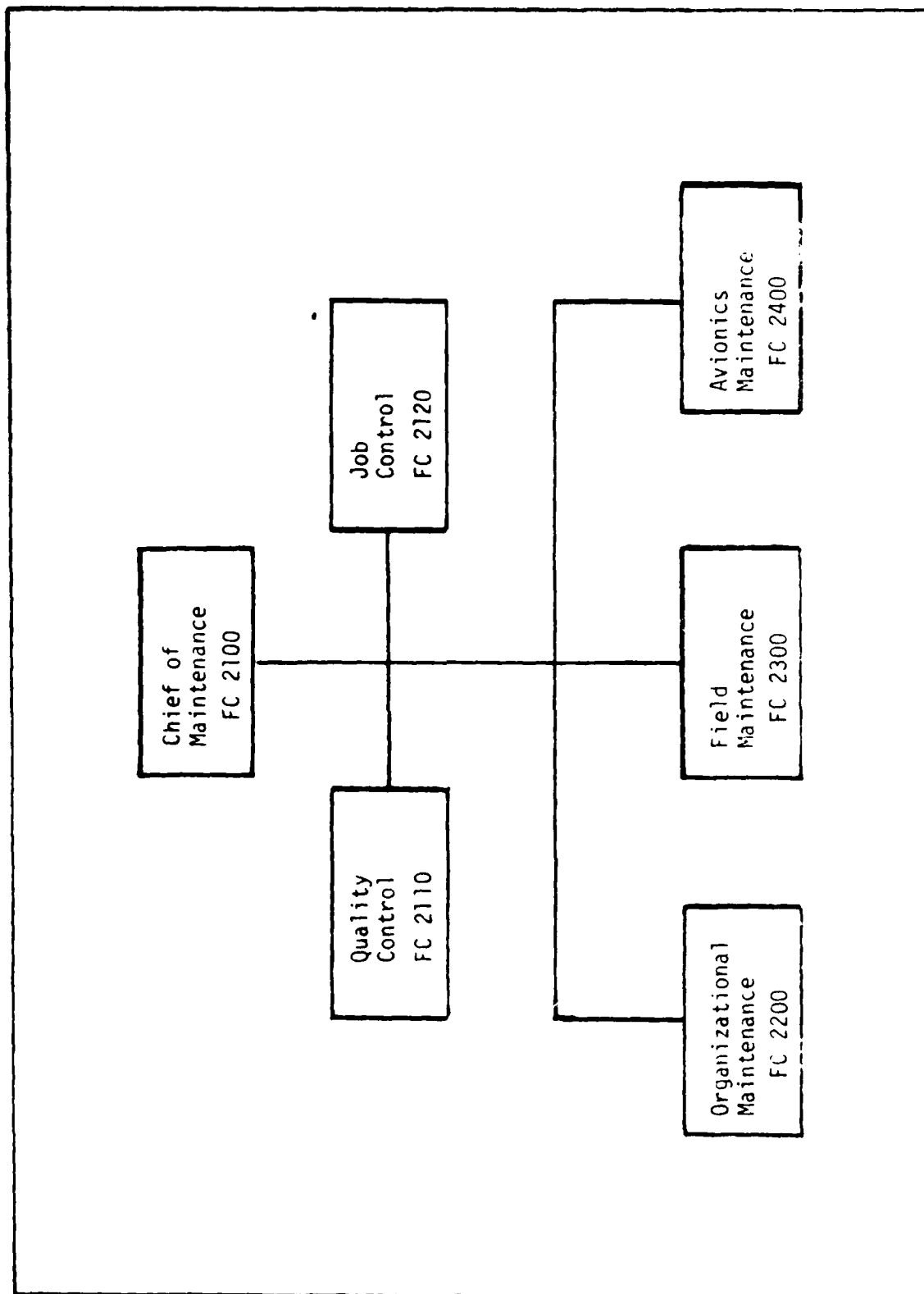


Figure 6. LCOM F-15 TFW Maintenance Organization Structure

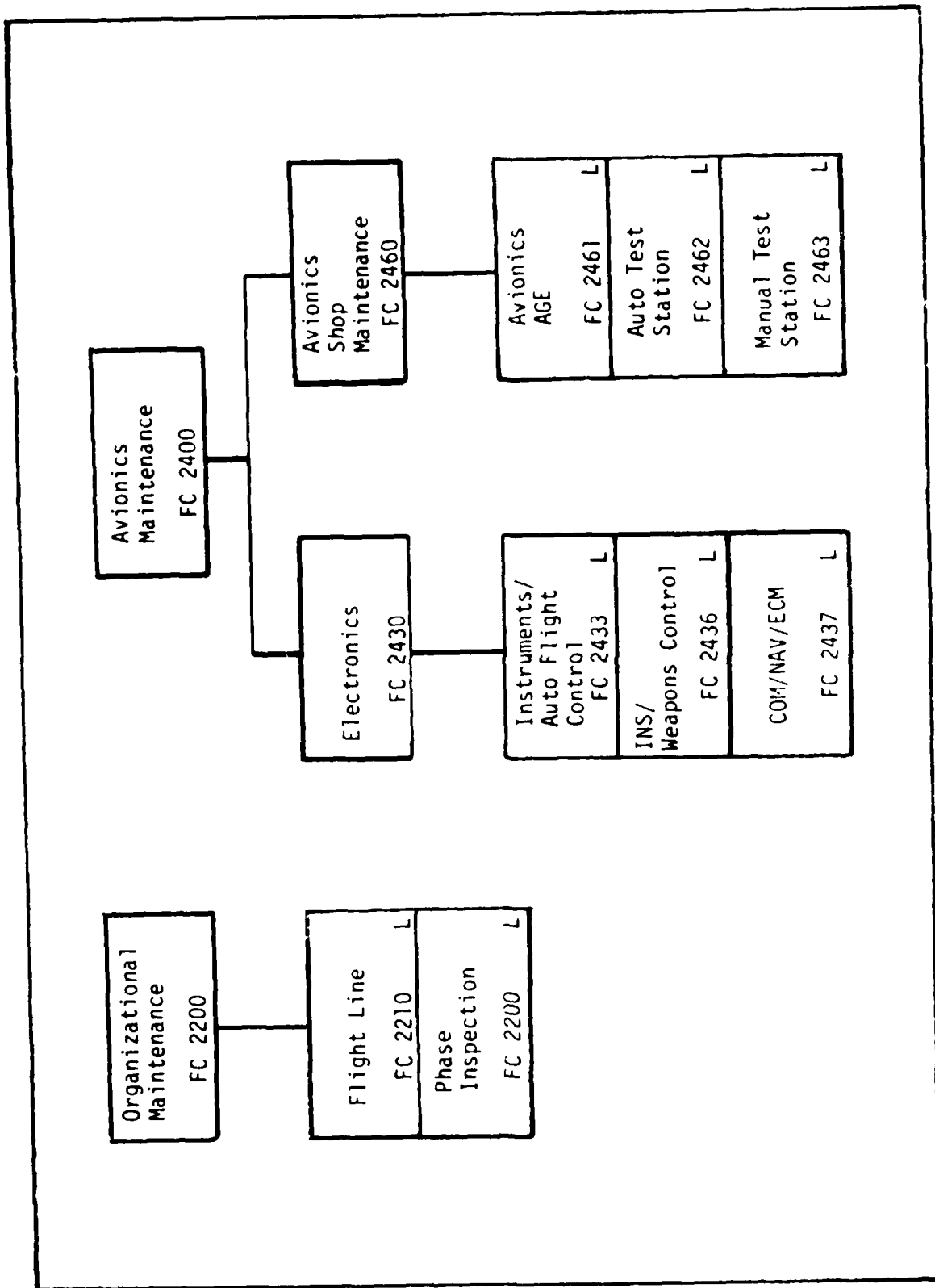


Figure 6. LCOM F-15 TFW Maintenance Organization Structure (Continued)

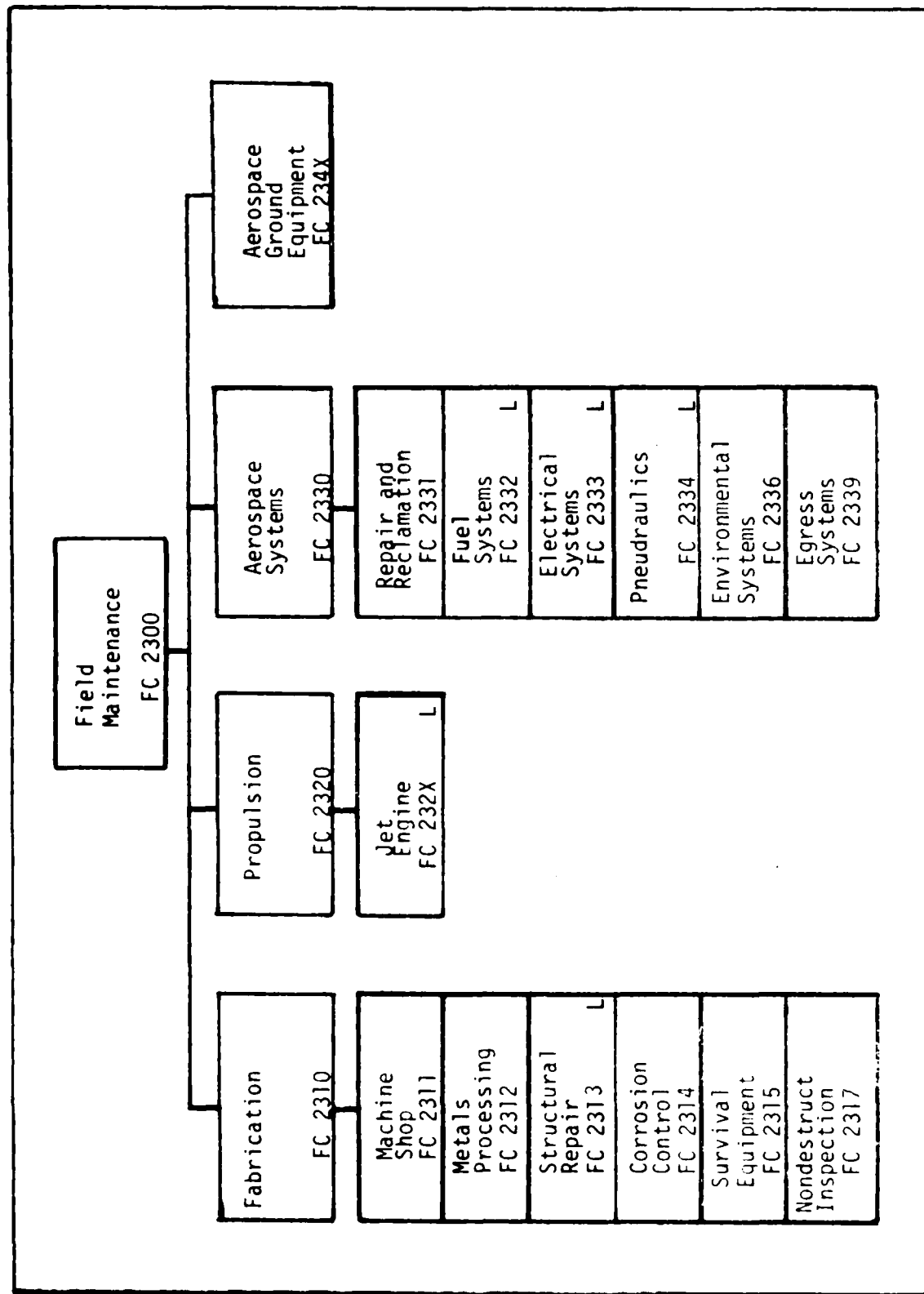


Figure 6. LCOM F-15 TFW Maintenance Organization Structure (Continued)

Table I
Function Code to AFSC Translation

FC	WORK DESCRIPTION	AFSC
22XX	Flight Line Crew Chief/ Phase Inspection	431X1
2313	Structural Repair	531X3
232X	Jet Engine Shop/Jet Engine Flight Line/Test Cell	426X2
2332	Fuel Systems	423X3
2333	Electrical Systems	423X0
2334	Pneudraulics	423X4
2336	Environmental Systems	423X1
2339	Egress Systems	423X2
2433	Automatic Flight Control/Instruments	326X2B
2436	Inertial Navigation System/Weapon Control	326X2A
2437	Communications/Navigations/Electronic Counter Measures	326X2C
2462	Automatic Test Station	326X1D
2463	Manual Test Station	326X1C

Scheduled and Unscheduled Maintenance. The wartime data base contained maintenance procedures peculiar to a wartime environment. With the technical assistance of the TAC advisor, the authors deleted wartime procedures and added, when necessary, the appropriate peacetime maintenance functions. The resulting LCOM networks represent those scheduled and unscheduled maintenance procedures performed by the 58th TFTW located at Luke AFB, Arizona. These modifications are based on an operational audit of maintenance procedures at Luke AFB (Ref 22) and TAC coordinated peacetime maintenance assumptions (Ref 16, 17, and 27). These assumptions consist of the following:

- The LCOM simulation models maintenance procedures of a 72 U.E. TFTW operating under TAC Training Syllabus course numbers F1500 B, I, and TX (Ref 30).
- Both F-15A and TF-15A aircraft maintenance are modeled.
- The 20mm gun is loaded with 1,000 rounds of ammunition and reloaded after two DART missions are flown. This is the only "live" ammunition used in the simulation.
- Ground aborted missions are not rescheduled since course flying requirements have a nine percent refly factor in establishing the Flying Training Program.
- The wing maintenance activity is organized per AFM 66-1 (Ref 4) and does not reflect Maintenance Posture Improvement Program (MPIP) reorganization.
- The F-15/TF-15 phase inspection procedures performed by the 58th TFTW at Luke AFB are used in scheduled maintenance networks.

- Not reparable this station (NRTS) components use a 15 day resupply time.
- On/off equipment maintenance is available 24 hours a day and seven days a week.
- On-equipment failure of a component is corrected by a remove and replace task when parts are available.
- Cannibalization is initiated when spare parts are constrained and a removed component cannot be repaired in time to accomplish a mission.
- End-of-runway teams are always available during scheduled flying periods.

Maintenance Repair/Service Time. Maintenance task repair and service times are based on interviews with the respective work center supervisors at Luke AFB, Arizona (Ref 1). The data base listing in Appendix A depicts these times and the respective maintenance tasks.

Weapon System Components. The authors used the F/TF-15A Series Work Unit Code (WUC) Manual to describe all weapon system components (parts) (Ref 36). A WUC is a five character code (11XXX-99XXX) that identifies each weapon system part. The maintenance data base describes each F-15 part at the two-four significant character WUC level. This description is equivalent to the line replaceable unit (LRU) level.

Component Failure Parameters. The maintenance data tape (Ref 1) for the 58th TFTW at Luke AFB, defines failure parameters for components in the corrective maintenance networks. This tape contains maintenance

data for the September 1975 - February 1976 time period and includes 2132 F/TF-15 flying sorties and 2867 flying hours.

Tetmeyer, Moody, and Nichols (Ref 32 and 33) describe the detailed procedures necessary to extract useful maintenance data from this tape. They also illustrate the method to compute the LCOM failure parameters (MSBMA and G/E Probabilities).

The data base listing in Appendix A illustrates the G and E probabilities for each corrective maintenance network. Appendix D contains each component failure clock, its corresponding MSBMA, and decrement value. The decrement values come from the F-15/F-16 Wartime Study (Ref 5).

Operations Data Base

The F-15 peacetime operations data base contains the flying training schedule and maintenance wash and phase inspection schedules and supports a 72 U.E. TFTW consisting of 48 single seat (F-15) and 24 tandem seat (TF-15) aircraft. The following TAC coordinated assumptions (Ref 16, 17, and 27) were used during construction of the operational scenarios contained in Appendix B.

- TAC Training Syllabus Course Numbers F1500 B, I, and TX define the unit's flying requirements (Ref 30).
- The modeled TFTW conducts only a conversion and air-to-air training program.
- Flying schedule sortie length and variance are derived from the training syllabi.

- Flying training is not scheduled on weekends or holidays.
- Night flying is scheduled as training requires.
- Aircraft scheduled for morning flights are thru-flighted as required to meet mission requirements.
- Aircraft missions delayed longer than two hours are cancelled.
- Only scheduled and spare mission aircraft are preflighted each day.
- Preflight inspections for each aircraft are completed at least two hours prior to scheduled takeoff.

Flying Schedule. This study uses three flying schedules to obtain scheduled sortie rates of .43, .74, and 1.0. Each schedule contains a 13 percent over schedule for maintenance cancellations and a nine percent over schedule for rescheduled training requirements. The .74 sortie rate establishes the base line flying schedule while the .43 and 1.0 sortie rates allow for decreased or increased demands in F-15 pilots. The schedules use a 65/35 ratio of F-15 versus TF-15 aircraft.

The flying schedules involved two basic mission types: Conversion and Air-Air missions. Conversion missions familiarize the pilot with basic F-15 aircraft performance characteristics. Air-Air missions contain tactical air intercept, combat, and gunnery maneuvers. All three flying schedules are based on a 30/70 ratio of Conversion versus Air-Air missions.

Maintenance Schedule. The maintenance schedule specifies the number of spare aircraft, thru-flights, washes, and phase inspections. In this study, the following conditions apply: 52 percent of scheduled aircraft are thru-flighted each day; airframes receive a wash every 75 hours and a phase inspection every 50 hours; spare aircraft are based on 10 percent of scheduled sorties.

Table II summarizes the daily maintenance requirements for the three operational scenarios used in this study.

Table II
Daily Maintenance Requirements

	Scheduled Sortie Rate		
	.43	.74	1.0
Scheduled Aircraft	21	35	47
Scheduled Sorties	31	53	72
Spare Aircraft	4	6	8
Hours per Airframe per Month	15	25	33

Resource Constraints

During the LCOM simulation, the authors constrain selected spare parts and support equipment to measure the effects on accomplished sortie rate and maintenance manpower. These constraints reflect the quantity of spare parts and support equipment available from base supply stock.

This study uses part supply levels found in the F-15/F-16 Wartime manpower Study (Ref 5:60-64). These quantities reflect the most current information on part levels. Appendix E lists the constrained spare parts by WUC and the corresponding supply quantity.

The only support equipment constrained during simulation are avionic test stations (ATS's). Maintenance personnel use these stations to troubleshoot aircraft avionic components. There are three ATS types in the maintenance data base. Appendix E lists each type, the job description, and constrained quantity.

Summary

The F-15 TFTW maintenance and operations data bases and resource constraints were discussed in this chapter. The discussion included pertinent TAC coordinated assumptions and the modeled maintenance organization structure. The next section contains the procedures used in this study to simulate peacetime maintenance and operations data base interaction and analyze the resultant manpower estimates.

IV METHODOLOGY

In this chapter, the authors discuss the concepts and procedures employed in the development of manning estimates using the LCOM model, and the analyses of results obtained. Specifically, this includes an explanation of the sequence of simulation runs performed, the use of the resulting data to compute manpower estimates, and the procedures employed to validate the model. Further, the authors discuss the statistical concepts used to define steady state for the model and to construct confidence intervals for the manpower estimates. Finally, the use of the Moody Regression and Moody Manpower Programs to investigate the sensitivity of manning requirements to parts/ATS constraints is explained.

Sequence of Simulation Runs

In order to estimate manpower requirements for a particular combination of sortie rate and parts/ATS constraints, a series of LCOM runs was performed as shown in Figure 7. To investigate the sensitivity of manpower requirements to various constraints and sortie rates, this sequence was repeated for each of the nine possible combinations of the three sortie rates (.43, .74, and 1.0) and the three levels of resource constraints (unconstrained parts/ATS, constrained parts and unconstrained ATS, and constrained parts/ATS).

Determination of Manpower Requirements

The LCOM determined manpower requirements are based on the total manhours used for each AFSC. After running the model with unconstrained manpower as indicated in Figure 7, it is necessary to constrain the number of men available in the model in order to estimate the actual number

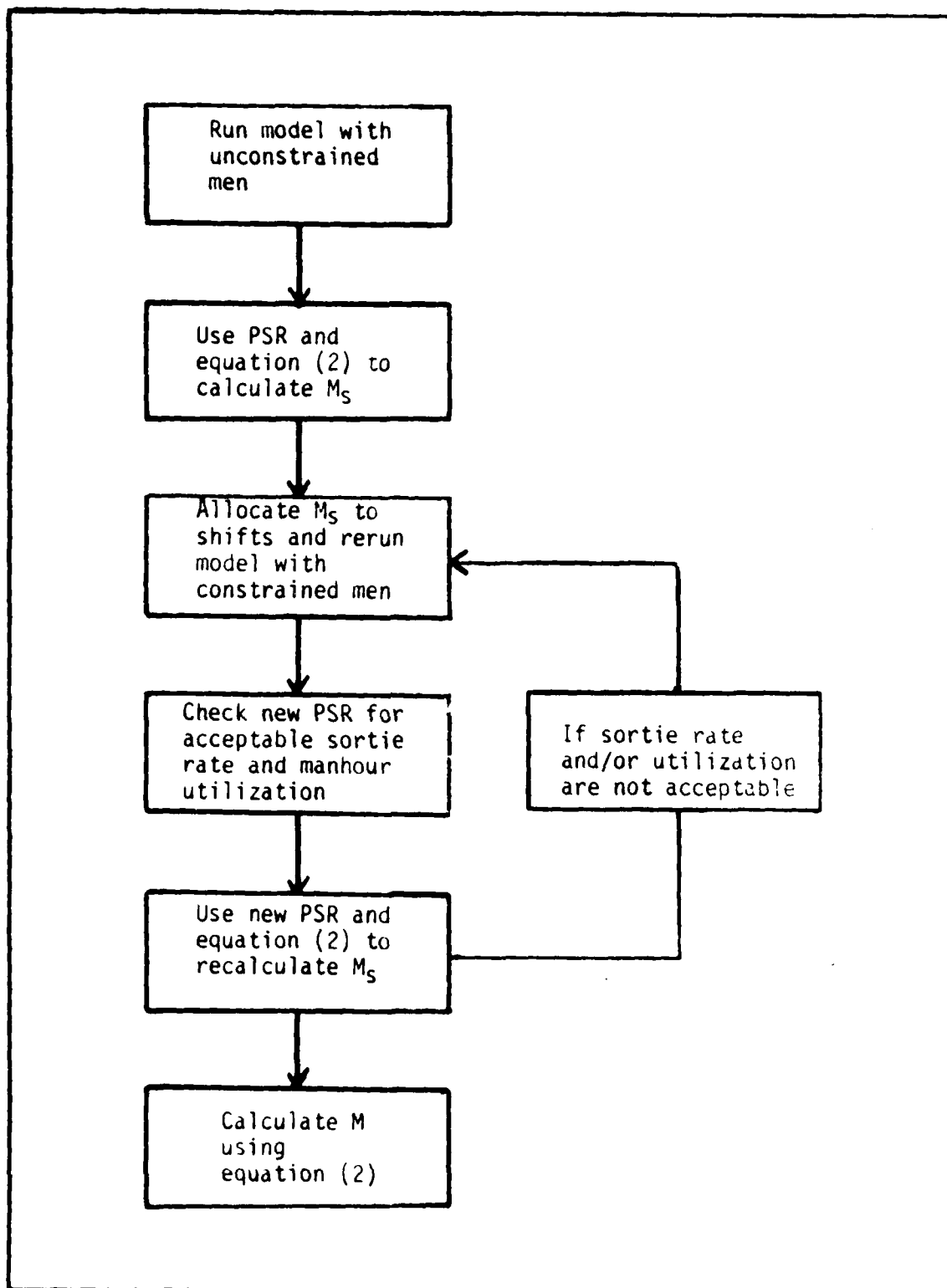


Figure 7. Sequence of Simulation Runs

of men required to support a specified sortie rate. Equation (2) is used to convert each AFSC's total manhours used into these manning constraints.

$$M_s = \frac{\text{Total Manhours Used}}{\left(\frac{\text{Utilization}}{\text{Factor}}\right) \left(\frac{\text{Number}}{\text{of Days}}\right) \left(\frac{\text{Shift}}{\text{Length}}\right)} \quad (2)$$

In this equation, the total manhours used for each AFSC are obtained from the simulation's performance summary report (PSR). The utilization factor is the fraction of manhours available for direct work; in this case, the Air Force standard is 0.6 (Ref 2: Chap. 6, p. 29). Shift length is eight hours. The M_s then becomes the average number of men available each day for each AFSC (Ref 33:121). This number is allocated over the three shifts using the manpower matrices as a guide. The resulting shift manning is incorporated into the model as a constraint on manpower. Certain AFSC's require a minimum crew size to perform their maintenance functions. In cases where M_s is less than the daily minimum crew manning, the minimum crew size is assigned to each shift as the constraint on manpower. The simulation is then rerun to determine what change has occurred in the accomplished sortie rate, as defined by equation (1), and to ensure that the resulting manhour utilization rate has not exceeded 0.6. If the accomplished sortie rate and/or manhour utilization rate are unacceptable, the process is repeated as indicated in Figure 7.

The M_s resulting from this procedure, however, is not the actual number of men required because it does not consider the fact that each individual normally works five days a week, takes leave, and may otherwise be legitimately absent from work. The Air Force standard for actual hours worked per man per month is 144 hours (Ref 3:7-8). Equation (3) is used to convert M_s into Direct Manning (M). Direct Manning

represents the final manpower estimate for each AFSC in the LCOM simulation.

$$M = \frac{M_s(\text{work days/month})(\text{shift length})}{144 \text{ hours/man/month}} \quad (3)$$

Model Validation

If a simulation model is to be of use in making predictions, then those predictions must be shown to be correct or at least as good as predictions made using some other method. Emshoff and Sisson state that the best possible evidence of such validity is that the model has made satisfactory predictions in the past (Ref 10:204). In this respect, the general LCOM model has been proven valid by numerous previous studies of other weapons systems and scenarios. There was, however, no direct counterpart to the present study, and for this reason a further investigation of validity was conducted.

A first-time model, such as the one under consideration here, cannot be validated completely until the system it represents actually comes into existence. Until that time, the model's validity can only be evaluated in terms of credibility. Emshoff and Sisson suggest that such validation consists of debugging the program, checking that key subsystem models predict their part of the world well (using historical data), and that knowledgeable individuals agree to the reasonableness of the model structure and output or face validity (Ref 10:206). The authors used these criteria in conjunction with a more detailed debugging procedure, recommended by Tetmeyer, to develop the following validation procedure (Ref 33:111, 113).

A 28 day unconstrained simulation was run, with complete diagnostics, and the output checked to insure that: all phases and scheduled

inspections were accomplished as well as a high percentage of scheduled sorties, there were no unsatisfied demands for personnel, the number of repairable generations for each item in the shop repair summary was equal to the number of units demanded for the same item in the supply summary, and, finally, there were no cannibalizations, supply backorders or unsatisfied demands (anything else would have indicated a data error) (Ref 33:113).

Next, a 28 day simulation was run with each of the three flying schedules. In each case, all unscheduled maintenance was removed from the model, thus preventing any equipment or aircraft breakdowns. In each case, all scheduled sorties were in fact accomplished, demonstrating the feasibility of the flying scenarios.

Finally, the MSBMA assigned from historical data to each failure clock was compared to the MSBMA actually observed during a 28 day run of the simulation. In most cases the variation was low; those few cases that did show a large variation in MSBMA had a large assigned MSBMA (the failure should seldom occur). In these cases small numerical differences between observed and predicted numbers of failures resulted in large changes in MSBMA. In light of the negative exponential distribution of failures in the model, and the short time span of the test simulation, variations of this sort were not unexpected. Further, as noted by Emshoff and Sisson, variations in the distribution of infrequent events are not normally significant when the model is intended to predict the behavior of some larger system (Ref 10:205). Consequently, the authors saw no reason to doubt the validity of the model based on its stochastic behavior.

The model was also tested for face validity. Emshoff and Sisson state that face validity exists when knowledgeable individuals agree to the reasonableness of the model structure and output (Ref 10:204). In this case, Lowell and Moody examined the model and output and found it, in their opinion, to be reasonable (Ref 24).

Steady State

In any simulation model, one of the important questions the researcher must answer is, "How long must the simulation be run until the parameters of interest (in this study sortie rate and manhours used) reach typical values for the system, or steady state?" Steady state, of course, is a relative condition depending on the specific parameters being considered and the degree of accuracy desired from the simulation. For instance, the time series output of a hypothetical simulation might appear like that shown in Figure 8.

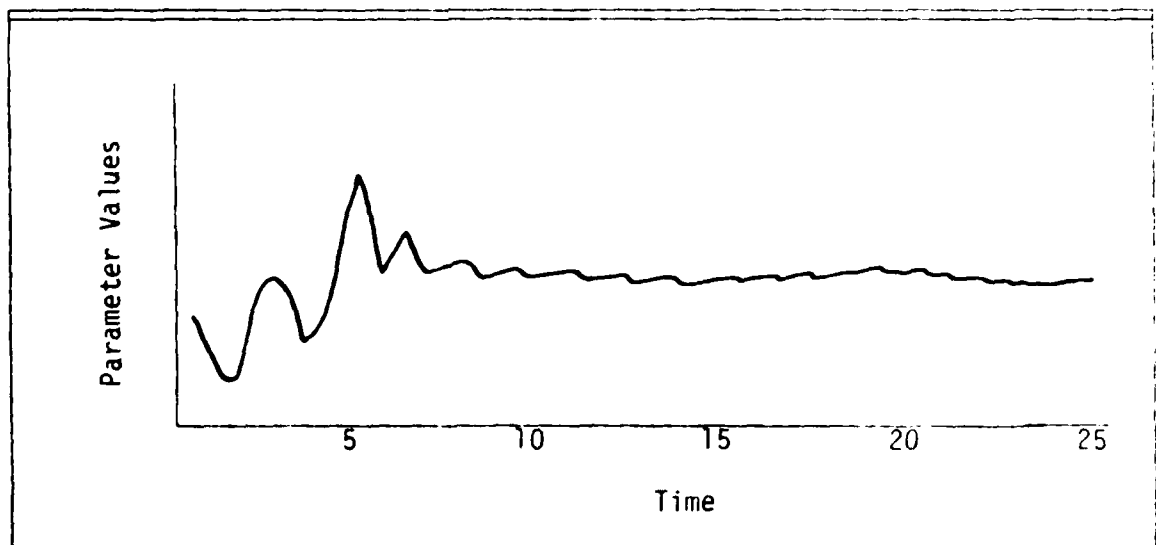


Figure 8. Type I Hypothetical Steady State Behavior

In this particular hypothetical example, after time period 10 the value of the output parameter is reasonably constant. In such a situation, the user could confidently accept data after that time as being typical of the system being modeled.

Unfortunately, many simulations do not exhibit the type of behavior just described. The values of output parameters may increase or decrease over time, indicating that they do not have a typical value within the system being simulated. Another possibility is that the value of the output may fluctuate considerably from one observation to the next; yet, in viewing such data over time the individual data points show no particular trends; but instead, appear to be randomly distributed about some central value. Such a case is illustrated in Figure 9. A closer

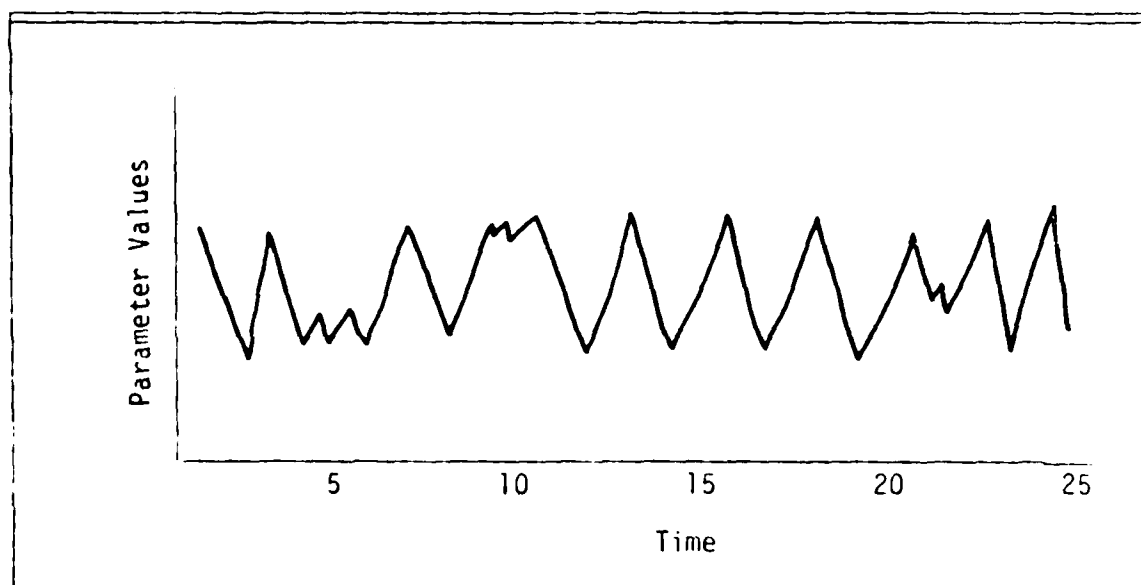


Figure 9. Type II Hypothetical Steady State Behavior

examination of the two situations depicted in Figures 8 and 9 reveals that the graph in Figure 8 after period 10, is actually similar to the situation depicted in Figure 9 except for the amplitude of the fluctuations.

Some Criteria for Steady State

Tetmeyer states in his discussion of the LCOM model that steady state is reached when successive thirty day manhour totals for each AFSC do not vary more than five percent (Ref 33:112). Of course, this is just another way of stating how much error the user is willing to accept.

As noted by Conway:

"...it is also important to recognize that equilibrium is a limiting condition which may be approached but never actually attained. This means that there is no single point in the execution of a simulation experiment beyond which the system is in equilibrium. The difference between the temporal and limiting distribution presumably decreases with time and one seeks a point beyond which he is willing to neglect the error that is made by considering the system to be in equilibrium" (Ref 6).

Emshoff and Sisson mention a procedure similar to that used by Tetmeyer, but go on to discuss other methods which the authors of this study felt were possibly more appropriate (Ref 10:192). Specifically, they state that steady state has been reached when successive output values vary randomly about some typical value; or similarly, when successive observations of the time series output are statistically indistinguishable (Ref 10:190).

The procedure described by Tetmeyer for identifying steady state is in common usage among LCOM practitioners. In an effort to reduce computer running time, the authors elected to investigate the feasibility of determining steady state by comparing probability distributions as suggested by Emshoff and Sisson.

Student's T Test. Student's T test is a very powerful statistical test which can be used to compare the means of two populations. Such

a test might be used to indicate if the mean values of the simulation output over two adjacent time periods were statistically indistinguishable (Ref 25:343). This, in turn, would indicate that the simulation was in steady state. To use the test, however, one must be able to assume that the sample data is from at least a near normal or mound shaped probability distribution (Ref 12:169).

Since, in this study, the flying scenario calls for no flying on Saturday or Sunday, the distribution of manhours used per day is bimodal in nature. Consequently, the authors felt an assumption of normality was not warranted.

It is important to point out, nevertheless, that in other experiments having a continuous flying schedule, such as a wartime model or a peacetime scenario as described by Tetmeyer, the T test might be an appropriate tool (Ref 33:126-127). For a further discussion of the T test, the reader is referred to any elementary text on parametric statistics.

The Man-Whitney U Test. The Mann-Whitney U test is a nonparametric statistical test designed to indicate if two independent random samples can reasonably be expected to have come from different probability distributions, or if the two are stochastically indistinguishable. The primary advantage of this test is its applicability regardless of the probability distribution of the data to be tested (Ref 28:116).

Use of the U Test in Determining Steady State. In light of the distribution-free nature of the Mann-Whitney test, it was tested as an indicator of steady state on the simulation runs which had constrained

manpower. The first fourteen days of simulation output were compared to the remainder of the data from each run; a two week segment was chosen to provide sufficient data for meaningful application of the test, and also to avoid bias which would have resulted if proportionately more Saturdays and Sundays (nonflying days) were included in one of the samples than in the other. The null hypothesis (H_0) was defined to be:

H_0 : The two samples come from the same probability distribution.

If H_0 is not rejected, then the test is not able to distinguish between the two samples, and the authors considered steady state to exist at the beginning of the first sample. The alternate hypothesis (H_a) was defined as:

H_a : The two samples do not come from the same probability distribution.

When H_a is accepted, a significant difference exists between the two samples indicating that steady state has not been reached at the beginning of the first sample. In such instances, the authors threw out data from the first part of the time series (in increments of seven days) until the test indicated that steady state had been reached.

Application of the Mann-Whitney test involves first, computing the value of the U statistic for the two samples being compared. U is defined as the smaller of

$$U = N_1 N_2 \frac{N_1 + 1}{2} - W_1 \quad (4)$$

or
$$U = N_1 N_2 \frac{N_2(N_2 + 1)}{2} W_2 \quad (5)$$

where N_1 and N_2 are the sample sizes of the two time periods being compared, and W_1 and W_2 are obtained by ranking the $(N_1 + N_2)$ data points from one to $(N_1 + N_2)$ and summing these ranks for each group. Then, for N_1 and N_2 greater than ten.

$$Z = \frac{U - E(U)}{V(U)} \quad (6)$$

where Z is the standard normal random variable, $E(U)$ is the expected value of the U statistic

$$E(U) = \frac{N_1 N_2}{2} \quad (7)$$

and $V(U)$ is the variance of the U statistic.

$$V(U) = \frac{N_1 N_2 (N_1 + N_2 + 1)}{12} \quad (8)$$

(Ref 25:535-538).

If H_0 is true then

$$P(|Z| \leq Z_{\alpha/2}) = \alpha \quad (9)$$

where $\alpha/2$ is equal to the integral of the standard normal distribution function from $Z_{\alpha/2}$ to ∞ (Ref 25:276). It can then be said with probability $(1 - \alpha)$ that if the absolute value of Z , from equation (6), is greater than or equal to $Z_{\alpha/2}$ then H_0 is not true.

The Runs Test. The Runs Test was used to identify steady state for simulation runs with unconstrained manpower. This test is a distribution

free statistical test which can be used to guard against nonrandomness in a time series. Such nonrandomness may be related to either trends or periodicities in the data. As noted earlier in this paper, one criteria for steady state in a simulation is randomness of the output data about some central value. To use the test, the time series is separated into observations above the mean and observations below the mean. A run is defined as a series of observations all above or all below the mean. Given the number of data points above the mean (N_1), the number of points below the mean (N_2), and the number of runs (R); it is possible to compute the probability of observing R or fewer runs assuming the sequence is in fact random. These probabilities are commonly tabled and can be used in testing various hypotheses (Ref 25:542-547).

Application of Runs Test in Determining Steady State. In using the Runs Test as an indicator of steady state, the authors aggregated the daily manhour totals by weeks. Too few runs, in a statistical sense, were taken as an indication of a trend in the data. The null and alternate hypotheses were defined as follows:

H_0 : There is no trend in the data--steady state is assumed to exist over the entire time series.

H_a : There is a trend in the data--steady state does not exist over the entire time series.

The rejection region was defined to be R such that $P(R) \leq .1$. As with the Mann-Whitney Test, if H_0 was rejected with the original data set, the data set was reduced until H_0 was no longer rejected.

Type I and Type II Errors. When using any statistical test of hypothesis, the experimenter must be aware of the errors that can be made in accepting or rejecting H_0 . The probability of rejecting H_0 when H_0 is in fact true is termed the Type I error and is denoted by α . The authors chose the relatively large value of 0.1 for α , so that the Type II error (β), defined as the probability of accepting H_0 when actually H_a is true, would not be too large. Mendenhall and Shaeffer note that as α increases β will decrease (Ref 25:330). Even so, with the relatively small sample sizes involved in this study, β will be quite large. The authors, however, do not consider this serious since the intention is not to "prove" that the null hypothesis is true, but only to detect any significant deviation from that hypothesis.

Confidence Intervals

The mean value for manhours used, from the simulation output, is merely an estimate of the true mean for the system being modeled. The accuracy of this estimate is affected by the analyst's decision on when steady state exists, the number of data points used in the estimate (N), and the variance of the sample data (S^2). When considering the accuracy of such an estimate, the analyst is led to the consideration of statistical confidence intervals.

If the sample data is composed of independent random variables, the sample mean will possess a normal distribution for sample sizes larger than thirty (Ref 25:270). Then, the statistic

$$Z = \frac{(\bar{X} - \mu)}{\sqrt{S^2/n}} \quad (10)$$

where μ = the population mean

\bar{X} = the sample mean

S_{μ}^2 = the sample variance of the mean ($\frac{S^2}{N}$)

S_{μ} = the sample standard deviation of the mean ($\sqrt{S_{\mu}^2}$)

As before, Z is the standard normal random variable with zero mean and variance equal to one. From equation (10) can be constructed the following confidence interval:

$$\mu = \bar{X} \pm Z_{\alpha/2} S_{\mu} \quad (11)$$

where $Z_{\alpha/2}$ is such that the integral of the standard normal density function from $Z_{\alpha/2}$ to ∞ is equal to $\alpha/2$. It can now be stated with probability $(1 - \alpha)$ that the true population mean is contained in the interval given in equation (11) (Ref 25:276-277).

Autocorrelation. In many simulation models, the parameter values for separate observations are not independent; they are affected in some way by those values that precede them. For instance, in the LCOM model used in this study, high work loads on one day may carry over into the next day causing the man hours used on both days to be high. This type of dependence is called autocorrelation. The autocorrelation coefficient, ρ , where ρ is as defined by equation (12), is a measure of this dependency. If man hours used on any particular day is assumed to be normally distributed, ρ equal zero implies independence, and ρ equal one implies complete dependence (Ref 35:70).

$$\rho(L) = \frac{E([X_t - \bar{X}][X_{t+L} - \bar{X}])}{\sigma^2} \quad (12)$$

where E = expected value

x_t = output value at time (t)

\bar{x} = sample mean

σ^2 = population variance

L = interval or lag between data points to be tested for dependence (Ref 10:194-199).

Given only a sample from the entire population, it is not possible to compute $\rho(L)$. However, an estimate, $\hat{\rho}(L)$ is available as follows.

$$\hat{\rho}(L) = \frac{\sum_{t=1}^{N-L} (x_t - \bar{x})(x_{t+L} - \bar{x})}{\sum_{t=1}^N (x_t - \bar{x})^2} \quad (13)$$

Correcting for Autocorrelation. The procedure developed previously for constructing confidence intervals employed an estimate of the variance of the mean, S_{μ}^2 , based on an assumption of independence. If autocorrelation is present, then, the procedure for constructing confidence intervals must be modified.

One possibility is to examine $\hat{\rho}(L)$. If a value of (L) can be found such that $\hat{\rho}(L) = 0$, then the data can be combined or blocked into intervals of length (L). The mean values for these blocks will now be independent, and as such can be used to construct confidence intervals as previously described (Ref 10:199-200).

A second possibility is to correct the variance of the mean (S_{μ}^2) by using the following relationship.

$$\text{Corrected } S_{\mu}^2 = S_{\mu}^2 \left[1 + 2 \sum_{L=1}^{N-1} \left(1 - \frac{L}{N} \right) \hat{\rho}(L) \right] \quad (14)$$

The reader should note that when $\hat{\rho}(L) = 0$, the above reduces to the form used in the previous development of confidence intervals (Ref 10:199).

Sensitivity Analysis

The Moody Regression Program, discussed in Chapter II, was used to develop a relationship between direct manning requirements and flying hours per month. A regression equation was developed for each AFSC with constrained manpower only, constrained manpower and parts, and constrained manpower, parts and ATS. These equations were then plotted to demonstrate the sensitivity of manning requirements, for each AFSC, to various sortie rates and parts/ATS constraints.

The primary inputs to the Regression Program consist of flying hours per month and final direct manning (M from equation (3)) rounded in accordance with AFM 25-5 (Ref 2:7-8). Manning for some LCOM shred-outs is combined under a single AFSC as shown in Appendix A. Further, direct manning for some LCOM shred-outs cannot be properly estimated using LCOM hours from the PSR. For instance, the End of Runway Crew requires very few LCOM hours in the model. In reality though, the positions must be manned during all flying operations. Direct manning in this case was estimated using the following relationship (Ref 3:2-4).

$$M = \frac{(\text{crew size})(\text{work days/wk})(\text{hrs/day})(4.348 \text{ wks/mo})}{144 \text{ hours/man/month}} \quad (15)$$

Direct manning for these LCOM shred-outs was combined under the appropriate AFSC in the Regression Program.

Developing a Manning Document

The final step in obtaining an estimate of required manpower involves the use of the Moody Manpower Program. Up until this point only

direct manning has been discussed; that is, no consideration has been given to the fact that there is a requirement for supervisory and other overhead personnel in the maintenance organization being modeled. The Moody Manpower Program converts the results of the final simulation runs and the Moody Regression runs into a completed manning document, which reflects the total maintenance manning, by AFSC and work center, necessary to support the organization under study at a specified sortie rate and with specified constraints on parts/ATS.

In this study the authors used the Moody Manpower Program to develop estimates for total required manning, and also to demonstrate the sensitivity of total manning to parts/ATS constraints.

Summary

This chapter has included a discussion of the concepts and procedures used by the authors in accomplishing the objectives of this study. In the next chapter the authors demonstrate the methodology discussed here and present the results.

V. ANALYSIS AND RESULTS

The analysis and results of the F-15 peacetime LCOM study are documented in this chapter. The analysis section investigates the simulation's steady state conditions and autocorrelation functions. The results section consists of maintenance manpower estimates for each AFSC listed in Table I of Chapter III, statistical confidence intervals for these estimates, manpower sensitivity to variations in spare parts and ATS, and a complete basic manning document for the modeled F-15 TFTW.

Analysis

Simulation analysis consisted of graphical and statistical interpretation of accomplished aircraft sortie rate, AFSC manhours used, and AFSC autocorrelation coefficients. The authors used the procedures discussed in Chapter IV to analyze these variables. The simulation run length during this analysis consisted of 98 simulation days including weekends; this period is equivalent to 14 seven day weeks.

Steady State. The authors conducted steady state analysis on both unconstrained and constrained manpower simulations. During the unconstrained manpower simulations, PSR's were requested every seven days. The authors used daily PSR's for the constrained manpower simulations.

The authors chose a seven day data period for unconstrained manpower simulations due to a fundamental seven day cycle in the LCOM statistical output. This cycle was caused primarily by the peacetime operational scenarios; the five day flying and seven day maintenance schedule resulted in an appreciable decrease in manhours used for most AFSC's during the weekends. The accumulation of output data into seven day intervals smoothed this cyclic pattern and simplified the steady state

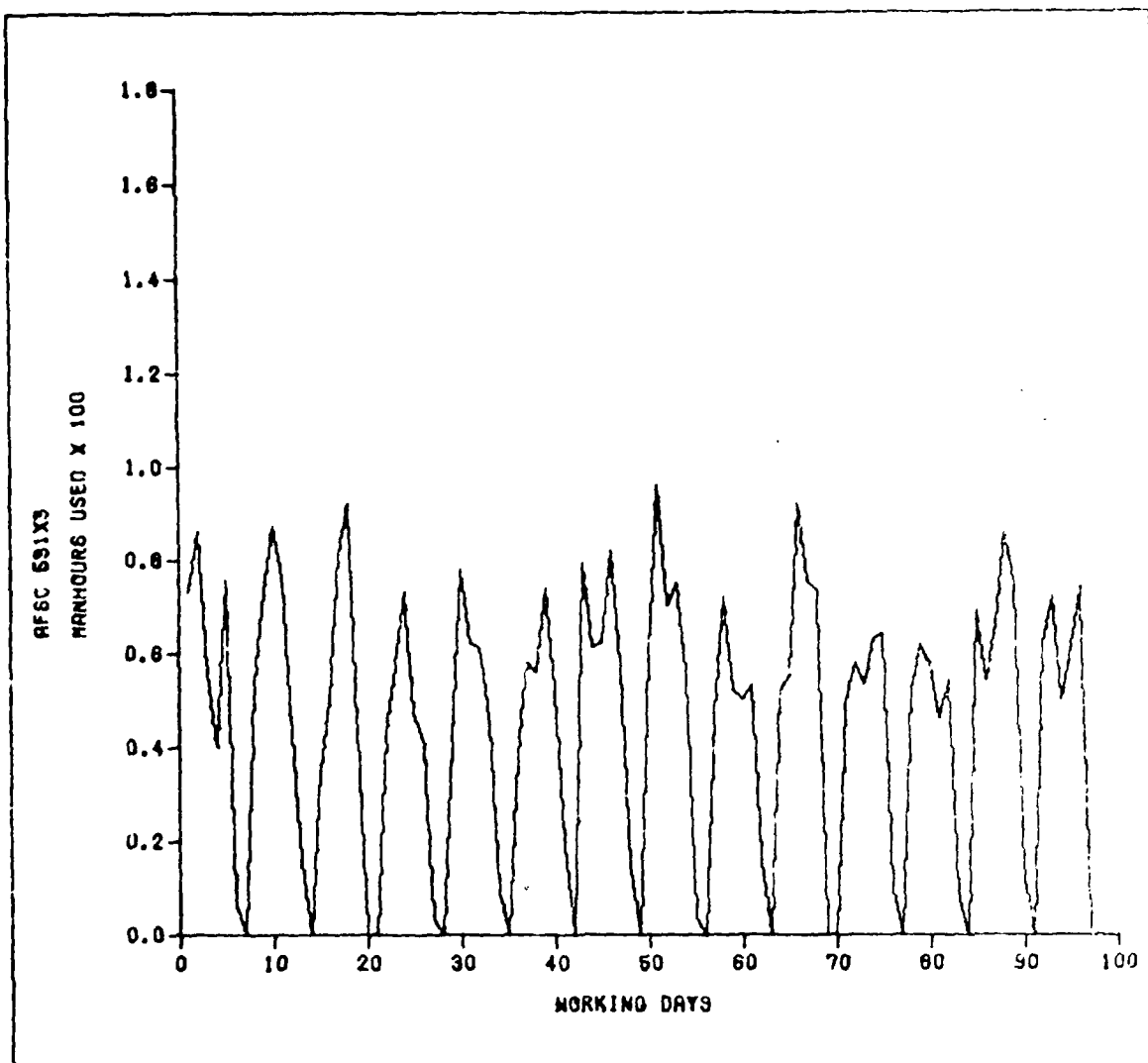


Figure 10. AFSC 531X3 (Structural Repair) Daily Manhours Used

analysis. For example, Figure 10 graphically depicts the daily manhours used for AFSC 531X3 (Structural Repair) over the 93 day simulation period based on unconstrained parts/ATS at a .74 scheduled sortie rate. The graph illustrates the seven day cyclic pattern caused by decreased man-hours used during weekends. Figure 11 contains the weekly manhours used for the same AFSC with identical simulation conditions. The graph, in this case, clearly represents steady state conditions throughout the

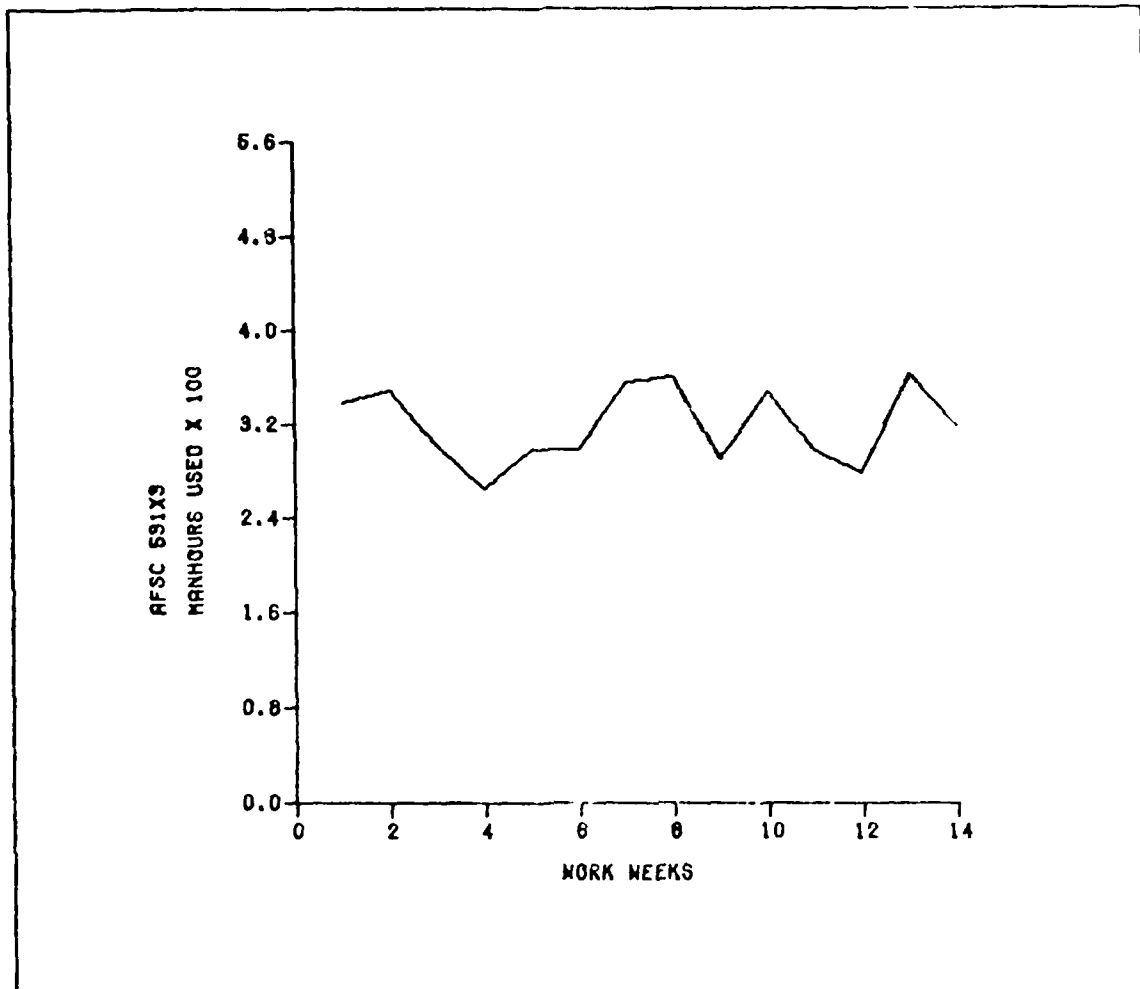


Figure 11. AFSC 531X3 (Structural Repair) Weekly Manhours Used

14 week period; additionally, the Runs test described in Chapter IV indicated no trends in this weekly data. All AFSC's except AFSC 423X3 (Fuel Systems) exhibited similar graphical and statistical steady state conditions throughout the 98 day unconstrained manpower simulations.

AFSC 423X3 was the only manpower statistic to exhibit nonsteady state conditions during the unconstrained manpower simulations. This AFSC exhibited an unstable condition during the constrained parts/ATS simulation at a .43 scheduled sortie rate. Figure 12 graphically

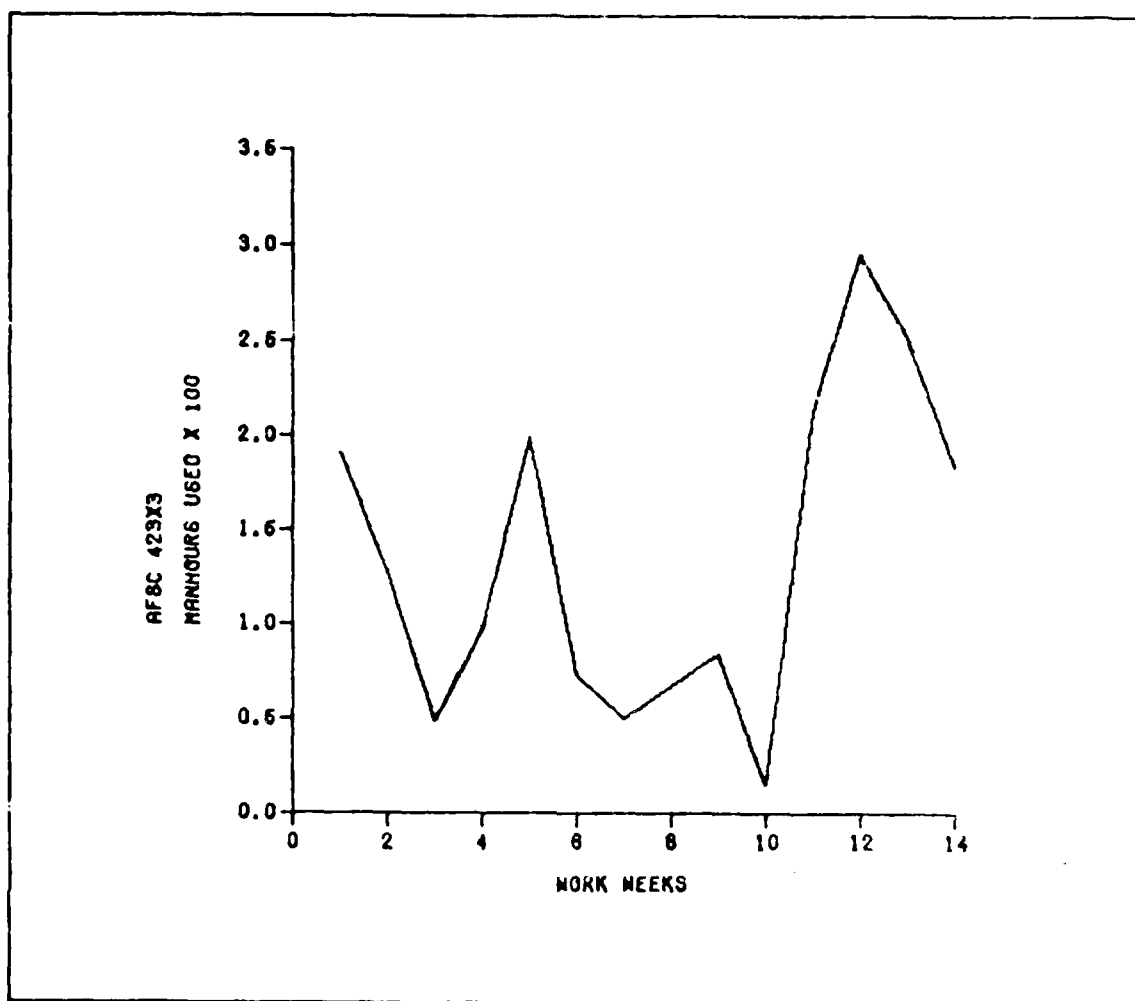


Figure 12. AFSC 423X3 (Fuel Systems) Weekly Manhours Used

illustrates this AFSC's instability in manhours used. The increase in manhours used during the eleventh through thirteenth weeks is especially noteworthy. This demand indicates a backlog of work during the latter portion of the simulation period. The authors, therefore, constrained manpower for this AFSC using the average daily manhours used during the eleventh through thirteenth weeks. This method of constraining manpower has two advantages: first, manpower is allocated to the constrained manpower simulation based on peak workloads as described by Tetmeyer (Ref 33:119); second, if peak workloads are not considered during the

manpower constraint process, the constrained manpower simulation's PSR will indicate manhour utilization for the AFSC in question greater than 60 percent and an additional constrained manpower simulation will be necessary to reduce this utilization below 60 percent.

Table III
AFSC 531X3 Manpower Constraint Calculation

Source	Calculation
Equation (2)	$M_s = \frac{(0-98 \text{ Day PSR})}{\left(\frac{\text{Manhours Used}}{\left(\frac{\text{Utilization}}{\text{Factor}} \right) \left(\frac{\text{Number}}{\text{of Days}} \right) \left(\frac{\text{Shift}}{\text{Length}} \right)} \right)}$ $= \frac{4445}{(.6)(98)(8)}$ $= 9.449 \approx 10 \text{ Men}$

Since all other AFSC's exhibited steady state conditions during the entire simulation period, the authors constrained manpower for these AFSC's using equation (2) from Chapter IV and the respective AFSC man-hours used contained in the 0-98 day cumulative PSR. Table III illustrates the calculation of the manpower constraint for AFSC 531X3 (Structural Repair) using equation (2) and the respective manhours used in Figure C-1 of Appendix C. It should be noted that all manpower constraints are rounded to the next highest integer value during input to the main LCOM program.

During the constrained manpower simulations, the authors used a modified version of LCOM (Ref:19) which provided daily PSR's containing

only operations and personnel data. The elimination of shop repair and supply data from the PSR's appreciably reduced the amount of unneeded computer output during these simulations. Daily manhours used data was required in order to accurately compute the autocorrelation coefficients and statistical confidence intervals discussed later in the chapter; the daily data permits large sample size statistical analysis and increases the statistical confidence in the output data.

Figure 13 graphically illustrates the daily manhours used for AFSC 431X1 (Flight Line Crew Chief) for the unconstrained parts/ATS simulation at a .74 scheduled sortie rate. This graph indicates two major points: first, the seven day cycle of manhours used is very evident; second, the underlying steady state nature of the data throughout the 98 day simulation period is visible. Because steady state conditions are more difficult to detect in the daily manhours used data, the Mann-Whitney Test described in Chapter IV was used to verify output stability. The test indicated no statistical differences in the data contained in Figure 13.

All AFSC's except those listed in Table IV exhibited similar steady state conditions during the entire 98 day constrained manpower simulation period. For those AFSC's in Table IV, the Mann-Whitney test initially indicated instability in the data. The test was, therefore, reapplied to these AFSC's after eliminating the first seven days of data. In most cases, the reduced data set passed the test. In other cases, the first 14 days of data had to be eliminated before the reduced data set would pass the Mann-Whitney test. Table IV indicates each AFSC and its respective usable data sub-set. These data subsets were used to verify

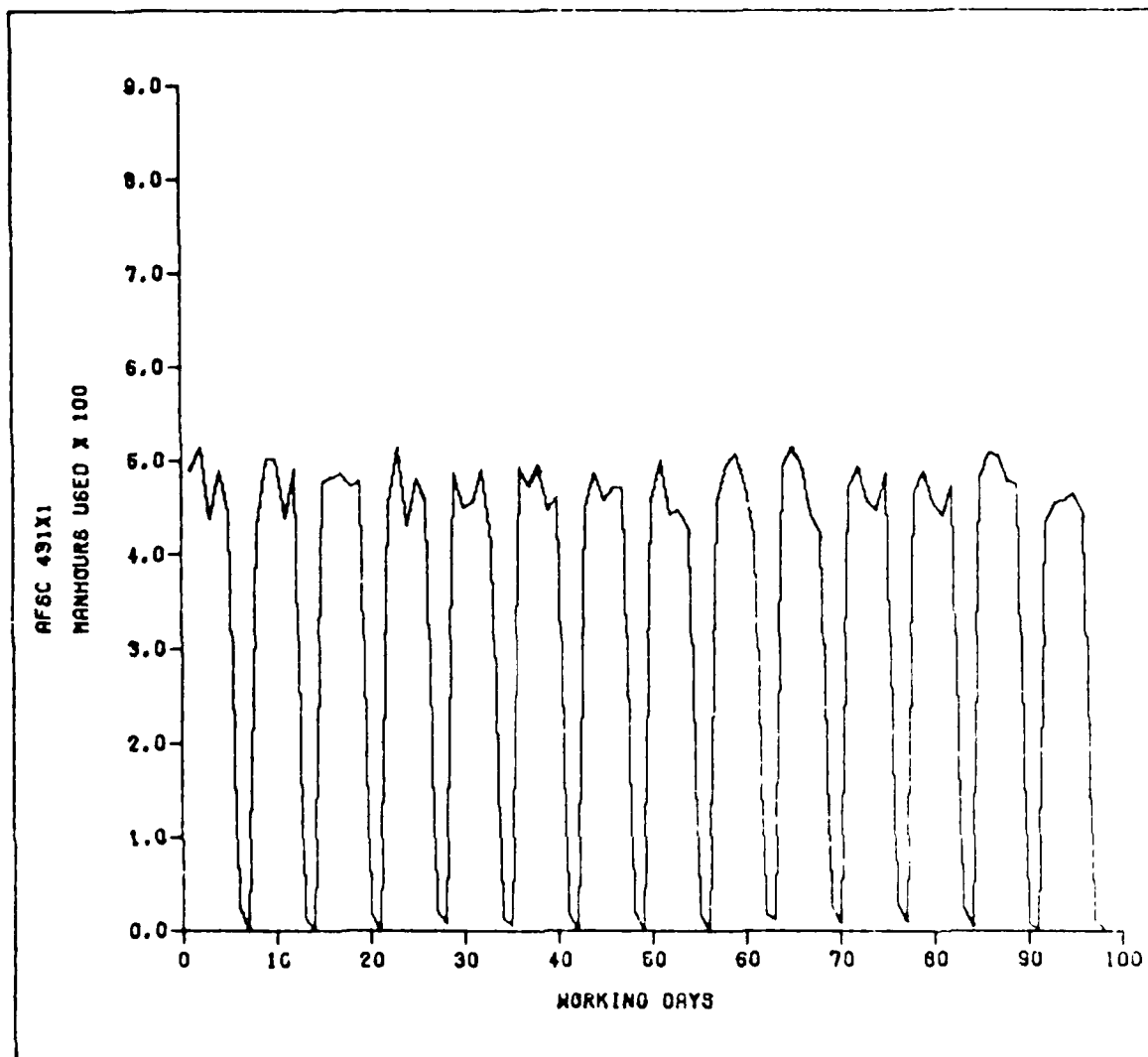


Figure 13. AFSC 431X1 (Flight Line Crew Chief) Daily Manhours used

manhour utilization, calculate manpower estimates, and compute confidence intervals for the AFSC's listed in Table IV.

The authors also analyzed accomplished aircraft sortie rate for the constrained manpower simulations. If this sortie rate exhibits steady state conditions, then the modeled F-15 TFTW can satisfy TAC training syllabi requirements on a routine basis.

Table IV

LCOM AFSC's That Exhibited Initial Transient Conditions

Constraint Type	Scheduled Sortie Rate	AFSC	Usable Simulation Period
Unconstrained Parts/ATS	1.0	326X2A (COM/ NAV/ ECM)	Last 91 Days
Constrained Parts/ Unconstrained ATS	1.0	423X3 (Fuel Systems)	Last 84 Days
Constrained Parts/ Constrained ATS	1.0	326X1D (Automatic Test Station)	Last 91 Days
	1.0	326X2A (Inertial Navigation System)	Last 91 Days
	1.0	431X1 (Phase Inspection)	Last 91 Days
	.74	426X2 (Jet Engine)	Last 84 Days

Figure 14 depicts the accomplished aircraft sortie rate for the unconstrained parts/ATS simulation at a .74 scheduled sortie rate. The graph excludes weekends due to the undefined nature of sortie rate for nonflying days. In Figure 14, accomplished sortie rate exhibits a steady state condition throughout the 70 flying days. The Mann-Whitney test also verified steady state conditions in the data. Accomplished sortie rates

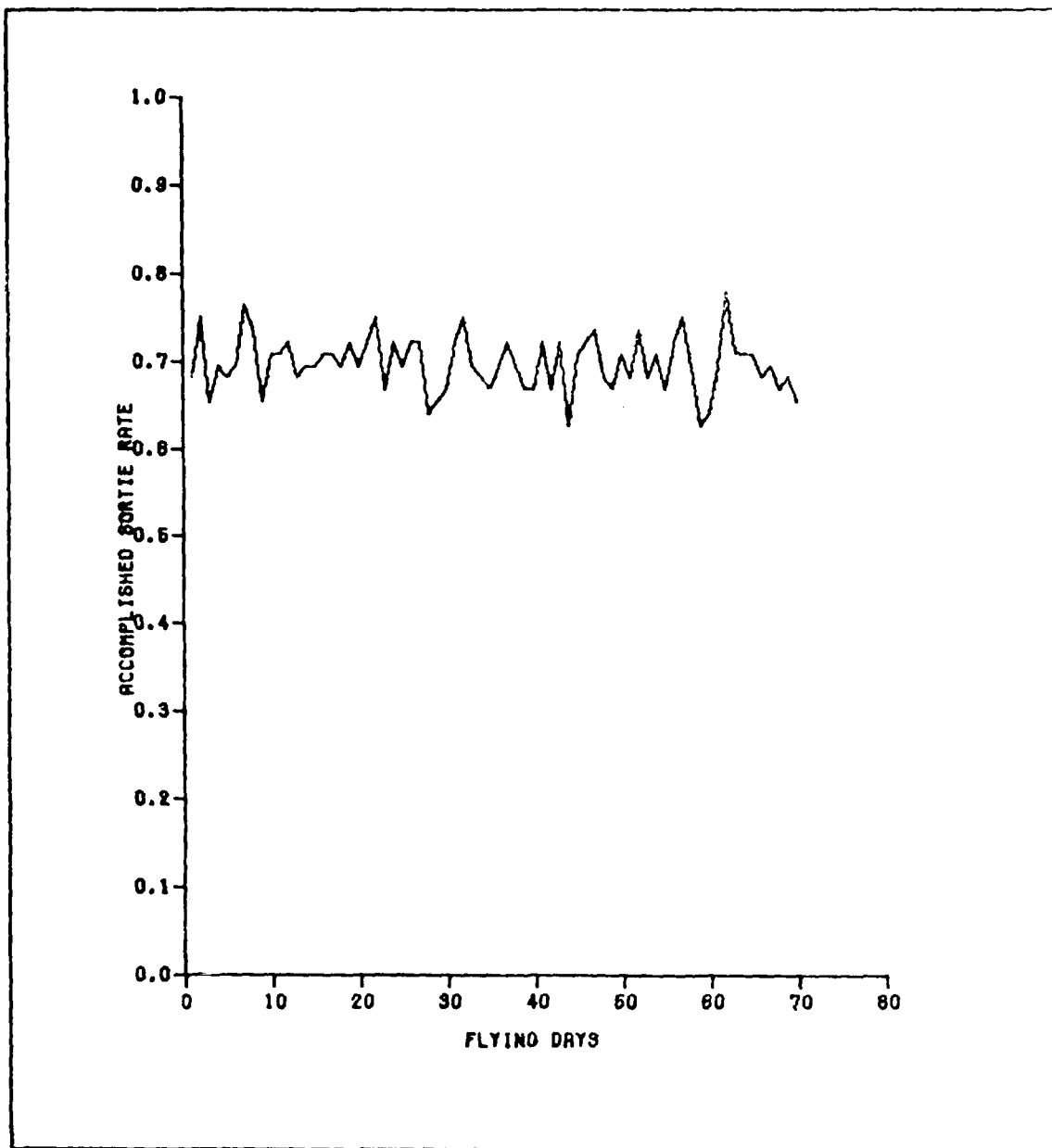


Figure 14. Accomplished Aircraft Sortie Rate for Constrained Manpower and Unconstrained Parts/ATS Simulation at .74 Scheduled Sortie Rate

for each of the nine combinations of parts/ATS constraints and scheduled sortie rates exhibited similar steady state conditions. These steady state conditions indicate that the modeled F-15 TFTW can routinely meet syllabi training requirements.

Autocorrelation. The authors conducted the autocorrelation analysis on the constrained manpower simulations. The autocorrelation coefficients ($\hat{\rho}(L)$) were estimated for each AFSC using the respective manhours used and equation (13) found in Chapter IV; the lag (L) between daily observations was incremented to include a one through 97 day lag. For those AFSC's listed in Table IV, $\hat{\rho}(L)$ was estimated for the corresponding reduced data sets. The analysis consisted of both graphical and statistical interpretation of the autocorrelation function.

Figure 15 graphically illustrates the autocorrelation function versus the lag in days for AFSC 431X1 (Flight Line Crew Chief) for the unconstrained parts/ATS simulation at a .74 scheduled sortie rate. This graph indicates two major points: first, the seven day cyclic nature of the function caused by the reduced manhour demands on weekends is clearly evident; second, multiple lags of seven days are highly correlated. The high correlation of manhours used on multiple seven day lags is due to the seven day cyclic nature of the simulation data. This functional form of autocorrelation coefficients prevents the grouping of manhours used into blocks of independent observations. The authors, therefore chose to use the estimated correlation coefficients and equation (14) to correct the variance of daily manhour observations during the computation of manpower statistical confidence intervals.

AFSC 423X3 (Fuel Systems) was the only AFSC to exhibit a more desirable autocorrelation function. The reason for this unique difference was that the fuel systems shop did not show a routine decrease in manhours used each weekend. This resulted in an absence of the seven day cycle. Figure 16 illustrates the graphical nature of the autocorrelation function for this AFSC. In the graph, lags of 15 or more days indicate

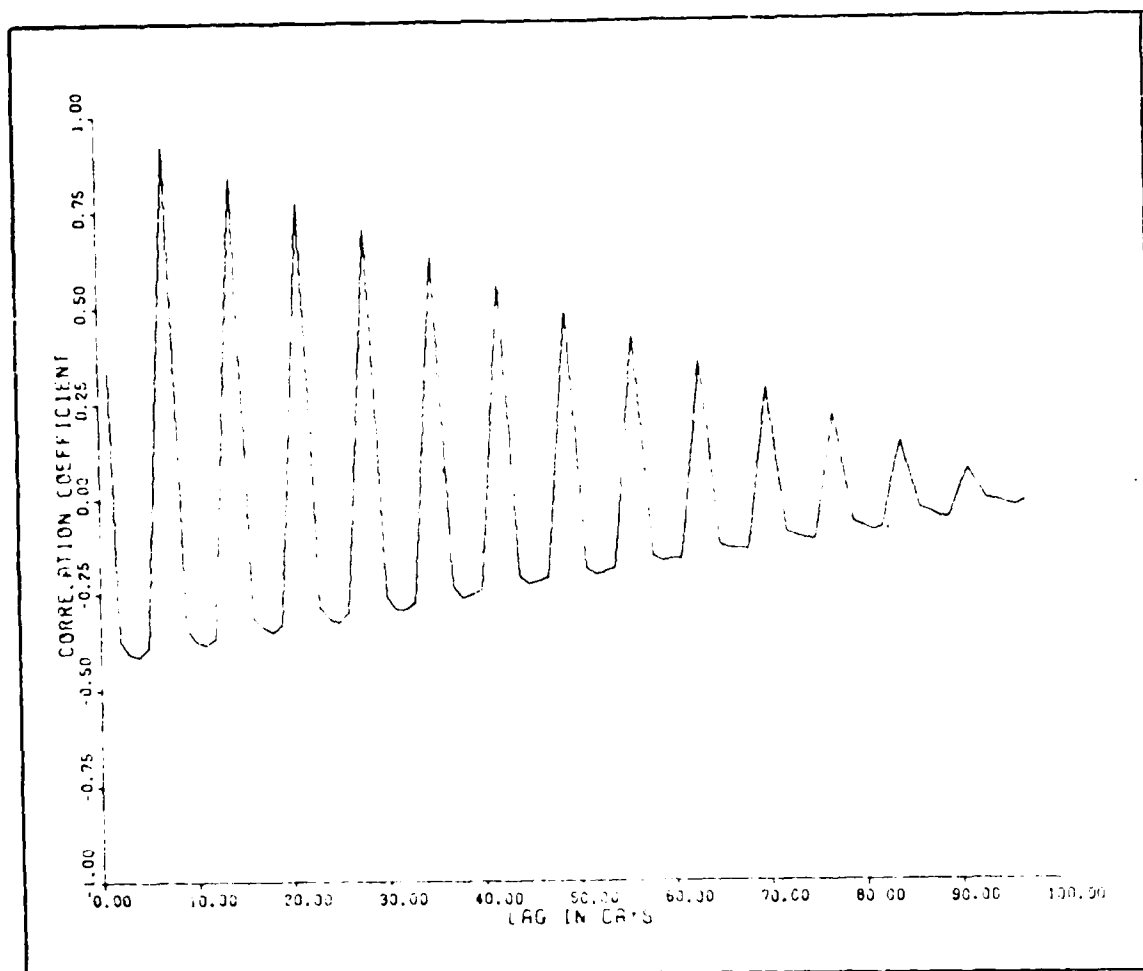


Figure 15. AFSC 431X1 (Flight Line Crew Chief) Autocorrelation Function

a $\hat{\rho}(L)$ close to zero. As a result, manhours used contained on cumulative 15 day PSR's would be statistically independent and could be treated as independent observations during the calculation of statistical confidence intervals. The type of autocorrelation function illustrated in Figure 16 is often found in an LCOM simulation where maintenance and flying activity operate concurrently. Concurrent maintenance and flying activity do not produce the cyclic output data that is found in this study. In particular, wartime LCOM simulations contain the functional form illustrated in Figure 16.

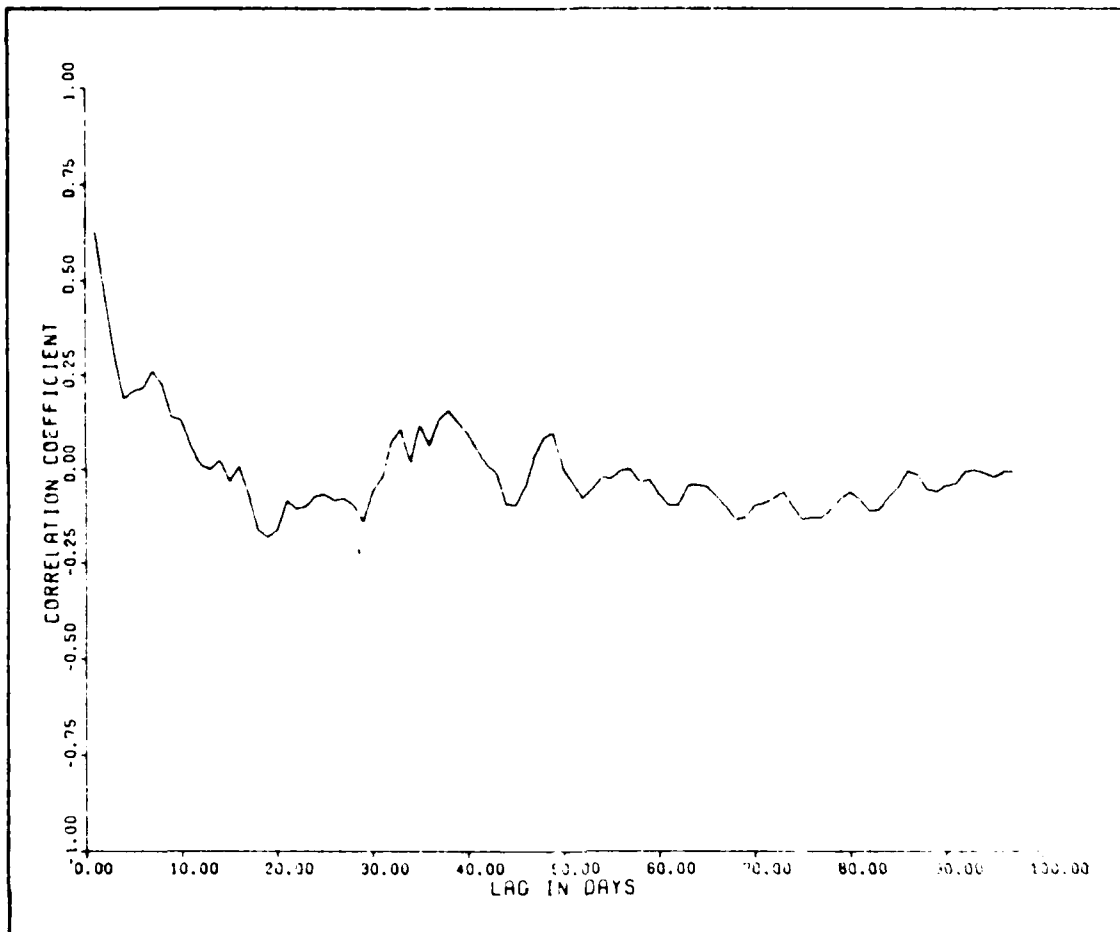


Figure 16. AFSC 423X3 (Fuel Systems) Autocorrelation Function

Because the majority of AFSC's in this study exhibited autocorrelation functions similar to Figure 15, the variance of daily manhours used for each AFSC including AFSC 423X3 was corrected using equation (13). These corrected variances were used during calculation of the manpower confidence intervals.

Results

The results of the F-15 TFTW LCOM simulation contain the direct manning estimations (M) for each AFSC contained in Table I of Chapter III,

95 percent confidence intervals for these estimates, and sensitivity of M to constrained parts and constrained parts/ATS. The final output of these estimates is a USAF basic manning document for the F-15 TFTW based on unconstrained parts and ATS.

Direct Manning. The average daily manhours used from the final constrained manpower simulations are applied to equations (1) and (2) from Chapter IV to calculate the direct manning for each AFSC listed in Table I. Direct Manning is then converted to whole men according to AFM 25-5 standards (Ref 2:Chap. 6, p. 29). During the calculation of M, the AFM 25-5 standard of 30.44 work days per month is applied to equation (2). Table V illustrates the computation of direct manning for AFSC 531X3 (Structural Repair) for the unconstrained parts/ATS simulation at .74 scheduled sortie rate.

Table V
AFSC 531X3 Direct Manning Computation

Source	Calculation
Equation (1)	$M_s = \frac{\text{Average Daily Manhours Used}}{(\text{Utilization Factor})(\text{Shift Length})}$ $= \frac{(40.44)}{(.6)(8)}$ $= 8.425$
Equation (2)	$M = \frac{M_s (\text{Workdays/mo})(\text{Shift Length})}{144 \text{ Hours/Man/Month}}$ $= \frac{(8.425)(30.44)(8)}{144}$ $= 14.248$
AFM 25-5	Direct Manning = 14 Men

Confidence Intervals. Confidence intervals for direct manning are computed using equations (1), (2), (11), and (14) found in Chapter IV. The computation is a six step process: first, estimate the sample variance of daily manhours used (Ref 25:268); second, use equation (14) to calculate the corrected sample variance of daily manhours used; third, convert the corrected sample variance into a standard deviation of daily manhours used; fourth use equations (1) and (2) to transform the standard deviation of daily manhours used into a direct manning standard deviation; fifth, use equation (11) to develop 95 percent confidence intervals for direct manning; finally, convert the confidence intervals into integer values in accordance with AFM 25-5 (Ref 2: Chap. 6, p. 29). Table VI illustrates the computation of a 95 percent confidence interval for the direct manning of AFSC 531X3 based on unconstrained parts/ATS at a .74 scheduled sortie rate. In these calculations, N equals the number of steady state days simulated. In all cases, except those AFSC's listed in Table IV, N equals 98.

The procedures contained in Tables V and VI were used to compute each AFSC's direct manning and confidence intervals for the three constraint types (unconstrained parts/ATS, constrained parts/unconstrained ATS, and constrained parts/ATS) and scheduled sortie rates (.43, .74, and 1.0). The direct manning for the End of Runway Crew was separately calculated using equation (15) found in Chapter IV and added to the direct manning estimate and confidence interval of AFSC 431X1 (Flight Line Crew Chief). This calculation is illustrated in Table VII.

Table VI

AFSC 531X3 Confidence Interval Computation

Source	Calculation
Sample Variance of Daily Manhours Used	$S_{\mu}^2 = 5.526$
Equation (14)	$\text{Corrected } S_{\mu}^2 = S_{\mu}^2 \left[1 + 2 \sum_{L=1}^{N-1} \left(1 - \frac{L}{N} \right) \hat{p}(L) \right]$ $= 5.256 \left[1 + 2 \sum_{L=1}^{97} \left(1 - \frac{L}{98} \right) \hat{p}(L) \right]$ $= .507$
Convert Variance to Standard Deviation	<p>Average Daily Manhours Used = $\sqrt{.507}$</p> <p>Standard Deviation = .712</p>
Equation (1)	$M_s \text{ Standard Deviation} = \frac{(\text{Average Daily Manhours Used Standard Deviation})}{(\text{Utilization Factor})(\text{Shift Length})}$ $= \frac{(.712)}{(.6)(8)}$ $= .148$
Equation (2)	$M \text{ Standard Deviation} = \frac{(M_s \text{ Standard Deviation})(\text{Work Days/Mo})(\text{Shift Length})}{(144 \text{ Hours/Man/Month})}$ $= \frac{(.148)(30.44)(8)}{144}$ $= .250$

Table VI. (Continued)

AFSC 531X3 Confidence Interval Computation

Source	Calculation
Equation (11)	$\begin{aligned} \text{95\% Confidence Interval} &= M \pm (Z_{\alpha/2}) (M \text{ Standard Deviation}) \\ &= 14.248 \pm (1.96)(.250) \\ &= 14.248 \pm .49 \\ &= (13.758, 14.738) \end{aligned}$
AFM 25-5	$\begin{aligned} \text{95\% Confidence Interval for } M &= (13, 14) \text{ Men} \end{aligned}$

Table VII

End of Runway Crew Direct Manning Computation

Source	Computation
Equation (15)	$\begin{aligned} M &= \frac{(\text{Crew Size})(\text{Workdays per Month})(\text{Hours per Day})(\text{4.348 Weeks per Month})}{144 \text{ Hours/Man/Month}} \\ &= \frac{(3)(5)(16)(4.348)}{144} \\ &= 7.25 \end{aligned}$
AFM 25-5	Direct Manning = 7 Men

Direct Manning Sensitivity. This section illustrates both graphically and statistically the sensitivity of direct manning estimates to each of the three simulation constraint types and scheduled sortie rates. The authors used the Moody Regression Program to develop a regression equation for each constraint type comparing AFSC direct manning with flying hours per month (FHPM). The accomplished sortie rate (ASR) corresponding to the simulation's scheduled sortie rate was converted into FHPM for the purpose of this comparison. Table VIII depicts the resulting ASR and FHPM for the three constraint types and scheduled sortie rates.

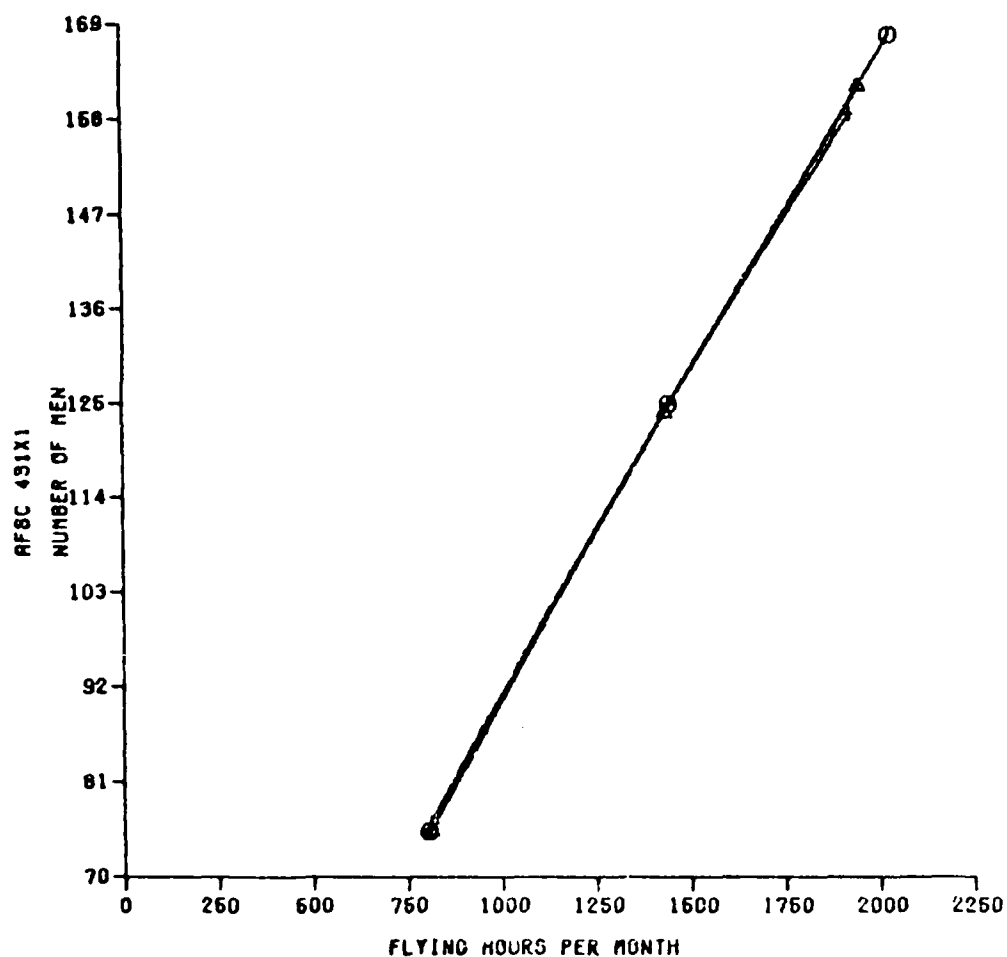
Table VIII

Accomplished Sortie Rate (ASR) and Flying Hours per Month (FHPM) versus Constraint Type and Scheduled Sortie Rate

Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
Unconstrained Parts/ Unconstrained ATS	.404 ASR 806 FHPM	.697 ASR 1444 FHPM	.955 ASR 2037 FHPM
Constrained Parts/ Unconstrained ATS	.406 ASR 809 FHPM	.692 ASR 1433 FHPM	.916 ASR 1954 FHPM
Constrained Parts/ Constrained ATS	.406 ASR 808 FHPM	.698 ASR 1446 FHPM	.904 ASR 1930 FHPM

Figures 17 through 30 depict the direct manning for those AFSC's listed in Table I. These figures use the Moody Regression equations to graphically illustrate the sensitivity of direct manning to constraint type and flying hours per month. The figures also depict in tabular form the direct manning and 95 percent confidence intervals corresponding to each constraint type and scheduled sortie rate.

Table VIII and Figures 17 through 30 summarize the relationships between scheduled sortie rate, flying hours per month, accomplished sortie rate, and direct manning. For example, AFSC 431X1 (Flight Line Crew Chief) in Figure 17 requires 76 direct men with a 95 percent confidence interval of (74-78) to achieve 806 FHPM and a .404 ASR based on unconstrained parts/ATS and a .43 scheduled sortie rate.



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	76 (74-78)	124 (120-128)	168 (163-172)
△ - Constrained Parts/ Unconstrained ATS	76 (74-79)	123 (119-127)	162 (157-167)
+ - Constrained Parts/ Constrained ATS	77 (75-79)	124 (119-128)	159 (149-169)

Figure 17. AFSC 431X1 (Flight Line Crew Chief) Direct Manning

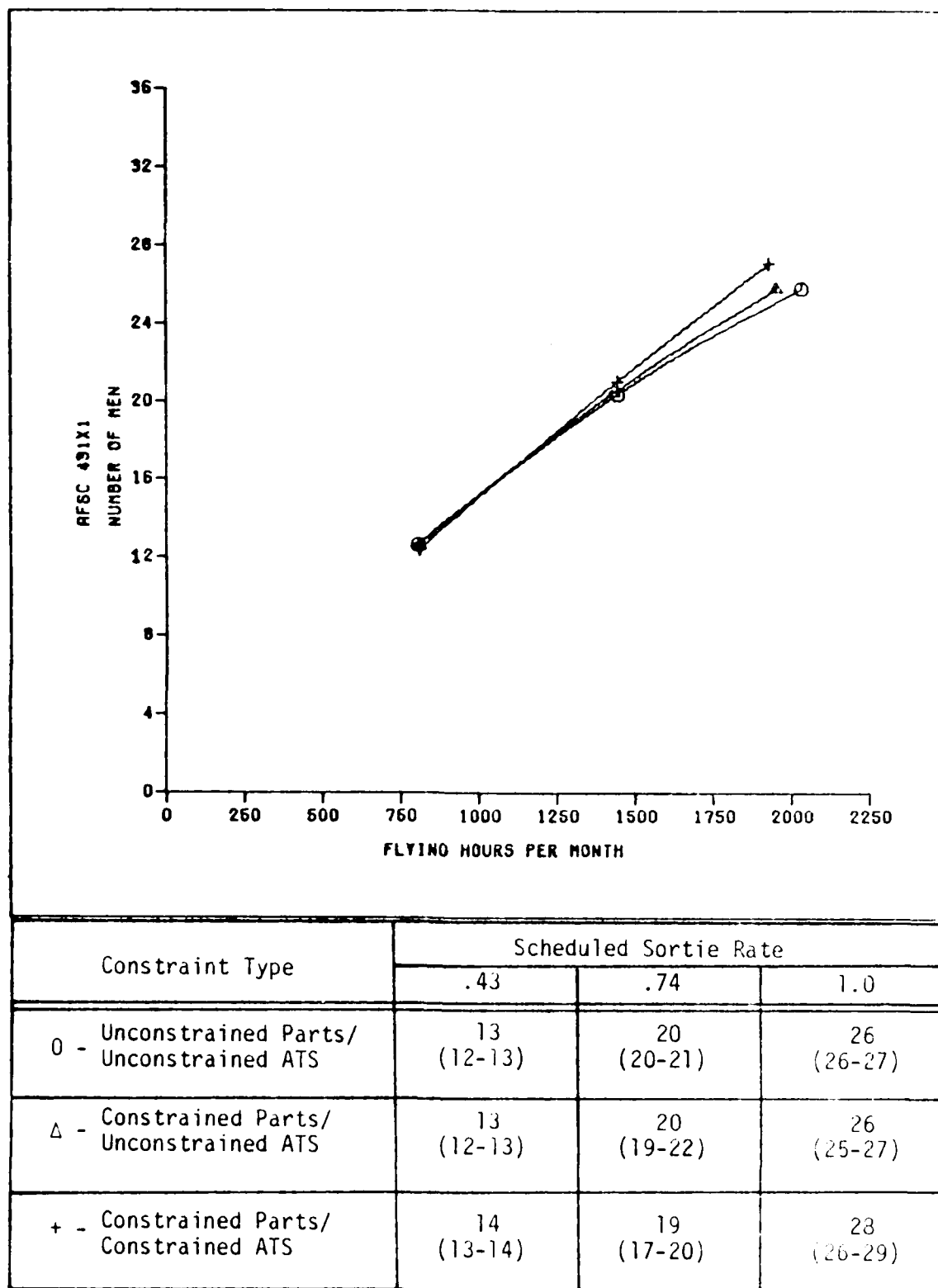


Figure 18. AFSC 431X1 (Phase Inspection) Direct Manning

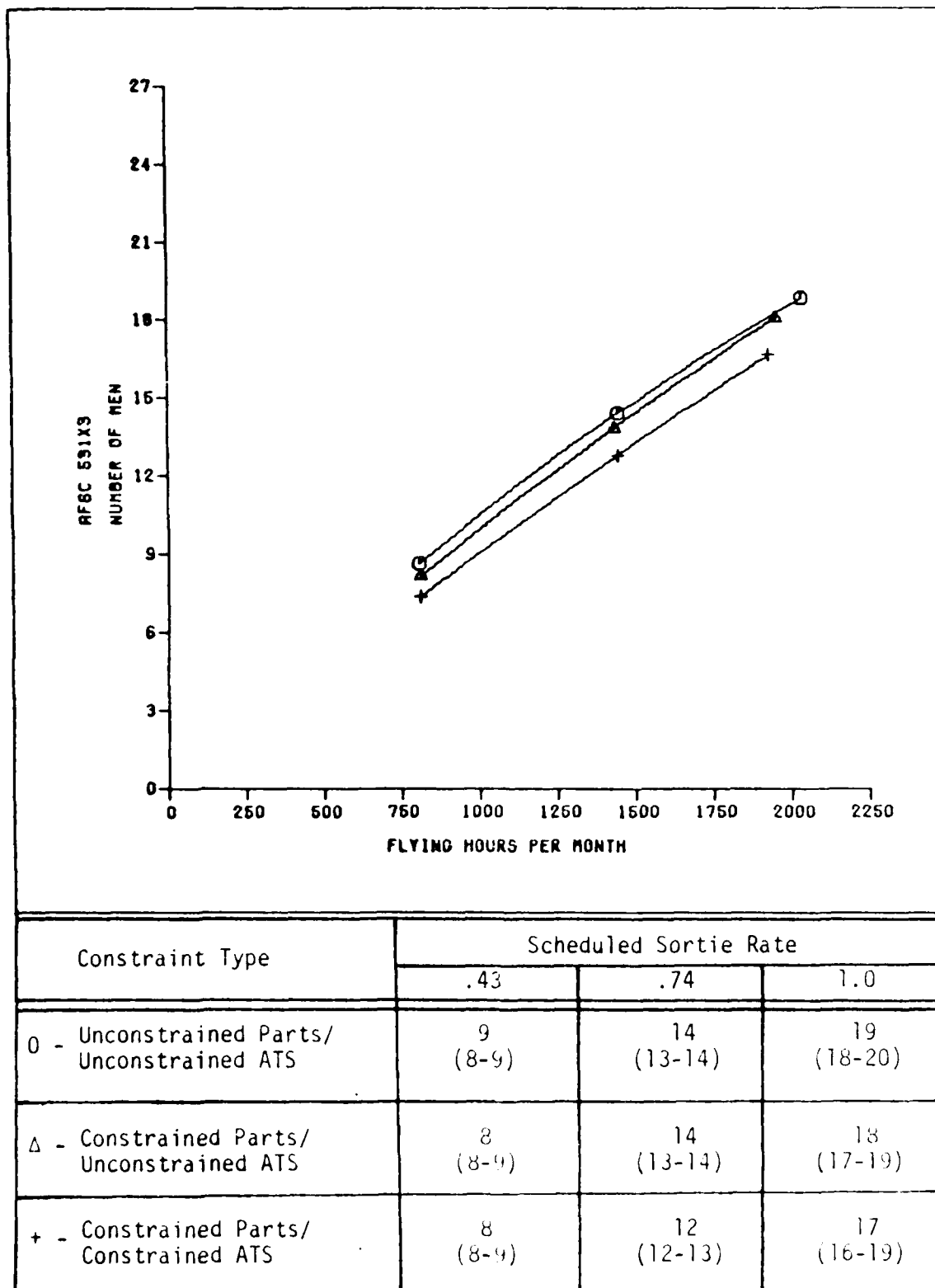


Figure 19. AFSC 531X3 (Structural Repair) Direct Manning

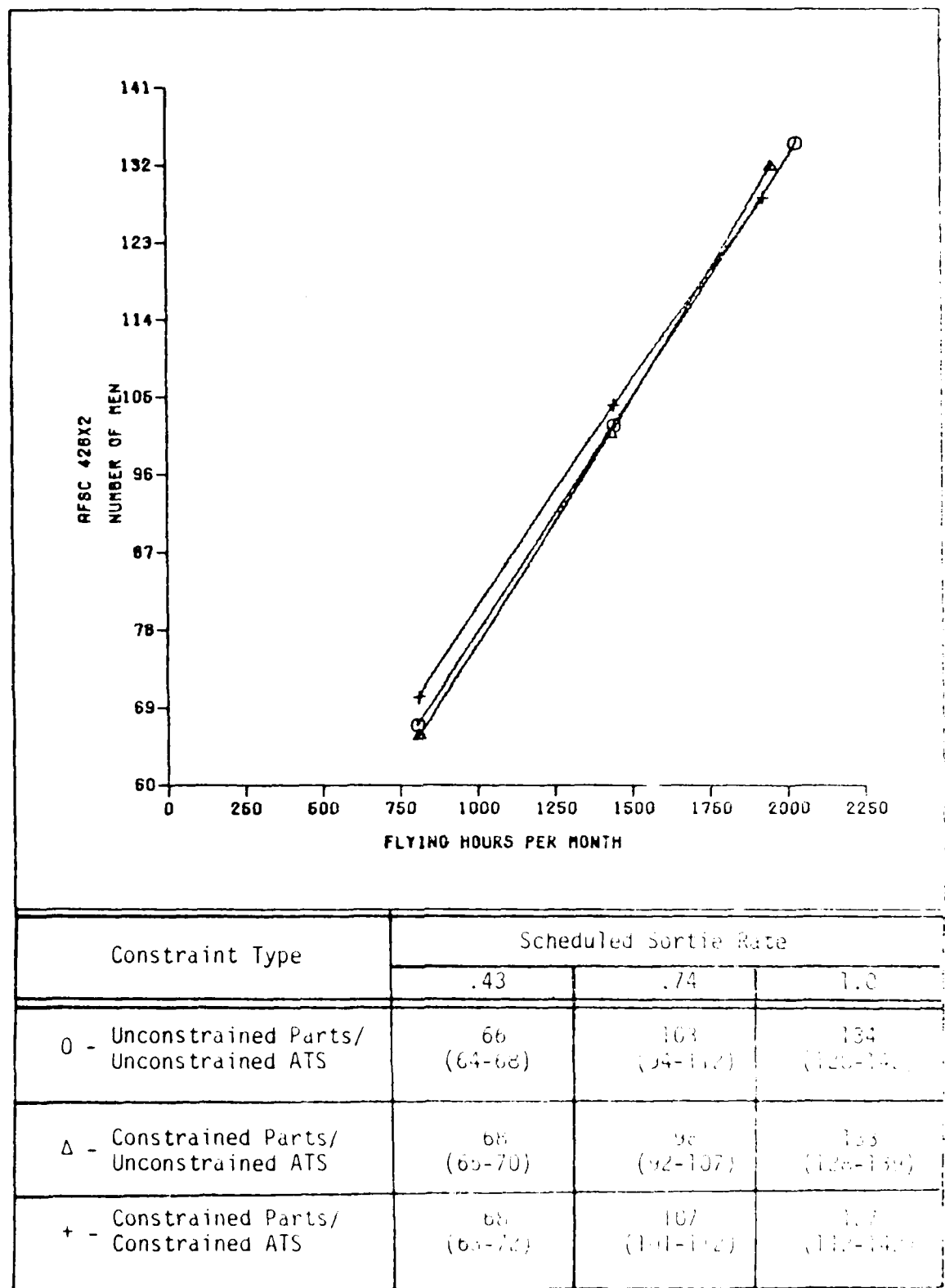


Figure 20. AFSC 426X2 (Jet Engine) Direct Manning

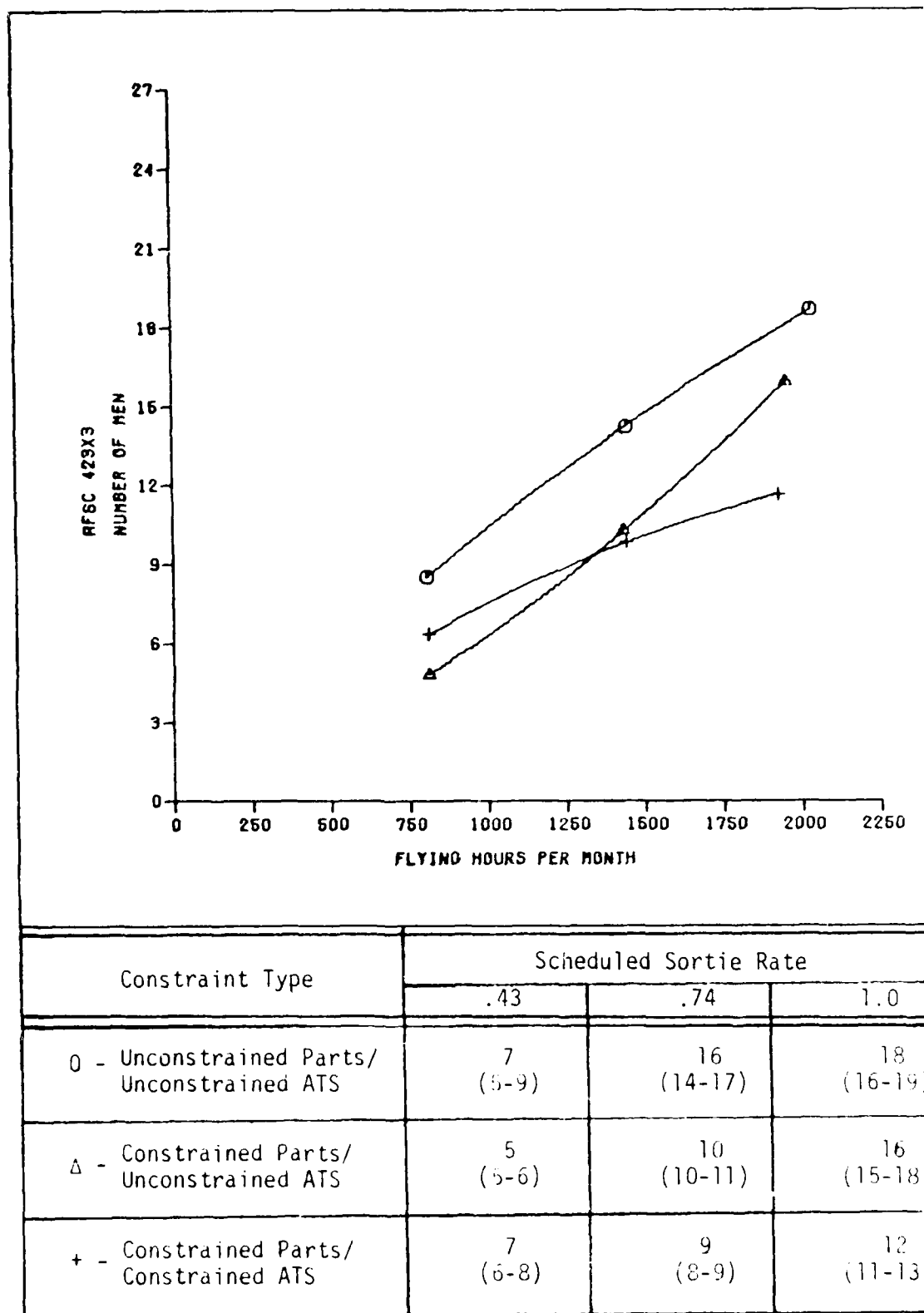
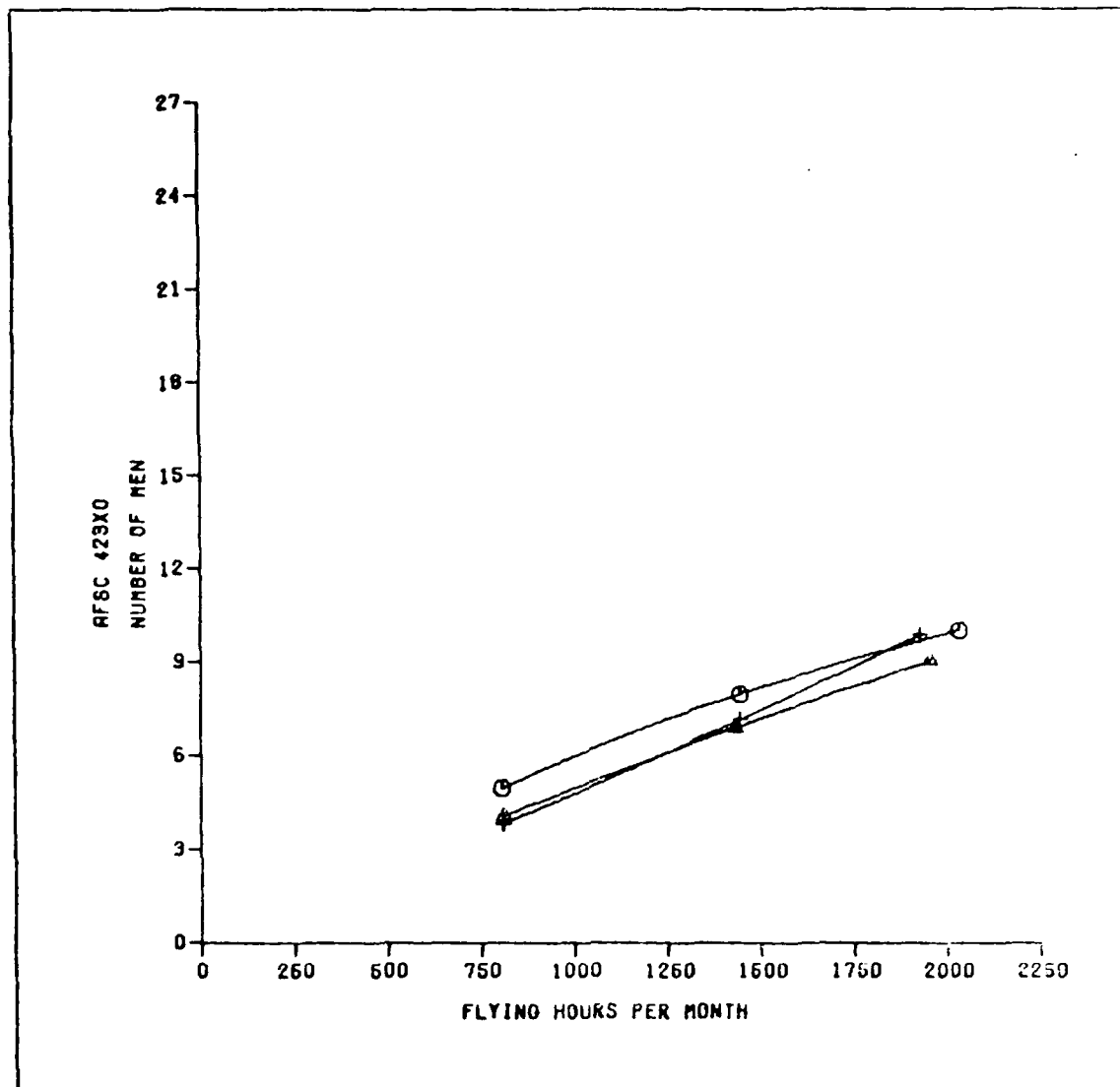
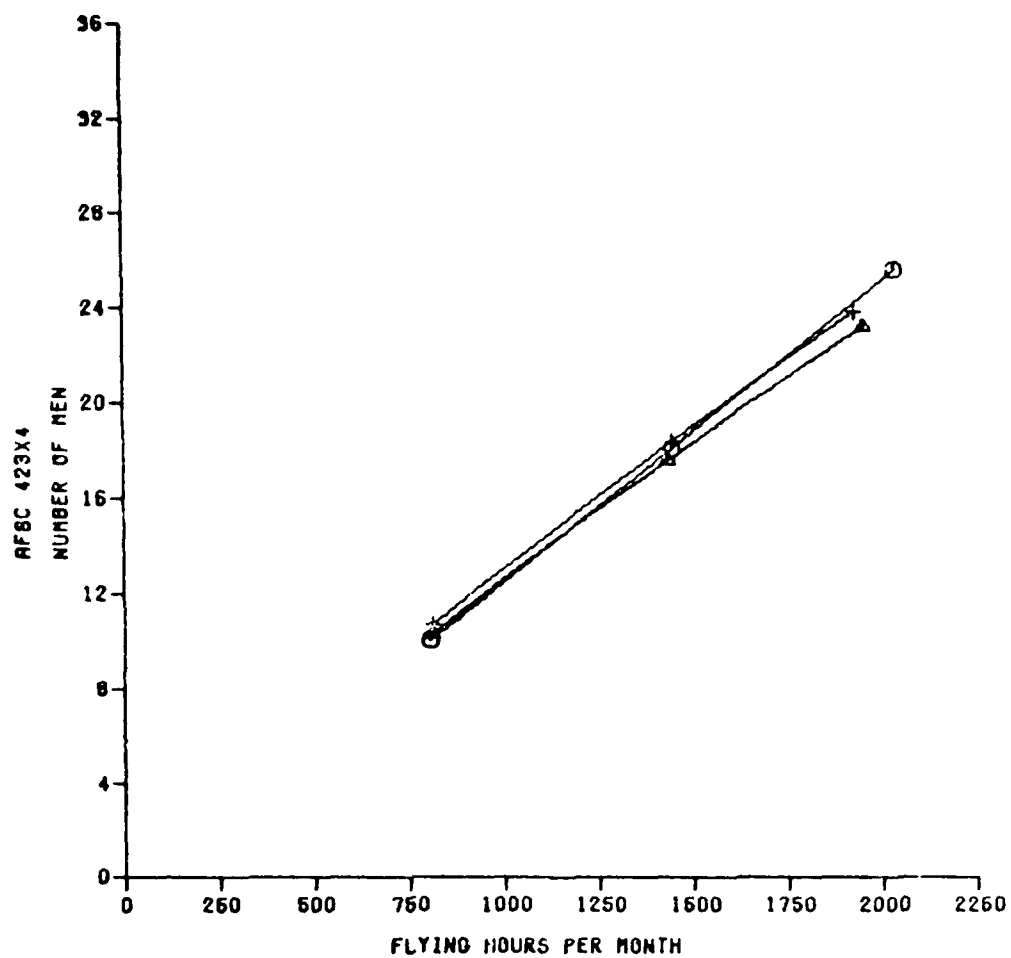


Figure 21. AFSC 423X3 (Fuel Systems) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	5 (5-5)	8 (7-8)	10 (9-10)
Δ - Constrained Parts/ Unconstrained ATS	4 (4-5)	7 (6-7)	9 (9-10)
+ - Constrained Parts/ Constrained ATS	4 (4-4)	7 (7-7)	10 (9-10)

Figure 22. AFSC 423X0 (Electrical Systems) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	11 (10-11)	17 (16-19)	26 (25-27)
Δ - Constrained Parts/ Unconstrained ATS	10 (9-11)	18 (17-19)	23 (22-24)
+ - Constrained Parts/ Constrained ATS	11 (10-11)	18 (18-19)	24 (22-25)

Figure 23. AFSC 423X4 (Pneudraulics) Direct Manning

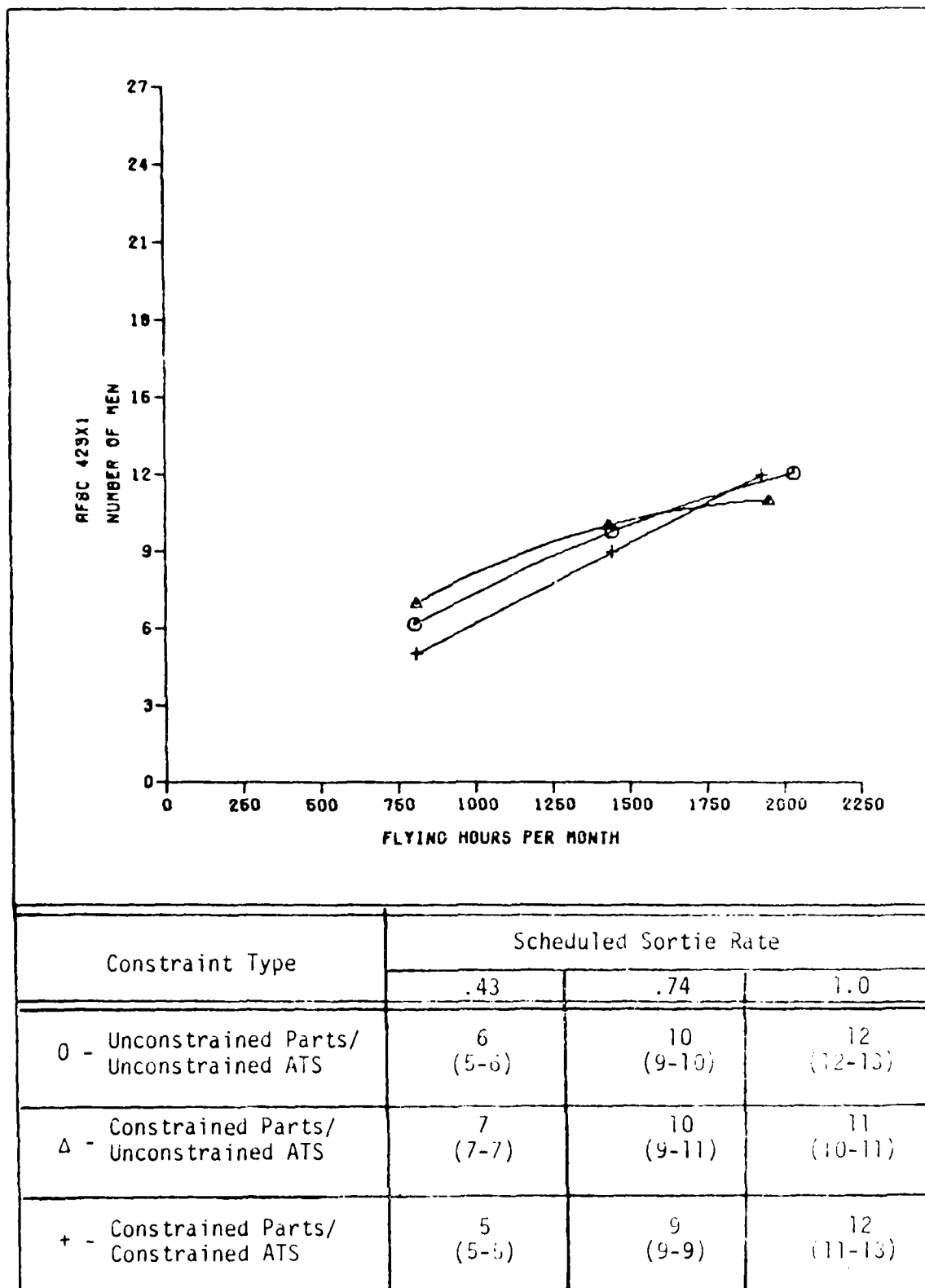
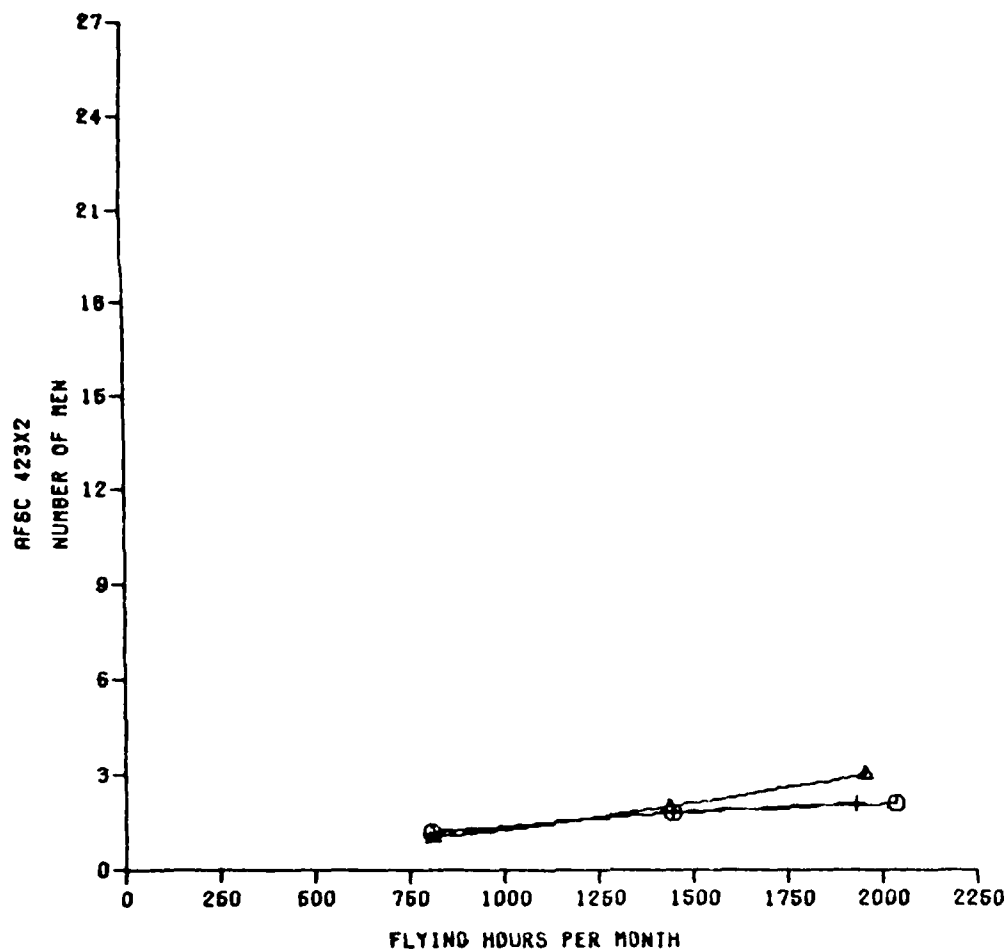


Figure 24. AFSC 423X1 (Environmental Systems) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	1 (1-2)	2 (2-2)	2 (2-3)
Δ - Constrained Parts/ Unconstrained ATS	1 (1-1)	2 (2-2)	3 (2-3)
+ - Constrained Parts/ Constrained ATS	1 (1-2)	2 (1-2)	2 (2-3)

Figure 25. AFSC 423X2 (Egress Systems) Direct Manning

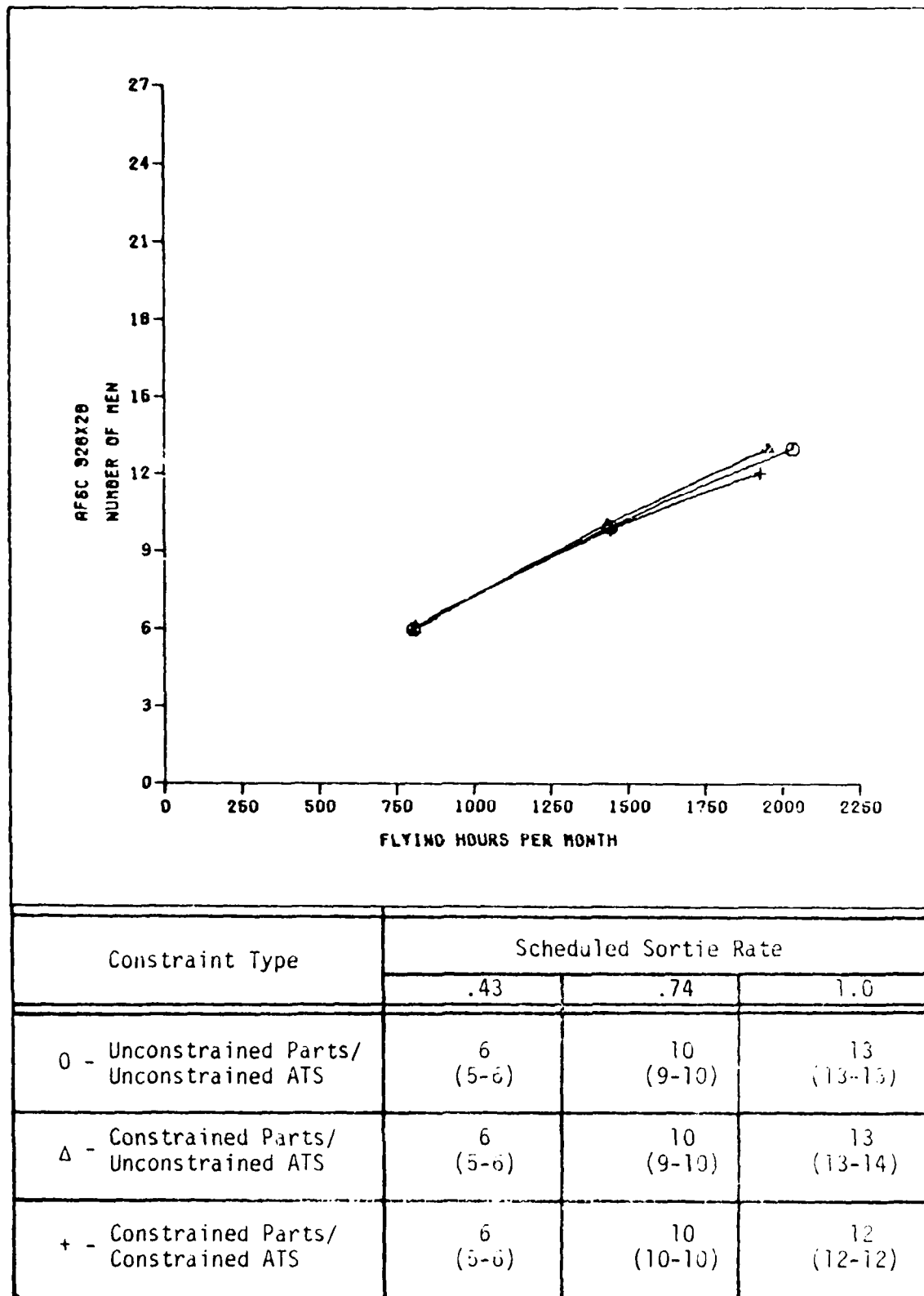
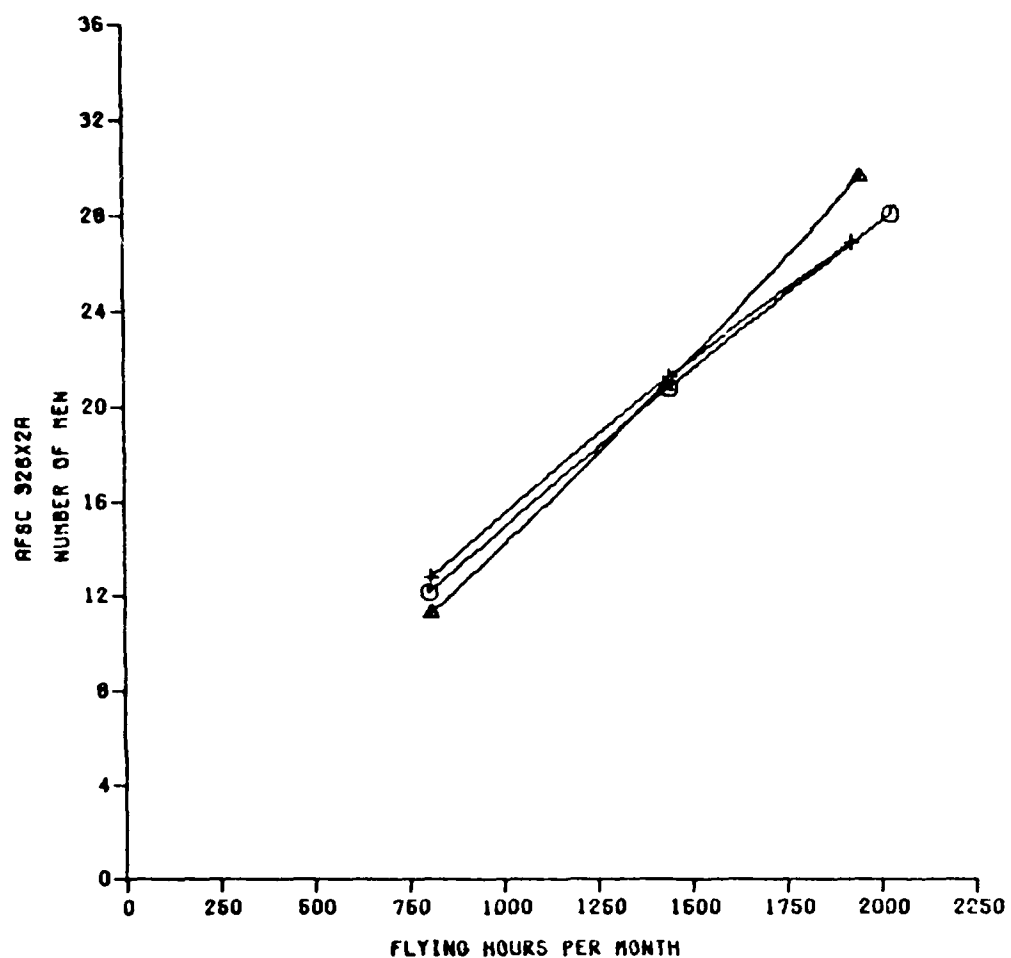
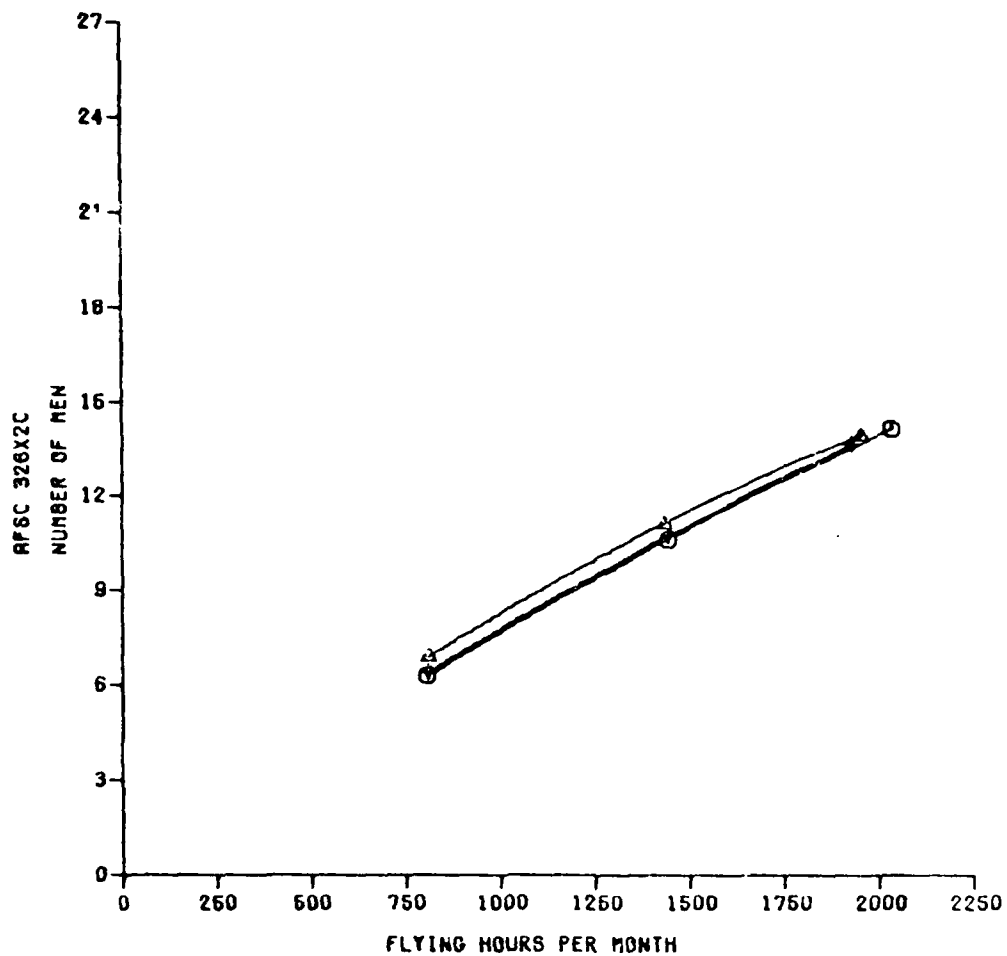


Figure 26. AFSC 326X2B (Automatic Flight Control/Instrument) Direct Manning



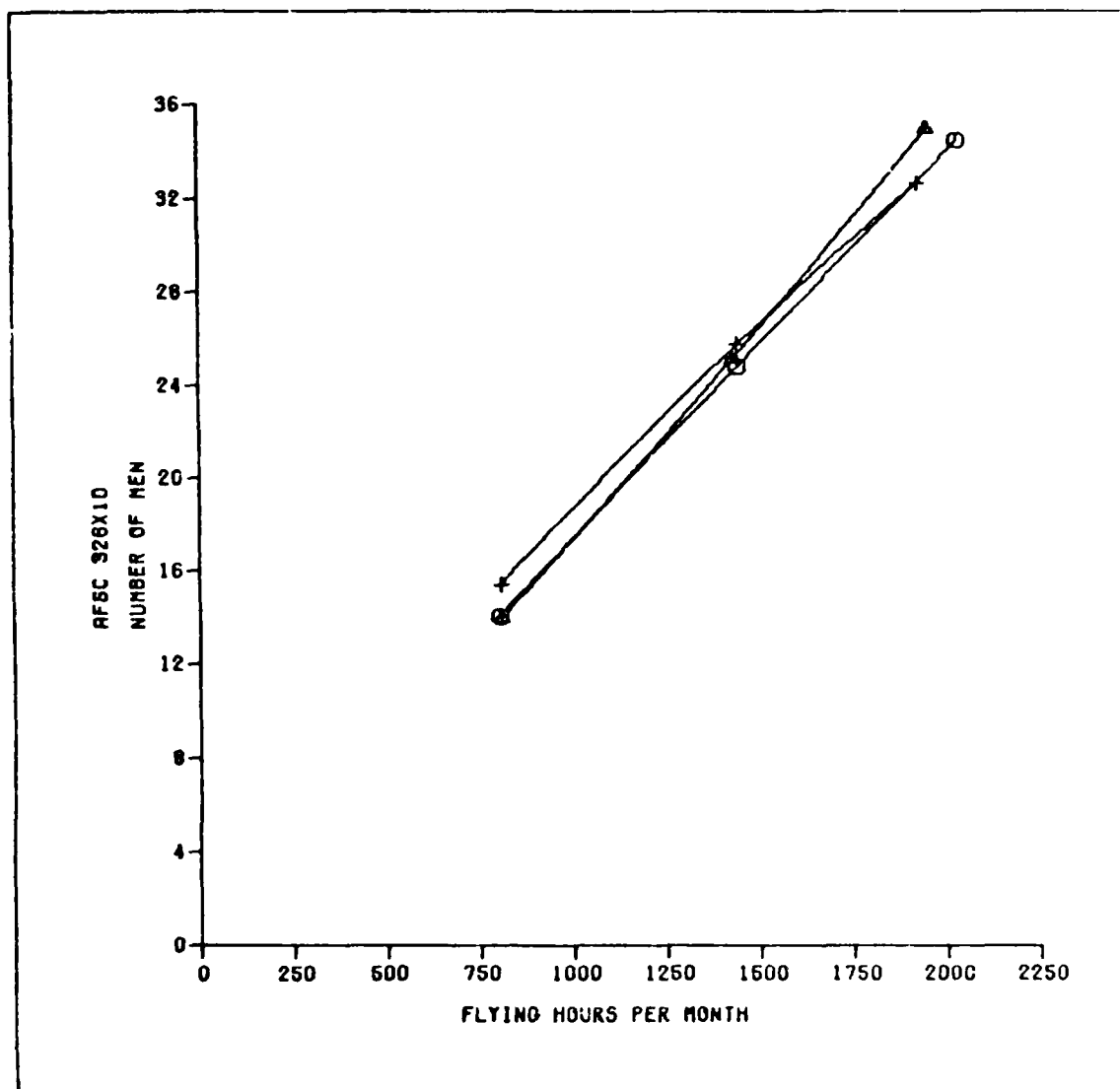
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	12 (11-12)	21 (21-22)	28 (28-29)
Δ - Constrained Parts/ Unconstrained ATS	12 (12-12)	20 (19-21)	30 (29-31)
+ - Constrained Parts/ Constrained ATS	13 (12-13)	21 (20-22)	27 (25-30)

Figure 27. AFSC 326X2A (Inertial Navigation System/Weapon Control)
Direct Manning



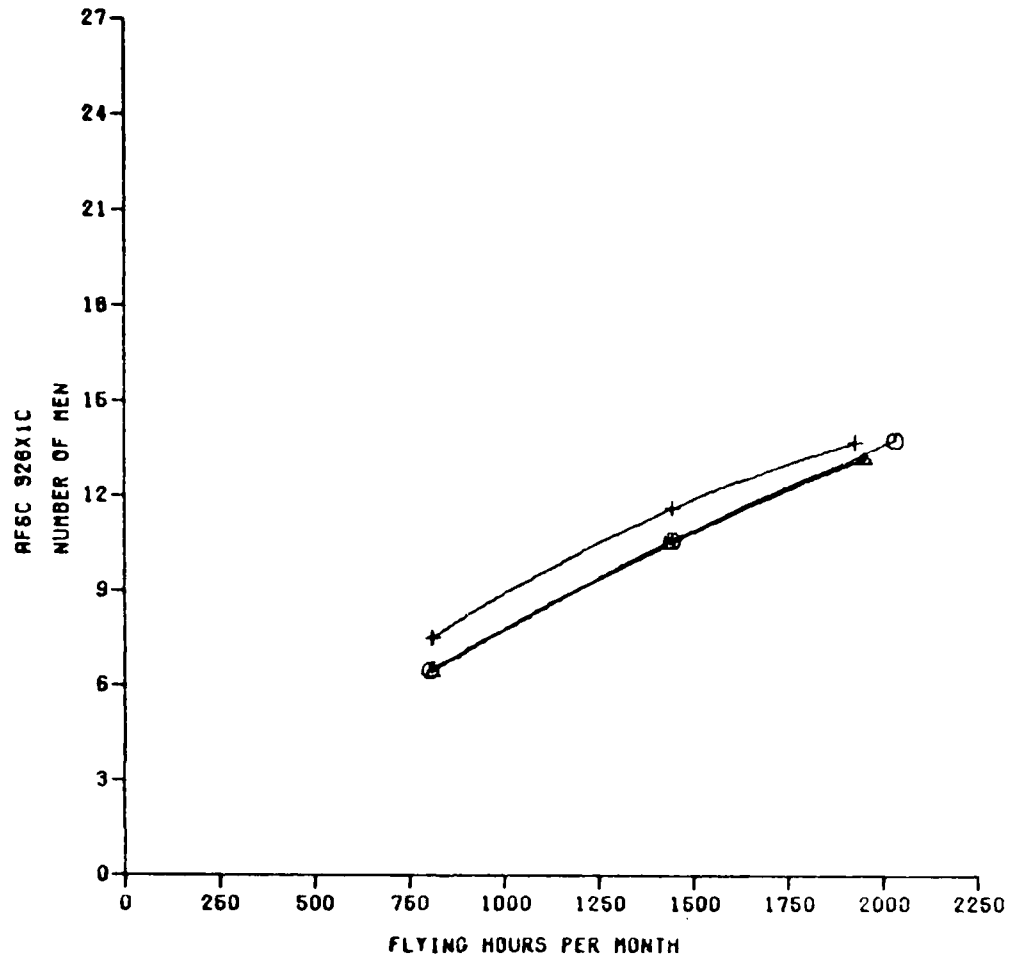
Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	6 (6-7)	11 (10-11)	14 (13-14)
Δ - Constrained Parts/ Unconstrained ATS	7 (6-7)	11 (10-11)	14 (14-15)
+ - Constrained Parts/ Constrained ATS	7 (6-7)	10 (10-11)	14 (13-15)

Figure 28. AFSC 326X2C (Communications/Navigations/Electronic Counter Measures) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
O - Unconstrained Parts/ Unconstrained ATS	13 (13-14)	26 (24-27)	34 (33-36)
Δ - Constrained Parts/ Unconstrained ATS	14 (13-15)	25 (23-27)	35 (34-37)
+ - Constrained Parts/ Constrained ATS	16 (15-16)	25 (25-26)	33 (31-34)

Figure 29. AFSC 326X1D (Automatic Test Station) Direct Manning



Constraint Type	Scheduled Sortie Rate		
	.43	.74	1.0
0 - Unconstrained Parts/ Unconstrained ATS	7 (7-8)	10 (9-11)	14 (13-14)
Δ - Constrained Parts/ Unconstrained ATS	6 (6-7)	11 (9-12)	13 (12-13)
+ - Constrained Parts/ Constrained ATS	8 (7-8)	11 (10-11)	14 (12-16)

Figure 30. AFSC 326X1C (Manual Test Station) Direct Manning

Manning Document. The authors used the Moody Manpower Program to develop a complete basic manning document for the maintenance organization depicted in Figure 6 of Chapter III. Additionally, the program was used to determine the total maintenance manning requirements for each constraint type and scheduled sortie rate. The Moody Manpower Program considers each AFSC's minimum crew manning during the development of total manning requirements. If direct manning estimates are below the respective minimum crew manning, the program uses the minimum crew manning to determine total manning requirements. Since the LCOM networks define minimum crew requirements for each maintenance task, AFSC minimum crew manning remains constant for each constraint type and scheduled sortie rate. Table IX depicts the minimum crew manning for each AFSC. Figure 31 indicates the sensitivity of the F-15 TFTW's total manning requirements to constraint type and scheduled sortie rate. Figure 32 illustrates the basic manning document for unconstrained parts/ATS at a .74 scheduled sortie rate.

Table IX
AFSC Minimum Crew Manning

AFSC	Work Description	Minimum Crew Manning
431X1	Flight Line Crew Chief	31
431X1	Phase Inspection	24
531X3	Structural Repair	10
426X2	Jet Engine	48
423X3	Fuel Systems	10
423X0	Electrical Systems	10
423X4	Pneudraulics	10
423X1	Environmental Systems	10
423X2	Egress Systems	10
326X2B	Automatic Flight Control/Instruments	10
326X2A	Inertial Navigation System/Weapon Control	10
326X2C	Communications/Navigations/Electronic Counter Measures	10
326X1D	Automatic Test Station	10
326X1C	Manual Test Station	10

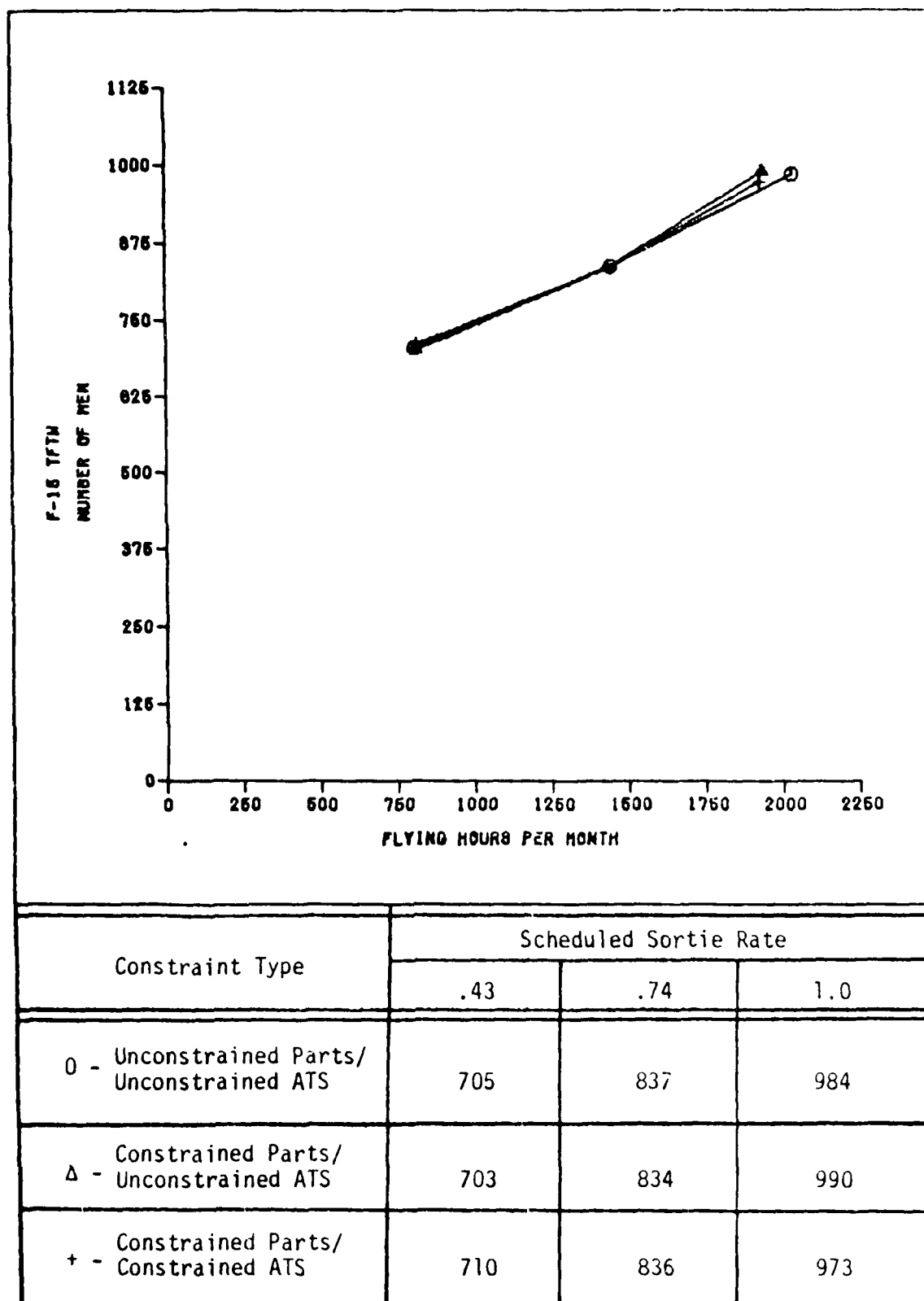


Figure 31. F-15 TFW Total Manning Requirements

F15 TFW MANNING DOCUMENT

CHIEF OF MAINTENANCE

F/C	DESC.	OSC	AFSC	GRADE	RQMT
210000	CHIEF OF MAINT	JN	4095	COL	1
210010	CHIEF OF MAINT	JN	4016	LTC	1
210030	CHIEF OF MAINT	JN	43191	CMS	1
210000	CHIEF OF MAINT	JN	43171C	MSG	1
210000	CHIEF OF MAINT	JN	70450	CIV	1
					6
210000	CHIEF OF MAINT	JND	70270	MSG	1
210000	CHIEF OF MAINT	JND	70250	SSG	2
210000	CHIEF OF MAINT	JND	70250	SGT	3
210000	CHIEF OF MAINT	JND	70230	AIC	1
					7
210010	CHIEF OF MAINT ENG MGT	JNB	75193	SMS	1
210000	CHIEF OF MAINT ENG MGT	JNB	75172	MSG	1
210000	CHIEF OF MAINT ENG MGT	JNB	75132	SSG	1
					3
210000	CHIEF OF MAINT PROD ANAL	JNA	39170A	MSG	1
210000	CHIEF OF MAINT PROD ANAL	JNA	39150A	SSG	1
210000	CHIEF OF MAINT PROD ANAL	JNA	39150A	SGT	1
					3
210000	QUALITY CONT ADM	JND	70250	CIV	2
					2
210000	PROGRAMS/MOBILITY	JNE	66170	MSG	2
					2
211000	QUALITY CONT ECF	JNHA	F4024	CPT	2
211000	QUALITY CONT	JNHA	43171C	MSG	1
					3
211000	QUALITY CONT I O DEST	JNHC	43151C	SSG	2
					2
211000	QUALITY CONT	JNH	4016	LTC	1
211000	QUALITY CONT	JNH	43191	SMS	1
					2

Figure 32. F-15 TFW Manning Document

AD-A156 540

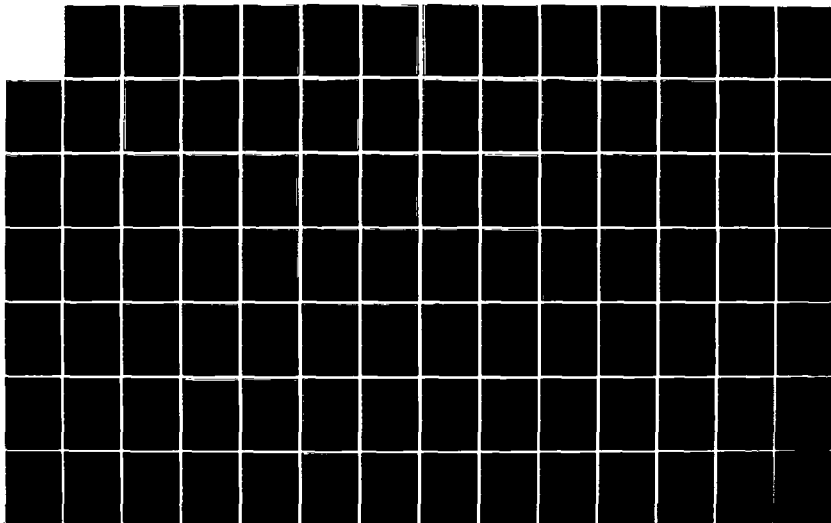
ESTIMATION OF F-15 PEACETIME MAINTENANCE MANPOWER
REQUIREMENTS USING THE (U) AIR FORCE INST OF TECH
WRIGHT-PATTESSON AFB OH SCHOOL OF ENGI

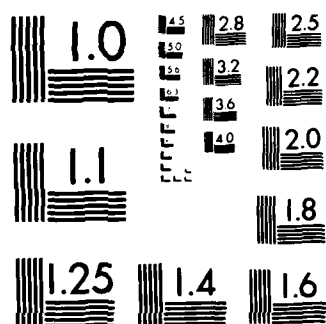
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NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

211000	QUALITY CONT	JNHB	42375	MSG	1
211000	QUALITY CONT	JNHB	42375	TSG	2
211000	QUALITY CONT	JNHB	46272	MSG	1
211000	QUALITY CONT	JNHB	46272	TSG	4
211000	QUALITY CONT	JNHB	43171C	MSG	2
211000	QUALITY CONT	JNHB	43171C	TSG	4
211000	QUALITY CONT	JNHB	43151C	SSG	1
211700	QUALITY CONT	JNHB	46270	MSG	1
211000	QUALITY CONT	JNHB	46270	TSG	1
211000	QUALITY CONT	JNHB	46170	MSG	1
211000	QUALITY CONT	JNHB	46170	TSG	1
211000	QUALITY CONT	JNHB	32672A	MSG	1
211000	QUALITY CONT	JNHB	32672A	TSG	1
211000	QUALITY CONT	JNHB	326729	TSG	1
211000	QUALITY CONT	JNHB	32672C	MSG	1
211000	QUALITY CONT	JNHB	32672C	TSG	2

25

212000	MAINT CONT	JNI	4016	LTC	1
212000	MAINT CONT	JNI	4024	CPT	1
212000	MAINT CONT	JNI	39290	CMS	1
212000	MAINT CONT	JNI	70250	SSG	1

4

212000	MAINT CONT JOB CNTL	JNIA	43191	SMS	1
212000	MAINT CONT JOB CNTL	JNIA	43171C	MSG	2
212000	MAINT CONT JOB CNTL	JNIA	43171C	TSG	6
212000	MAINT CONT JOB CNTL	JNIA	43151C	SSG	7
212000	MAINT CONT JOB CNTL	JNIA	43151C	SGT	8
212000	MAINT CONT JOB CNTL	JNIA	42355	SSG	2
212000	MAINT CONT JOB CNTL	JNIA	42355	SGT	2
212000	MAINT CONT JOB CNTL	JNIA	32672A	MSG	1
212000	MAINT CONT JOB CNTL	JNIA	32652A	SSG	1
212000	MAINT CONT JOB CNTL	JNIA	32652A	SGT	1
212000	MAINT CONT JOB CNTL	JNIA	46270	MSG	1
212000	MAINT CONT JOB CNTL	JNIA	46270	TSG	1
212000	MAINT CONT JOB CNTL	JNIA	46250	SSG	1
212000	MAINT CONT JOB CNTL	JNIA	46250	SGT	1

35

212000	MAINT CONT PLANS/SCH/002	JNIB	32672A	MSG	1
212000	MAINT CONT PLANS/SCH/002	JNIB	32672B	TSG	1
212000	MAINT CONT PLANS/SCH/002	JNIB	43171C	TSG	3
212000	MAINT CONT PLANS/SCH/002	JNIB	39230	SSG	6
212000	MAINT CONT PLANS/SCH/002	JNIB	39230	SGT	2
212000	MAINT CONT PLANS/SCH/002	JNIB	39270	MSG	2
212000	MAINT CONT PLANS/SCH/002	JNIB	39270	TSG	4
212000	MAINT CONT PLANS/SCH/002	JNIB	39290	SMS	1
212000	MAINT CONT PLANS/SCH/002	JNIB	70250	SGT	1
212000	MAINT CONT PLANS/SCH/002	JNIB	43171C	TSG	2
212000	MAINT CONT PLANS/SCH/002	JNIB	43151C	SSG	1
212000	MAINT CONT PLANS/SCH/002	JNIB	39270	MSG	1
212000	MAINT CONT PLANS/SCH/002	JNIB	39230	SSG	1

26

212000	MAINT CONT MAT CONT	JNIC	6424A	CPT	1
212000	MAINT CONT MAT CONT	JNIC	64570	MSG	1
212000	MAINT CONT MAT CONT	JNIC	70250	SGT	1

3

212000	MAINT CONT MAT CONT	JNICA	64570	TSG	4
212000	MAINT CONT MAT CONT	JNICA	64550	SSG	4
212000	MAINT CONT MAT CONT	JNICA	64550	SGT	5
212000	MAINT CONT MAT CONT	JNICA	64530	AIC	3

16

212000	MAINT CONT MAT CONT	JNICB	39270	MSG	3
212000	MAINT CONT MAT CONT	JNICB	39230	SSG	6
212000	MAINT CONT MAT CONT	JNICB	39230	SGT	6
212000	MAINT CONT MAT CONT	JNICB	39270	TSG	3

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Figure 32. F-15 TFTW Manning Document (continued)

ORGANIZA. MAINTENANCE SQUADRON

POS	DESC.	OSC	AFSC	GRADE	RQMT.
223000	ORGANIZ. MAINT SQ	AA	4016	MAJ	1
220000	ORGANIZ. MAINT SQ	AA	44016	LTC	1
220000	ORGANIZ. MAINT SQ	AA	70250	SSG	1
220000	ORGANIZ. MAINT SQ	AA	70233	AIC	1
220000	ORGANIZ. MAINT SQ	AA	43191	CMS	1
					5
220000	UNIT ADMIN	AU	7034	CPT	1
220000	UNIT ADMIN	AU	70250	SSG	1
220000	UNIT ADMIN	AU	70230	AIC	2
220000	UNIT ADMIN	AU	10090	MSG	1
					5
221000	FLIGHT LINE SUPV	MLM	4024	CPT	1
221000	FLIGHT LINE SUPV	MLM	70230	AIC	1
221000	FLIGHT LINE SUPV	MLM	4024	LT	1
221000	FLIGHT LINE SJPV	MLM	43191	SMS	1
221000	FLIGHT LINE CMF	MLM	431710	MSG	1
221000	FLIGHT LINE CMF	MLM	431710	MSG	1
221000	FLIGHT LINE CMF	MLM	431710	MSG	1
221000	FLIGHT LINE CMF	MLM	431710	MSG	4
221000	FLIGHT LINE CMF	MLM	431710	TSG	20
221000	FLIGHT LINE EXPEDITOR	MLM	431710	TSG	1
221000	FLIGHT LINE CMF	MLM	431510	SSG	1
221000	FLIGHT LINE INSPECTOR	MLM	43191	SMS	1
221000	FLIGHT LINE GO SUPT EDP	MLM	431710	MSG	1
221000	FLIGHT LINE BENCH STOCK	MLM	431510	SSG	1
221000	FLIGHT LINE BENCH STOCK	MLM	431510	SGT	1
221000	FLIGHT LINE 700 EQUIP	MLM	431710	TSG	1
221000	FLIGHT LINE 700 EQUIP	MLM	431510	SSG	1
221000	FLIGHT LINE 700 EQUIP	MLM	431510	SGT	1
221000	FLIGHT LINE 700 EQUIP	MLM	431310	AIC	1
221000	FLIGHT LINE	MLM	43191	SMS	1
221000	FLIGHT LINE	MLM	43191	MSG	1
221000	FLIGHT LINE	MLM	431710	MSG	1
221000	FLIGHT LINE	MLM	431710	TSG	1
221000	FLIGHT LINE	MLM	431710	SSG	5
221000	FLIGHT LINE	MLM	431510	SSG	19
221000	FLIGHT LINE	MLM	431510	SGT	41
221000	FLIGHT LINE	MLM	431510	AIC	10
221000	FLIGHT LINE	MLM	431310	AIC	41
					176
222000	PHASE	MLI	431	710MSG	1
222000	PHASE	MLI	431	710TSG	1
222000	PHASE	MLI	431	710SSG	1
222000	PHASE	MLI	431	510SSG	4
222000	PHASE	MLI	431	510SGT	8
222000	PHASE	MLI	431	510AIC	2
222000	PHASE	MLI	431	310AIC	7
					24

Figure 32. F-15 TFTW Manning Document (continued)

FIELD MAINTENANCE SQUADRON

F/C	DESC.	OSC	AFSC	GRADE	RQMT
230000	FIELD MAINT SQ	AA	4015	MAJ	1
230000	FIELD MAINT SQ	AA	44015	LTC	1
230000	FIELD MAINT SQ	AA	70250	SSG	1
230000	FIELD MAINT SQ	AA	42692	CMS	1
230000	FIELD MAINT SQ	AA	70230	A1C	1
					5
230000	UNIT ADMIN	AU	7034	CPT	1
230000	UNIT ADMIN	AU	70250	SSG	1
230000	UNIT ADMIN	AU	70230	A1C	1
230000	UNIT ADMIN	AU	10090	MSG	1
					4
231000	FABRICATION	MKM	53195	SMS	1
					1
231100	MACHINE SHOP	MKHA	53150	SSG	2
231100	MACHINE SHOP	MKHA	53150	SGT	2
231100	MACHINE SHOP	MKHA	53150	A1C	1
231100	MACHINE SHOP	MKHA	53130	A1C	1
					6
231200	METAL PROCESSING	MKHB	53151	SSG	2
231200	METAL PROCESSING	MKHB	53151	SGT	2
231200	METAL PROCESSING	MKHB	53131	A1C	2
					6
231300	STRUT REPAIR	MKHC	53173	SSG	1
231300	STRUT REPAIR	MKHC	53153	SSG	2
231300	STRUT REPAIR	MKHC	53153	SGT	5
231300	STRUT REPAIR	MKHC	53153	A1C	1
231300	STRUT REPAIR	MKHC	53133	A1C	5
					14
231400	CORROSION CONTROL	MKHF	53154	SSG	1
231400	CORROSION CONTROL	MKHF	53154	SGT	2
231400	CORROSION CONTROL	MKHF	53154	A1C	3
231400	CORROSION CONTROL	MKHF	53134	A1C	2
					8
231500	SURVIVAL EQUIPMENT	MKHE	50271	TSG	1
231500	SURVIVAL EQUIPMENT	MKHE	50251	SSG	2
231500	SURVIVAL EQUIPMENT	MKHE	50251	SGT	2
231500	SURVIVAL EQUIPMENT	MKHE	50231	A1C	2
231500	SURVIVAL EQUIPMENT	MKHE	50250	SSG	1
231500	SURVIVAL EQUIPMENT	MKHE	50250	SGT	1
231500	SURVIVAL EQUIPMENT	MKHE	50230	A1C	1
					10
231700	NON-DESTRUCTIVE INSPECTION	MKMG	53175	CIV	1
231700	NON-DESTRUCTIVE INSPECTION	MKMG	53175	TSG	1
231700	NON-DESTRUCTIVE INSPECTION	MKMG	53155	SSG	2
231700	NON-DESTRUCTIVE INSPECTION	MKMG	53155	SGT	2
231700	NON-DESTRUCTIVE INSPECTION	MKMG	53135	A1C	2
					8
232000	PROPULSION	MKI	4024	LT	1
232000	PROPULSION	MKI	45292	CMS	1
232000	REACH STOCK/TOOL RM	MKI	42672	TSG	1
232000	REACH STOCK/TOOL RM	MKI	42652	SSG	1
232000	REACH STOCK/TOOL RM	MKI	42652	SGT	1
232000	REACH STOCK/TOOL RM	MKI	42632	A1C	1
					6

Figure 32. F-15 TFTW Manning Document (continued)

232300	JET ENGINE	MKIC	42672	MSG	2
232300	JET ENGINE	MKIC	42672	TSG	2
232300	JET ENGINE	MKIC	42672	SSG	4
232300	JET ENGINE	MKIC	42652	SSG	16
232300	JET ENGINE	MKIC	42652	SGT	34
232300	JET ENGINE	MKIC	42652	AIC	8
232300	JET ENGINE	MKIC	42632	AIC	35
					101
233000	AEROSPACE SYSTEMS	MKJ	4024	LT	1
233000	AEROSPACE SYSTEMS	MKJ	70250	SGT	1
233000	AEROSPACE SYSTEMS	MKJ	42396	SMS	1
					3
233100	REPAIR AND RECLAMATION	MKJA	431710	MSG	2
233100	REPAIR AND RECLAMATION	MKJA	431710	TSG	3
233100	REPAIR AND RECLAMATION	MKJA	431510	SSG	6
233100	REPAIR AND RECLAMATION	MKJA	431510	SGT	6
233100	REPAIR AND RECLAMATION	MKJA	431310	AIC	5
					22
233200	FUEL SYSTEMS	MKJB	42373	SSG	1
233200	FUEL SYSTEMS	MKJB	42353	SSG	2
233200	FUEL SYSTEMS	MKJB	42353	SGT	5
233200	FUEL SYSTEMS	MKJB	42353	AIC	1
233200	FUEL SYSTEMS	MKJB	42333	AIC	5
					14
233300	ELECTRICAL SYSTEMS	MKJC	42370	SSG	1
233300	ELECTRICAL SYSTEMS	MKJC	42350	SSG	2
233300	ELECTRICAL SYSTEMS	MKJC	42350	SGT	1
233300	ELECTRICAL SYSTEMS	MKJC	42350	AIC	1
233300	ELECTRICAL SYSTEMS	MKJC	42330	AIC	3
					10
233400	PNEUMATICS	MKJD	42374	SSG	1
233400	PNEUMATICS	MKJD	42354	SSG	3
233400	PNEUMATICS	MKJD	42354	SGT	6
233400	PNEUMATICS	MKJD	42354	AIC	1
233400	PNEUMATICS	MKJD	42334	AIC	7
					18
233600	ENVIRONMENTAL SYSTEMS	MKJF	42351	SSG	2
233600	ENVIRONMENTAL SYSTEMS	MKJF	42361	SGT	1
233600	ENVIRONMENTAL SYSTEMS	MKJF	42351	AIC	1
233600	ENVIRONMENTAL SYSTEMS	MKJF	42331	AIC	4
					10
233900	EGRESS SYSTEMS	MKJI	42352	SSG	2
233900	EGRESS SYSTEMS	MKJI	42352	SGT	3
233900	EGRESS SYSTEMS	MKJI	42352	AIC	1
233900	EGRESS SYSTEMS	MKJI	42332	AIC	4
					10
234000	AEROSPACE GROUND EQUIPMENT	MKK	42375	MSG	2
234000	AEROSPACE GROUND EQUIPMENT	MKK	42375	TSG	2
234000	AEROSPACE GROUND EQUIPMENT	MKK	42375	SSG	4
234000	AEROSPACE GROUND EQUIPMENT	MKK	42355	SSG	15
234000	AEROSPACE GROUND EQUIPMENT	MKK	42355	SGT	33
234000	AEROSPACE GROUND EQUIPMENT	MKK	42355	AIC	8
234000	AEROSPACE GROUND EQUIPMENT	MKK	42335	AIC	34
					98

Figure 32. F-15 TFTW Manning Document (continued)

AVIONICS COMMAND SQUADRON

F/C	DESC.	OSC	AFSC	GRADE	RQMT
240000	AVIONICS SQ	AA	44096	LTC	1
240000	AVIONICS SQ	AA	4016	MAJ	1
240000	AVIONICS SQ	AA	32090	CMS	1
240000	AVIONICS SQ	AA	70250	SSG	1
240000	AVIONICS SQ	AA	70230	AIC	1
240000	AVIONICS SQ	AA	4024	CPT	1
					6
240000	UNIT ADMIN	AU	7034	CPT	1
240000	UNIT ADMIN	AU	10090	MSG	1
240000	UNIT ADMIN	AU	70250	SSG	1
240000	UNIT ADMIN	AU	70230	AIC	1
					4
243000	ELECTRONICS	HJO	4024	CPT	1
243000	ELECTRONICS	HJO	32672C	MSG	1
					2
243300	AUT FLT CON & INST SUPV	HJQ	32692	SMS	1
243300	AUT FLT CON & INST	HJQ	32652B	SSG	2
243300	AUT FLT CON & INST	HJQ	32652B	SGT	1
243300	AUT FLT CON & INST	HJQ	32652B	AIC	1
243300	AUT FLT CON & INST	HJQ	32632M	AIC	4
					11
243600	WEAP CON & INER NV SJPV	HJOA	32692	SMS	1
243600	WEAP CON & INER NV	HJOA	32672A	MSG	1
243600	WEAP CON & INER NV	HJOA	32672A	TSG	1
243600	WEAP CON & INER NV	HJOA	32672A	SSG	1
243600	WEAP CON & INER NV	HJOA	32652A	SSG	3
243600	WEAP CON & INER NV	HJOA	32652A	SGT	7
243600	WEAP CON & INER NV	HJOA	32652A	AIC	1
243600	WEAP CON & INER NV	HJOA	32632A	AIC	6
					21
243700	COMM NV & PEN AIDS	HJOC	32652C	SSG	1
243700	COMM NV & PEN AIDS	HJOC	32652C	SGT	3
243700	COMM NV & PEN AIDS	HJOC	32652C	AIC	1
243700	COMM NV & PEN AIDS	HJOC	32632C	AIC	5
					10
246000	AVN SHOP MAINT	HJP	4024	CPT	1
246000	AVN SHOP MAINT	HJP	32692	MSG	1
					2

Figure 32. F-15 TFTW Manning Document (continued)

246100	AVN AGE	HJPA	326700	MSG	1
246100	AVN AGE	HJPA	326700	TSG	1
246100	AVN AGE	HJPA	326700	SSG	1
246100	AVN AGE	HJPA	326500	SSG	4
246100	AVN AGE	HJPA	326500	SGT	9
246100	AVN AGE	HJPA	326500	A1C	2
246100	AVN AGE	HJPA	326300	A1C	8

					26
246200	AUTO TST STN SUPV	HJPB	32692	SMS	1
246200	AUTO TST STN	HJPB	326710	MSG	1
246200	AUTO TST STN	HJPB	326710	TSG	1
246200	AUTO TST STN	HJPB	326710	SSG	1
246200	AUTO TST STN	HJPB	326510	SSG	4
246200	AUTO TST STN	HJPB	326510	SGT	6
246200	AUTO TST STN	HJPB	326510	A1C	2
246200	AUTO TST STN	HJPB	326310	A1C	7

					26
246300	MAN TST STN	HJPC	326510	SSG	1
246300	MAN TST STN	HJPC	326510	SGT	1
246300	MAN TST STN	HJPC	326510	A1C	1
246300	MAN TST STN	HJPC	326310	A1C	1

					10

SUMMARY OF WHOLE WING

COL	1
LTC	6
MAJ	3
CPT	11
LT	3

TOTAL	24

GIV	4

OMS	6
SMS	12
MSG	5
MSG	46
TSG	89
SSG	23
SSG	146
SGT	227
A1C	47
A1C	200

TOTAL	590

Figure 32. F-15 TFTW Manning Document (continued)

Summary

This chapter contains a discussion of the analysis and results of the F-15 TFTW LCOM simulation. The analysis section contains a graphical and statistical interpretation of the simulation's steady state conditions and autocorrelation coefficients. The results consist of direct manning estimates for each AFSC listed in Table I, their respective 95 percent confidence intervals, the sensitivity of these estimates to variations in parts and ATS, and a USAF basic manning document for the F-15 TFTW. The Conclusion and Recommendation Chapter summarizes the results and makes recommendations concerning the thesis findings.

VI. CONCLUSIONS AND RECOMMENDATIONS

As stated in Chapter I, this thesis had three major objectives: first, use LCOM to estimate the maintenance manpower requirements for a 72 U.E. F-15 TFTW; second, construct statistical confidence intervals for these manpower estimates; third, investigate the sensitivity of maintenance manpower requirements to variations in the availability of aircraft spare parts and support equipment. The authors accomplished these objectives and presented their analysis and results in Chapter V. Figures 17 through 30 illustrate each AFSC's direct manning requirements, confidence intervals, and sensitivity to constraint type and scheduled sortie rate. Figure 31 depicts the total manning requirements for a 72 U.E. F-15 TFTW and the sensitivity of these requirements to constraint type and scheduled sortie rate. Finally, Figure 32 contains a basic manning document for a 72 U.E. F-15 TFTW based on *unconstrained parts/ATS* and a .74 scheduled sortie rate.

Conclusions

This thesis has allowed the authors to develop several noteworthy conclusions concerning LCOM manpower estimation, in general, and the peacetime model used in this study. They feel that these developments will enable greater statistical accuracy in LCOM manpower estimates and, therefore, further enhance LCOM's position in the manpower community.

Steady State. In this study, the authors developed a more efficient procedure for determining steady state conditions in an LCOM computer simulation. The procedure involved graphical and statistical analysis of daily and weekly AFSC manhour totals as described in Chapters IV and V.

Using this technique, the authors found that the F-15 TFTW model used in this thesis exhibited steady state conditions throughout the 98 day simulation period. In those isolated instances found in Table IV of Chapter V where individual AFSC's indicated transient behavior, this behavior disappeared after the first or second week into the simulation period. As a result, output data for the entire simulation period was used to estimate maintenance manpower requirements. When contrasted with the more common procedure of discarding the first 30 days in an LCOM simulation (Ref 33:114-115), the procedure used in this study more efficiently utilizes computer run time and allows equally accurate results. When one considers that this study required more than 25 computer runs, the overall savings in computer time is significant.

Autocorrelation. The study used autocorrelation analysis to develop 95 percent statistical confidence intervals for AFSC direct manning estimates. The procedure allowed the authors to estimate maintenance manpower requirements with a very high degree of statistical accuracy. Based on this procedure, all AFSC's except two indicated a five percent or less variability in direct manning estimates; AFSC's 426X2 (Jet Engine) and 423X3 (Fuel Systems) indicated an eight percent and nine percent, respectively, variability in direct manning estimates. Such accuracy lends confidence to the LCOM manpower estimation process.

Model Validity. In order to verify these procedures, the authors compared the LCOM direct manning estimates and corresponding statistical confidence intervals contained in Chapter V with estimates from three other LCOM simulation strategies. Table X illustrates this comparison using four sets of manning estimates based on unconstrained parts/ATS

Table X
Comparison of Simulation Strategies

AFSC	Simulation Strategy			
	1	2	3	4
431X1 (Flight Line Crew Chief)	124(120-128)	124	124	125
431X1 (Phase Inspection)	20(20-21)	21	20	20
531X3	14(13-14)	13	13	13
426X2	103(94-112)	97	107	97
423X3	16(14-17)	13	13	11
423X0	8(7-8)	7	7	8
423X4	17(16-19)	18	18	18
423X1	10(9-10)	9	10	8
423X2	2(2-2)	2	2	2
326X2B	10(9-10)	9	9	10
326X2A	21(21-22)	21	21	20
326X2C	11(10-11)	10	11	11
326X1D	26(24-27)	25	25	24
326X1C	10(9-11)	10	11	11
ASR	.697	.694	.708	.692
<p>Strategy 1 - 98 day simulation with 5 day flying schedule and 7 day maintenance schedule.</p> <p>Strategy 2 - 196 day simulation with 5 day flying schedule and 7 day maintenance schedule.</p> <p>Strategy 3 - 100 day simulation with 5 day flying schedule and 5 day maintenance schedule.</p> <p>Strategy 4 - 98 day simulation with 5 day flying schedule, 7 day maintenance schedule, and different random number seeds.</p>				

and a .74 scheduled sortie rate. In this table, Strategy 1 reflects the methodology and results contained in Chapters IV and V, respectively.

The direct manning estimates from Strategy 2 were obtained using methodology similar to Strategy 1 except the simulation period consisted of 196 days and the manning estimates were based solely on the last 98 simulated days. The reason for doubling the simulation period was to determine if the authors' assertions concerning the peacetime model's steady state behavior were, in fact, correct. Since the direct manning estimates obtained from Strategy 2 were similar to the corresponding Strategy 1 estimates, the authors concluded that longer computer run times did not significantly affect the F-15 TFTW direct manning estimates. This comparison confirmed their steady state analysis of the peacetime model.

In Strategy 3, the direct manning estimates were based on a 100 day simulation period with a concurrent five day flying and maintenance work week. Such a scenario eliminated weekends from the maintenance schedule and eliminated the opportunity to perform backlogged maintenance work on nonflying days. During the computation of direct manning under this strategy, 20.99 work days per month replaced 30.44 work days per month in Equation (3) of Chapter IV (Ref 2:Chap. 6, p. 29). Although the manning estimates from this strategy were similar to those of Strategy 1, the authors concluded that higher scheduled sortie rates, and/or more severe parts/ATS constraints would cause bottlenecks in the maintenance work flow and produce erratic day-to-day manhours used data. Such data would cause transient behavior at the beginning of the simulation period and would require longer computer run times in order to achieve steady state conditions. Since actual peacetime operations routinely schedule flying

and maintenance activity Monday through Friday and permit weekend maintenance activity to alleviate backlogged work, a scenario based on a five day flying and seven day maintenance work week is a logical simulation strategy for peacetime LCOM studies. Such a strategy reflects peacetime operations in that maintenance manpower only works on weekends when there exists a work demand and permits efficient LCOM estimation of peacetime maintenance manpower over a wide range of flying activity levels and aircraft part/ATS constraints.

The direct manning estimates from Strategy 4 were obtained using methodology identical to Strategy 1 and different random number seeds in the LCOM main program. The change in random number seeds created an independent replication of direct manning estimates; the slight differences in AFSC manning estimates between Strategies 1 and 4 are a normal occurrence in replicated data. At the same time, this small variability in AFSC direct manning between the two replications supported the internal validity of the F-15 TFTW model used in this study and reinforced the authors' confidence in the F-15 peacetime model (Ref 10:204).

It should be noted that the AFSC 423X3 (Fuel Systems) direct manning estimate in Strategies 2, 3, and 4 did not fall within the respective Strategy 1 confidence interval. Additionally, the Strategy 4 estimates for AFSC's 423X1 (Environmental Systems) and 326X2A (Inertial Navigation System/Weapon Control) did not lie within the corresponding Strategy 1 confidence intervals. The authors found these deviations interesting but not disconcerting. The authors expected isolated deviations in direct manning estimates for two reasons: first, when direct manning estimates are rounded to integer values in accordance with AFM 25-5 standards, two estimates such as 8.61 and 8.62 become eight and nine,

respectively; second, some variability in replicated data is to be expected. The comparison of simulation Strategy 1 with Strategies 2, 3, and 4 was intended to illustrate, in a general sense, that the authors methodology was valid. The authors could not completely explain the lower estimates for AFSC 423X3 in Strategies 2, 3, and 4. However, they do not feel that the deviation of these estimates from the Strategy 1 estimates was reason to question the overall validity of Strategy 1. If there had existed consistent deviations among a majority of the AFSC estimates in Strategies 2, 3, and 4 when compared to Strategy 1, the authors would have questioned the validity of their methodology. However, in general, just the opposite is true. The majority of estimates in Strategies 2, 3, and 4 agreed closely with the results of Strategy 1. Thus, the authors believe the comparison of simulation strategies supports, in a general sense, the validity of their methodology.

Manning Sensitivity. It is apparent from Figure 31 in Chapter V that F-15 TFTW total manning requirements were relatively insensitive to the constrained parts and ATS contained in Appendix E. Although total manning requirements indicated a slight sensitivity to parts and ATS constraints at the 1.0 scheduled sortie rate, these constraints had little effect on total manning requirements at the lower scheduled flying activity levels. The authors concluded that at and below a .74 scheduled sortie rate the spare part and ATS constraints contained in Appendix E were sufficient to support the daily flying activity.

At the 1.0 scheduled sortie rate, the spare parts and ATS constraints could not support the daily flying activity. As a result, the constrained parts simulation required additional manpower to repair and/or cannibalize aircraft parts while the constrained parts/ATS simulation

required less manpower because a limited number of men could perform ATS functions. As Table VIII in Chapter V indicates, these constraints also had a noticeable effect on accomplished sortie rate (ASR) and flying hours per month (FHPM). The authors concluded that more severe part and ATS constraints would have similar effects on the lower flying activity levels.

Individual AFSC manning showed no particular trend in sensitivity to constraint type. The AFSC 423X3 (Fuel Systems) in Figure 21 was the most sensitive estimate while AFSC 431X1 (Flight Line Crew Chief) displayed the least sensitivity. In most cases, the AFSC direct manning confidence intervals for the .43 and .74 scheduled sortie rates contained two or more constraint type manning estimates. The authors, therefore, concluded that, since the modeled F-15 TFTW conducts its routine flying training in the .43 and .74 scheduled sortie rate range, direct manning sensitivity to aircraft spare part and ATS constraints contained in Appendix E was statistically insignificant.

Recommendations

As a result of this study, the authors have gained an indepth understanding of the LCOM manpower estimation process. They believe this experience qualifies them to make several recommendations concerning future LCOM studies.

The authors recommend that the LCOM postprocessor program be modified to provide time series plots of AFSC manhours used. These plots would be similar to the graphs illustrated in Figures 10 through 13 in Chapter V. This capability would allow LCOM users to efficiently determine the steady state behavior of their simulation model. Tetmeyer

(Ref 31) agreed that such a capability would benefit the LCOM community; Drake (Ref 29) confirmed the feasibility of such a modification. The authors, therefore, recommend that the new version of LCOM (LCOM II) incorporate this feature.

It is recommended that LCOM peacetime studies use a five day flying and seven day maintenance work week. This type of scenario reflects actual peacetime operations and permits efficient LCOM estimation of maintenance manpower over a wide range of flying activity levels.

Finally, the authors recommend that the LCOM community use the methodology described in Chapter IV to develop statistical confidence intervals for manning estimates. This procedure adds statistical reliability to the LCOM estimates and provides decision makers with a realistic perspective of manpower requirements.

Future Work

The accomplishment of the authors stated objectives represent the conclusion of this thesis effort. However, the authors feel that future LCOM studies should investigate the interaction of peacetime manning estimates with a wartime environment. For example, the peacetime manning estimates derived from this thesis should be incorporated into the F-15 wartime model in order to measure the effect on accomplished sortie rate and manhour utilization rate. Such an effort would realistically portray the conversion of a peacetime flying organization into a wartime operation and give the decision maker direction in determining potential operational problem areas.

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APPENDIX A

F-15 TFTW DATA BASE

F-15 TFTW DATA BASE

[illegible]

Figure A-1. LCOM Extended Form 11

2. The networks include the following coding conventions.

a. ACTION CODES:

- F - Failure Clock.
- T - Troubleshoot On-aircraft.
- X - Work to Facilitate Maintenance (Access, Preparation, etc.).
- A - Get and Hookup Aircraft Ground Equipment.
- R - Remove/Replace LRU.
- M - Repair On-aircraft.
- V - Verify Systems Works.
- W - Check and Repair In-shop.
- K - Check OK in Shop.
- N - Check and NRTS/Condemn.
- J - Aircraft Handling.
- B - Loading/Downloading.
- G - Fueling.
- H - Flightline Inspection/Service.
- P - Phase Inspection.
- C - Call Section (Reference to a sub-network).
- Q - Draw LRU from Supply.
- D - Decrement a Failure Clock.
- Z - Fly Sortie.

b. Task names for unscheduled maintenance use the appropriate LRU work unit code (WUC). Task names for general aircraft servicing and support tasks are mnemonic abbreviations of the task description. For example, the task of reloading the gun is named LDGUN, and the task of servicing liquid oxygen is named LOXSV.

c. LCOM SELECTION MODES:

- A - Non-Mutually Exclusive Probability.
- C - Call Section Reference to a Sub-network.
- D - Task Done in Indicated Order.
- E - Mutually Exclusive Probability.
- F - Task Done if Indicated Failure Occurs.
- G - Relative Probability, Non-Mutually Exclusive.
- H - Task Not Done if Indicated Failure Occurs.
- I - Task Done Only if Cannibalization is Required.
- X - Task Done When Failure Occurs in Subsequent Tasks.
- S - Sortie (Externally Scheduled).

3. Task resource names are the Air Force Specialty Codes (AFSC's) of maintenance personnel, or mnemonic abbreviations for ground support equipment. For example, LXCART indicates a liquid oxygen service cart, and D60 indicates an M32-60 Ground Power Unit. The fourth (skill level) digit of the Air Force Specialty Code is replaced by an X, except in cases where a further shredout is necessary. Table A-I depicts each AFSC whose manpower was estimated by LCOM, the corresponding LCOM shredout, and the work description.

Table A-I

LCOM AFSC Shredout Used in F-15 Data Base

AFSC	LCOM Shredout	Work Description
326X1D	326A1	Automatic Test Station
326X2A	326A2	Inertial Navigation System/Weapon Control
326X1C	326B1	Manual Test Station
326X2B	326B2	Automatic Flight Control/Instruments
326X2C	326C2	Communications/Navigation/Electronic Counter Measures
423X0	423X0	Electrical Systems
423X1	422X1	Environmental Systems
423X2	422X2	Egress Systems
423X3	424X0	Fuel Systems
423X4	421X2	Pneudraulics
426X2	432X0	Jet Engine Shop/Jet Engine Flight Line
	432T0	Jet Engine Test Cell
431X1	431X1	Flight Line Crew Chief
	431P1	Phase Inspection
531X3	531X3	Structural Repair

JGP151.1275	4.11	95	09 1 0.1 17	MAIN NETWORKS FOR F15 TESTW OPERATION	ORASE	1
				THIS IS AN UPDATE OF THE F15 STUDY	ORASE	2
				ACCOMPLISHED OCTOBER 1975. THE	ORASE	3
				CLOCKS HAVE BEEN CHANGED TO REFLECT	ORASE	4
				ACTUAL LUXE AFS DATE FROM THE PERIOD	ORASE	5
				SEP 75 THRU FEB 76. THE PHASE AND	ORASE	6
				ENGINE NETWORKS HAVE BEEN CHANGED	ORASE	7
				DRAMATICALLY. THE PHASE A-DOUCE TAD	ORASE	8
				AND AFLO NO LONGER SUPPORT THE NEW	ORASE	9
				24 HOUR PHASE INSPECTION THAT WAS	ORASE	10
				SUGGESTED BY STGT JOUNG. THE ENGINE HOARE	ORASE	11
				HAD TO BE REINFORCED TO AFFECT MUI	ORASE	12
				ALL NETWORK CHANGES WERE ACCOMPLISHED	ORASE	13
				UNDER THE DIRECTION OF A TAC REF-EDN-	ORASE	14
				ATIVE AND ALL SIMULATION WILL BE CONE	ORASE	15
				AS AN AFIT THIS TOPIC.	ORASE	16
				PLACELIGHT DUMMY SORTIE	ORASE	17
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	18
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	19
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	20
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	21
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	22
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	23
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	24
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	25
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	26
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	27
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	28
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	29
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	30
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	31
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	32
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	33
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	34
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	35
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	36
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	37
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	38
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	39
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	40
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	41
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	42
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	43
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	44
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	45
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	46
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	47
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	48
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	49
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	50
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	51
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	52
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	53
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	54
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	55
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	56
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	57
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	58
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	59
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	60
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	61
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	62
JGP151.1275	4.11	95	09 1 0.1 17		ORASE	63

AA19	CALLS: AA19	C	00010 31	DBASE	64
AA19	CLGUMH	C	00010 31	DBASE	65
AA19		4	00010 31 AIR-AIR TNG TURN TO TURN	DBASE	66
AA19	HLUNCH AA19	C	00010 31	DBASE	67
AA19	HSTRT2 AA19	C	00010 31	DBASE	68
AA19	OCENT1 AA19	C	00010 31	DBASE	69
AA19	DALE2 AA19	C	00010 31	DBASE	70
AA19	CALUK2 AA19	C	00010 31	DBASE	71
AA19	CALLUM AA19	C	00010 31	DBASE	72
AA19	CALLS: AA19	C	00010 31	DBASE	73
AA19	JTAXI AA19	C	00010 31	DBASE	74
AA19	HEGEG2 AA19	C	00010 31	DBASE	75
AA19	ZL... AA19	S	00010 11	DBASE	76
AA19	HEORTM AA19	C	00010 31	DBASE	77
AA19	HTAXI AA19	C	00010 31	DBASE	78
AA19	OCENT2 AA19	C	00010 31	DBASE	79
AA19	OCENT5 AA19	C	00010 31	DBASE	80
AA19	DALE2 AA19	C	00010 31	DBASE	81
AA19	HTHPU1 AA19	C	00010 31	DBASE	82
AA19	HTHPU2 AA19	C	00010 31	DBASE	83
AA19	DALE2 AA19	C	00010 31	DBASE	84
AA19	CALUK2 AA19	C	00010 31	DBASE	85
AA19	CALLS: AA19	C	00010 31	DBASE	86
AA19	CLGUMH	C	00010 31	DBASE	87
AA19		4	00010 31 AIR-AIR TNG TURN TO LAST	DBASE	88
AA19	HLUNCH AA19	C	00010 31	DBASE	89
AA19	HSTRT2 AA19	C	00010 31	DBASE	90
AA19	OCENT1 AA19	C	00010 31	DBASE	91
AA19	DALE2 AA19	C	00010 31	DBASE	92
AA19	CALUK2 AA19	C	00010 31	DBASE	93
AA19	CALLUM AA19	C	00010 31	DBASE	94
AA19	CALLS: AA19	C	00010 31	DBASE	95
AA19	JTAXI AA19	C	00010 31	DBASE	96
AA19	HEGEG2 AA19	C	00010 31	DBASE	97
AA19	ZL... AA19	S	00010 11	DBASE	98
AA19	HEORTM AA19	C	00010 31	DBASE	99
AA19	OCENT2 AA19	C	00010 31	DBASE	100
AA19	OCENT5 AA19	C	00010 31	DBASE	101
AA19	HTAXI AA19	C	00010 31	DBASE	102
AA19	DALE2 AA19	C	00010 31	DBASE	103
AA19	OCENT1 AA19	C	00010 31	DBASE	104
AA19	OCENT2 AA19	C	00010 31	DBASE	105
AA19	OCENT5 AA19	C	00010 31	DBASE	106
AA19	DALE2 AA19	C	00010 31	DBASE	107
AA19	CALUK1 AA19	C	00010 31	DBASE	108
AA19	CALLS: AA19	C	00010 31	DBASE	109
AA19	CLGUMH	C	00010 31	DBASE	110
AA19		4	00010 31 AIR-AIR FIRST TO LAST	DBASE	111
AA19	CALPRE AA19	C	00010 31	DBASE	112
AA19	OCENT1 AA19	C	00010 31	DBASE	113
AA19	HLUNCH AA19	C	00010 31	DBASE	114
AA19	HSTRT2 AA19	C	00010 31	DBASE	115
AA19	OCENT1 AA19	C	00010 31	DBASE	116
AA19	DALE2 AA19	C	00010 31	DBASE	117
AA19	CALUK2 AA19	C	00010 31	DBASE	118
AA19	CALLUM AA19	C	00010 31	DBASE	119
AA19	CALLS: AA19	C	00010 31	DBASE	120
AA19	JTAXI AA19	C	00010 31	DBASE	121
AA19	HEGEG2 AA19	C	00010 31	DBASE	122
AA19	ZL... AA19	S	00010 11	DBASE	123
AA19	HEORTM AA19	C	00010 31	DBASE	124
AA19	OCENT2 AA19	C	00010 31	DBASE	125
AA19	OCENT5 AA19	C	00010 31	DBASE	126
AA19	HTAXI AA19	C	00010 31	DBASE	127
AA19	DALE2 AA19	C	00010 31	DBASE	128
AA19	OCENT1 AA19	C	00010 31	DBASE	129

AA117	WPOST:	0	00010	31	03ASE	130	
AA117	WPOST2	0	00010	31	03ASE	131	
AA117	CALC21	AA118	0	00010	31	03ASE	132
AA118	CALC21	AA119	0	00010	31	03ASE	133
AA119	CALC21	AA120	0	00010	31	03ASE	134
AA120	CALC21		0	00010	31	03ASE	135
CONVERSION TNG MISSION FIRST TO TURN						03ASE	136
CON1	CALC22	CON2	0	00010	31	03ASE	137
CON2	CALC23	CON3	0	00010	31	03ASE	138
CON3	WST21	CON4	25	00010	31	03ASE	139
CON3	WST22	CON4	75	00010	31	03ASE	140
CON4	WST21		0	00010	31	03ASE	141
CON4	CALC22	CON5	0	00010	31	03ASE	142
CON5	CALC23	CON6	0	00010	31	03ASE	143
CON6	CALC24	CON7	0	00010	31	03ASE	144
CON7	CALC25	CON8	0	00010	31	03ASE	145
CON8	WST21	CON9	0	00010	31	03ASE	146
CON8	WST22	CON9	0	00010	31	03ASE	147
CON10	WST21	CON11	0	00010	31	03ASE	148
CON11	WST22	CON12	0	00010	31	03ASE	149
CON12	WST21	CON13	0	00010	31	03ASE	150
CON13	WST22	CON14	0	00010	31	03ASE	151
CON14	WST21		0	00010	31	03ASE	152
CON14	WST22		0	00010	31	03ASE	153
CON15	CALC21	CON16	0	00010	31	03ASE	154
CON16	CALC22	CON17	0	00010	31	03ASE	155
CON17	CALC23		0	00010	31	03ASE	156
CONVERSION TNG MISSION TURN TO LAST						03ASE	157
CON18	CALC24	CON19	0	00010	31	03ASE	158
CON19	CALC25	CON20	0	00010	31	03ASE	159
CON20	WST21	CON21	25	00010	31	03ASE	160
CON20	WST22	CON21	75	00010	31	03ASE	161
CON21	WST21		0	00010	31	03ASE	162
CON21	CALC22	CON22	0	00010	31	03ASE	163
CON22	CALC23	CON23	0	00010	31	03ASE	164
CON23	CALC24	CON24	0	00010	31	03ASE	165
CON24	CALC25	CON25	0	00010	31	03ASE	166
CON25	CALC21	CON26	0	00010	31	03ASE	167
CON26	WST21	CON27	0	00010	31	03ASE	168
CON27	WST22	CON28	0	00010	31	03ASE	169
CON28	WST21	CON29	0	00010	31	03ASE	170
CON29	WST22	CON30	0	00010	31	03ASE	171
CON30	WST21	CON31	0	00010	31	03ASE	172
CON31	WST22	CON32	0	00010	31	03ASE	173
CON32	WST21		0	00010	31	03ASE	174
CON32	WST22		0	00010	31	03ASE	175
CON33	CALC21	CON34	0	00010	31	03ASE	176
CON34	CALC22	CON35	0	00010	31	03ASE	177
CON35	CALC23		0	00010	31	03ASE	178
CONVERSION TNG MISSION TURN TO TURN						03ASE	179
CON36	CALC24	CON37	0	00010	31	03ASE	180
CON37	CALC25	CON38	25	00010	31	03ASE	181
CON37	CALC25	CON38	75	00010	31	03ASE	182
CON38	CALC21	CON39	0	00010	31	03ASE	183
CON39	CALC22	CON40	0	00010	31	03ASE	184
CON40	CALC23	CON41	0	00010	31	03ASE	185
CON41	CALC24	CON42	0	00010	31	03ASE	186
CON42	CALC25	CON43	0	00010	31	03ASE	187
CON43	WST21	CON44	0	00010	31	03ASE	188
CON44	WST22	CON45	0	00010	31	03ASE	189
CON45	WST21	CON46	0	00010	31	03ASE	190
CON46	WST22	CON47	0	00010	31	03ASE	191
CON47	WST21	CON48	0	00010	31	03ASE	192
CON48	WST22	CON49	0	00010	31	03ASE	193
CON49	WST21	CON50	0	00010	31	03ASE	194
CON50	WST22	CON51	0	00010	31	03ASE	195

PHA.16	CSPEC1	PHA.167	0	PHASE 32		0BASE	262
PHA.17	PJUM1	PHA.168	9	PHASE 32		0BASE	263
PHA.17	PQC	PHA.169	1	PHASE 32	10 29L 4431P1	0BASE	264
PHA.18	CFIX	PHA.170	0	PHASE 32		0BASE	265
PHA.19	CPAN	PHA.171	0	PHASE 32		0BASE	266
PHA.19	PTOW	PHA.172	0	PHASE 32	6 29L 5431P1	0BASE	267
PHA.20	PQDI	PHA.173	0	PHASE 32	45 29L 2531X5	0BASE	268
PHA.21	PEO	PHA.174	3	PHASE 32	21 29L 2431P1	0BASE	269
PHA.22	PJUM1	PHA.175	55	PHASE 32		0BASE	270
PHA.23	PTOW2		0	PHASE 32	5 29L 5431P1	0BASE	271
CPAN	PPAN1		0	PHASE 32	10 29L 1431P1	0BASE	272
CPAN	PPAN2		0	PHASE 32	10 29L 1431P1	0BASE	273
CPAN	PPAN3		0	PHASE 32	10 29L 1431P1	0BASE	274
CPAN	PPAN4		0	PHASE 32	10 29L 1431P1	0BASE	275
CSPEC1	CLOCK1		0	PHASE 32		0BASE	276
CSPEC1	CLUR1		0	PHASE 32		0BASE	277
CSPEC1	CLUR1		0	PHASE 32	20 29L 232632	0BASE	278
CSPEC1	CLUR1		0	PHASE 32	2 29L 232612	0BASE	279
CSPEC1	CLUR1		0	PHASE 32	20 29L 2431P1	0BASE	280
CSPEC1	CLUR1		0	PHASE 32	10 29L 1431P1	0BASE	281
CLUR1	LU11		0	PHASE 32	1 29L 2431P1	0BASE	282
CLUR1	LU12		0	PHASE 32	3 29L 2431P1	0BASE	283
CLUR1	LU11		0	PHASE 32		0BASE	284
CLUR1	LU12		0	PHASE 32		0BASE	285
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CLUR1	LU12		0	PHASE 32		0BASE	295
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CLUR1	LU12		0	PHASE 32		0BASE	303
CLUR1	LU11		0	PHASE 32		0BASE	304
CLUR1	LU12		0	PHASE 32		0BASE	305
CFIX	PFIX1		0	PHASE 32	20 29L 4431P1	0BASE	306
CFIX	PFIX2		0	PHASE 32	10 29L 2421X2	0BASE	307
CFIX	PFIX3		0	PHASE 32	30 29L 1531X3	0BASE	308
CLOCK1	LOCK1		0	PHASE 32	30 29L 1431P1	0BASE	309
CLOCK1	LOCK2		0	PHASE 32	33 29L 1431P1	0BASE	310
CLOCK1	LOCK3		0	PHASE 32		0BASE	311
CLOCK1	LOCK4		0	PHASE 32	2 29L 1431P1	0BASE	312
CLOCK1	LOCK5		0	PHASE 32		0BASE	313
CLOCK1	LOCK6		0	PHASE 32		0BASE	314
CLOCK1	LOCK7		0	PHASE 32	5 29L 1431P1	0BASE	315
CLOCK1	LOCK8		0	PHASE 32		0BASE	316
CLOCK1	LOCK9		0	PHASE 32	1 29L 1431P1	0BASE	317
CLOCK1	LOCK10		0	PHASE 32		0BASE	318
PH9011	PSAFE	PH9012	0	PHASE 32		0BASE	319
PH9012	CPAN	PH9013	0	PHASE 32		0BASE	320
PH9013	PHYDOP	PH9014	0	PHASE 32	40 29L 1431P1 2421X2	0BASE	321
PH9014	CSPEC2	PH9015	0	PHASE 32		0BASE	322
PH9015	PJUM1	PH9016	9	PHASE 32		0BASE	323
PH9016	PJC	PH9017	1	PHASE 32		0BASE	324
PH9017	CFIX	PH9018	0	PHASE 32		0BASE	325
PH9018	CPAN	PH9019	0	PHASE 32		0BASE	326
PH9019	CPAN	PH9020	0	PHASE 32		0BASE	327

PH0036 T3H0HT	0	PHASE 32	5 29L 3431X1	DBASE 328
CSPE02 BT1ST2	0	PHASE 32	17 29L 312532	DBASE 329
CSPE02 PF/CL	0	PHASE 32		DBASE 330
CSPE02 PH0002 PH0003	0	PHASE 32	11 29L 446273	DBASE 331
PH0038 SH0AP1 PH0013	0	PHASE 32	107 29L 2-02X1	DBASE 332
PH0038 PH0003	0	PHASE 32	20 29L 440273	DBASE 333
CSPE02 CL00K2	0	PHASE 32		DBASE 334
CSPE02 PH0002	0	PHASE 32	11 29L 4422Y1	DBASE 335
CSPE02 PH0022	0	PHASE 32	15 29L 1421X2	DBASE 336
CSPE02 PH0005	0	PHASE 32	11 29L 1432Y1	DBASE 337
CSPE02 CL0032	0	PHASE 32		DBASE 338
CL0032 L0031	0	PHASE 32		DBASE 339
CL0032 L0031	0	PHASE 32		DBASE 340
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CL0032 L0031	0	PHASE 32		DBASE 347
CL00K2 L00K2	0	PHASE 32		DBASE 348
CL00K2 L00K2	0	PHASE 32		DBASE 349
CL00K2 L00K2	0	PHASE 32		DBASE 350
CL00K2 L00K2	0	PHASE 32		DBASE 351
CL00K2 L00K2	0	PHASE 32	10 29L 2431P1	DBASE 352
CL00K2 L00K2	0	PHASE 32		DBASE 353
CL00K2 L00K2	0	PHASE 32	5 29L 2431P1	DBASE 354
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 355
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 356
PH0038 PH0002 PH0003	0	PHASE 32	5 29L 1431P1 2431P1	DBASE 357
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PH0038 PH0002 PH0003	0	PHASE 32		DBASE 361
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 362
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 363
CSPE02 PH0002 PH0003	0	PHASE 32	10 29L 3-0270	DBASE 364
PH0038 PH0002 PH0003	0	PHASE 32	10 29L 2-02X1	DBASE 365
PH0038 PH0002 PH0003	0	PHASE 32	10 29L 3-0270	DBASE 366
CSPE02 CL00K3	0	PHASE 32		DBASE 367
CSPE02 CL0033	0	PHASE 32		DBASE 368
CSPE02 PH0002	0	PHASE 32	30 29L 1432X0	DBASE 369
CSPE02 PH0002 PH0003	0	PHASE 32		DBASE 370
PH0038 PH0002	0	PHASE 32	5 29L 1-21X0	DBASE 371
PH0038 PH0002	0	PHASE 32	20 29L 1-21X0	DBASE 372
CSPE02 PH0002	0	PHASE 32	20 29L 2-02X1	DBASE 373
CL00K3 L00K3	0	PHASE 32		DBASE 374
CL00K3 L00K3	0	PHASE 32		DBASE 375
CL00K3 L00K3	0	PHASE 32		DBASE 376
CL00K3 L00K3	0	PHASE 32	10 29L 1-21P1	DBASE 377
CL00K3 L00K3	0	PHASE 32		DBASE 378
CL00K3 L00K3	0	PHASE 32		DBASE 379
CL003 L0031	0	PHASE 32		DBASE 380
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CL003 L0031	0	PHASE 32		DBASE 390
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 391
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 392
PH0038 PH0002 PH0003	0	PHASE 32		DBASE 393

PH001- P24CAN PH0005 0	PHASE 32	10 29L 343101	ORASE 394
PH001- CSPED- PH0005 0	PHASE 32		ORASE 395
PH001- P20P3 PH0007 0	PHASE 32		ORASE 396
PH001- P20 PH0007 0	PHASE 32		ORASE 397
PH001- P21X PH0009 0	PHASE 32		ORASE 398
PH001- P21N PH0009 0	PHASE 32		ORASE 399
PH001- T04OUT 0	PHASE 32		ORASE 400
CSPED- P240X- 0	PHASE 32		ORASE 401
CSPED- P240PY 0	PHASE 32		ORASE 402
CSPED- P240- 0	PHASE 32		ORASE 403
CSPED- P240T2 0	PHASE 32		ORASE 404
CSPED- P240- 0	PHASE 32	10 29L 1422X1	ORASE 405
CSPED- P4Y0- 0	PHASE 32	10 29L 1421X2	ORASE 406
CSPED- P240- 0	PHASE 32	10 29L 1423X0	ORASE 407
CSPED- P240- 0	PHASE 32	10 29L 1432X0	ORASE 408
CLGCK- L00K- 0	PHASE 32		ORASE 409
CLGCK- L00K- 0	PHASE 32		ORASE 410
CLGCK- L00K2 0	PHASE 32		ORASE 411
CLGCK- L00K2 0	PHASE 32		ORASE 412
CLGCK- L00K2 0	PHASE 32		ORASE 413
CLGCK- L00K2 0	PHASE 32		ORASE 414
CLGCK- L00K2 0	PHASE 32		ORASE 415
CLUB- L001 0	PHASE 32		ORASE 416
CLUB- L001 0	PHASE 32		ORASE 417
CLUB- L001 0	PHASE 32		ORASE 418
CLUB- L001 0	PHASE 32		ORASE 419
CLUB- L001 0	PHASE 32		ORASE 420
CLUB- L001 0	PHASE 32		ORASE 421
CLUB- L001 0	PHASE 32		ORASE 422
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CLUB- L001 0	PHASE 32		ORASE 429
CLUB- L001 0	PHASE 32		ORASE 430
CCANPY FF PH0011 0	PHASE 32		ORASE 431
CCANPY FF PH0011 0	PHASE 32		ORASE 432
PH001- P240S1 PH0012 0	PHASE 32	35 29L 2422X2	ORASE 433
PH001- P240S2 PH0013 0	PHASE 32	30 29L 2422X2	ORASE 434
PH001- P240S3 PH0014 0	PHASE 32	5 29L 1422X2	ORASE 435
PH001- P240S7 PH0015 0	PHASE 32	35 29L 2422X2	ORASE 436
PH001- P240S8 PH0016 0	PHASE 32	35 29L 1431P1	ORASE 437
PH001- P240S9 PH0017 0	PHASE 32	15 29L 2422X2	ORASE 438
PH001- P240S10 PH0018 0	PHASE 32	15 29L 2422X2	ORASE 439
PH001- P240S11 PH0019 0	PHASE 32	2 29L 1422X2	ORASE 440
PH001- P240S12 PH0020 0	PHASE 32	15 29L 2422X2	ORASE 441
PH001- P240S13 PH0021 0	PHASE 32	10 29L 1431P1	ORASE 442
PH001- P240S14 PH0022 0	PHASE 32		ORASE 443
PH001- P240S15 PH0023 0	PHASE 32		ORASE 444
PH001- P240S16 PH0024 0	PHASE 32		ORASE 445
PH001- P240S17 PH0025 0	PHASE 32		ORASE 446
PH001- P240S18 PH0026 0	PHASE 32		ORASE 447
PH001- P240S19 PH0027 0	PHASE 32		ORASE 448
PH001- P240S20 PH0028 0	PHASE 32		ORASE 449
PH001- P240S21 PH0029 0	PHASE 32		ORASE 450
PH001- P240S22 PH0030 0	PHASE 32		ORASE 451
PH001- P240S23 PH0031 0	PHASE 32		ORASE 452
PH001- P240S24 PH0032 0	PHASE 32		ORASE 453
PH001- P240S25 PH0033 0	PHASE 32		ORASE 454
PH001- P240S26 PH0034 0	PHASE 32		ORASE 455
PH001- P240S27 PH0035 0	PHASE 32		ORASE 456
PH001- P240S28 PH0036 0	PHASE 32		ORASE 457
PH001- P240S29 PH0037 0	PHASE 32		ORASE 458
PH001- P240S30 PH0038 0	PHASE 32		ORASE 459

TIME	FROM	TO	TYPE	STATUS	DESCRIPTION	REMARKS
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0234						

A1001	F11000	A1001	F	4	11000	21		DRASE	524
A1001	F11000	A1002	F	4	11000	21	22 29L 1431X1	DRASE	527
A1001	F11000	A1002	F	4	11000	21	12 29L 1431X1	DRASE	528
A1001	F11000	A1002	F	4	11000	21	14 29L 2531X3	DRASE	529
A1001	F11000	A1002	F	4	11000	21	16 29L 1531X3	DRASE	530
A1001	F11000	A1002	F	4	11000	23		DRASE	531
S41001	L11000	I41001	G	11-57	11000	23		DRASE	532
L11000					11000	23	CTR FUSELAGE	DRASE	533
I41001	M11000		F	95	11000	23	34 29L 2531X3	DRASE	534
I41001	M11000		F	95	11000	23	15 29L 1531X3	DRASE	535
I41001	M11000		D		11000	21		DRASE	536
S41001	L11000	I41001	G	11-57	11000	23		DRASE	537
L11000					11000		ACCESS DOORS	DRASE	538
I41001	M11000		F	11	11000	23	17 29L 1531X3	DRASE	539
I41001	M11000		F	63	11000	23	34 29L 2531X3	DRASE	540
I41001	M11000		F	67	11000	23	16 29L 1531X3	DRASE	541
I41001	M11000		D		11000	21		DRASE	542
					11000		AFT FUSELAGE	DRASE	543
					11000		F-2 11K L	DRASE	544
					11000		F15 MSMA 9	DRASE	545
					11000		AFT FUSELAGE F15	DRASE	546
A1001	F11000	A1001	F	4	11000	21		DRASE	547
A1001	F11000	A1002	F	4	11000	21	28 29L 2431X1	DRASE	548
A1001	F11000	A1002	F	4	11000	21	18 29L 1431X1	DRASE	549
A1001	F11000	A1002	F	4	11000	21	10 29L 1531X3	DRASE	550
A1001	F11000	A1002	F	4	11000	21	16 29L 2531X3	DRASE	551
A1001	F11000	A1002	F	4	11000	23		DRASE	552
S41001	L11000	I41001	G	11-57	11000	23		DRASE	553
L11000					11000	23	AFT FUSELAGE	DRASE	554
I41001	M11000		F	24	11000	23	23 29L 1531X1	DRASE	555
I41001	M11000		F	67	11000	23	25 29L 1531X3	DRASE	556
I41001	M11000		F	65	11000	23	16 29L 1531X1	DRASE	557
I41001	M11000		D		11000	21		DRASE	558
S41001	L11000	I41001	G	11-57	11000	23		DRASE	559
L11000					11000		ACCESS DOORS	DRASE	560
I41001	M11000		D		11000	23	19 29L 2531X3	DRASE	561
I41001	M11000		D		11000	21		DRASE	562
					11000		WING ASSY F15	DRASE	563
					11000		CRACKS IN WINGS SKIN BEING LOOKED	DRASE	564
					11000		INTO BY ENGINEERS	DRASE	565
					11000		F-2 112 USED FOR COMPARABILITY	DRASE	566
					11000		MSGT DICELLO LUKE SHEET MOL PM2767	DRASE	567
					11000		F15 DATA SHOWS 33 MSMA AUG75	DRASE	568
					11000		WING ASSY F15	DRASE	569
A1K01	F11K00	A1K01	F	21	11K00	21		DRASE	570
A1K01	F11K00	A1K02	F	15	11K00	21		DRASE	571
A1K01	M11K00		F	30	11K00	21	120 29L 2424X3	DRASE	572
A1K01	M11K00		F	77	11K00	21	29 29L 2424X3	DRASE	573
A1K01	M11K00	A1K02	F	21	11K00	21	95 29L 443101	DRASE	574
A1K01	M11K00	A1K02	F	22	11K00	21	25 29L 1431X1	DRASE	575
A1K01	M11K00		F	40	11K00	21	10 29L 1531X3	DRASE	576
A1K01	M11K00		F	40	11K00	21	18 29L 2531X3	DRASE	577
A1K01	M11K00	A1K02	F		11K00	23		DRASE	578
S41K01	L11K00	I41K01	G	11-55	11K00	23		DRASE	579
L11K00					11K00		LEADING EDGE TRAILING EDGE	DRASE	580
I41K01	M11K00		F	65	11K00	23	23 29L 1531X3	DRASE	581
I41K01	M11K00		F	34	11K00	23	15 29L 2536X3	DRASE	582
I41K01	M11K00		F		11K00	21	95 29L 443101	DRASE	583
S41K01	L11K00	I41K01	G	11-19	11K00	23		DRASE	584
L11K00					11K00		WING ACCESS PROVISIONS	DRASE	585
I41K01	M11K00		D		11K00	23	18 29L 2531X3	DRASE	586
I41K01	M11K00		F		11K00	21	28 29L 1431X1	DRASE	587
					11P00		AIR INDUCTION SYS IS EXPECTED TO	DRASE	588
					11P00		HAVE HIGHER FAIL RATE THAN F-2	DRASE	589
					11P00		REASON IS MORE CYLINDERS & SERVOS	DRASE	590
					11P00		F15 DATA SHOWS 18 MSMA AUG75	DRASE	591

M	11000	F4E 113 DATA USED 30 45PMA	DBASE	592
M	11000	A COMPOSITE OF F4E & F15 FOR SHCP	DBASE	593
4	11000	AIP INJECTION SYS F15	DBASE	594
A1P01	F15P01	A1P01	22 11000 21	DBASE 595
A1P01	F15P01	A1P02	04 11000 21	DBASE 596
A1P01	F15P01	A1P02	12 11000 21	DBASE 597
A1P01	F15P01	A1P02	03 11000 21	DBASE 598
A1P01	F15P01	A1P02	02 11000 21	DBASE 599
A1P01	F15P01	A1P02	24 11000 21	DBASE 600
A1P01	F15P01	A1P02	14 11000 21	DBASE 601
A1P01	F15P01	A1P02	05 11000 21	DBASE 602
A1P01	F15P01	A1P02	13 11000 21	DBASE 603
A1P01	F15P01	A1P02	05 11000 21	DBASE 604
A1P01	F15P01	A1P02	11 11000 21	DBASE 605
S41P01	L11P01	I41P01	0 11293 11000 23	DBASE 606
L11P01	11000	VARIABLE INLET PUMP SYS	DBASE 607	
I41P01	M11P01	0	11000*23	DBASE 608
I41P01	M11P01	1	11000 21	DBASE 609
S41P01	L11P01	I41P01	0 11655 11000 23	DBASE 610
L11P01	11000	CONTROLLER JIF INLET	DBASE 611	
I41P01	M11P01	1	11000 23	DBASE 612
I41P01	M11P01	1	11000*23	DBASE 613
I41P01	M11P01	I41P01	0 11000 23	DBASE 614
I41P01	M11P01	1	27 11000 23	DBASE 615
I41P01	M11P01	1	44 11000 23	DBASE 616
I41P01	M11P01	1	34 11000 23	DBASE 617
M	12000	F4E 121 DATA USED	DBASE 618	
4	12000	F4E 45PMA 210	DBASE 619	
4	12000	MSG OICELLO LUKE PH0793 SHEETMOL	DBASE 620	
4	12000	TSG SWEERS LUKE 130 PH 2466	DBASE 621	
4	12000	COCKPIT FURNISHINGS F15	DBASE 622	
A2001	F12001	A2001	0 102 12000 21	DBASE 623
A2001	F12001	A2002	03 12000 21	DBASE 624
A2001	F12001	A2002	07 12000 21	DBASE 625
A2001	F12001	A2002	47 12000 21	DBASE 626
A2001	F12001	A2002	45 12000 21	DBASE 627
A2001	F12001	A2002	0 12000 23	DBASE 628
S42001	L12001	I42001	0 10015 12000 23	DBASE 629
L12001	12000	PANELS	DBASE 630	
I42001	M12001	0	12000*23	DBASE 631
I42001	M12001	0	12000 21	DBASE 632
S42001	L12001	I42001	0 10015 12000 23	DBASE 633
L12001	12000	GLARE SHIELD INS PAN FWD CREW LH RH C	DBASE 634	
I42001	M12001	0	12000*23	DBASE 635
I42001	M12001	0	12000 21	DBASE 636
M	12000	EJECTION SEAT	DBASE 637	
4	12000	A70 120 DATA USED	DBASE 638	
4	12000	ASSUME NO SEAT REMOVAL EXCEPT SCHEP	DBASE 639	
4	12000	NO ITEM TO SHOP ITEM FAILING A70 IS	DBASE 640	
4	12000	NOT ON F15 F15 MS30A 122	DBASE 641	
4	12000	TSG JENSEN LUKE PH 2325 EXPRESS	DBASE 642	
4	12000	SSG SCHNEIDER EDWARDS EXPRESS	DBASE 643	
4	12000	MSG GREGSON LUKE PH 2325 EXPRESS VER	DBASE 644	
4	12000	MSG MILLER LUKE PH 2325 EXPRESS	DBASE 645	
4	12000	EJECTION SEAT F15	DBASE 646	
A2001	F12001	A2001	0 125 12000 21	DBASE 647
A2001	F12001	A2002	0 12000 21	DBASE 648
A2001	F12001	A2002	0 12000 21	DBASE 649
A2001	F12001	A2002	66 12000 21	DBASE 650
A2001	F12001	A2002	16 12000 21	DBASE 651
A2001	F12001	A2002	18 12000 21	DBASE 652
A2001	F12001	A2002	0 12000 21	DBASE 653
4	12000	CANOPY	DBASE 654	
4	12000	F4E 123 DATA USED	DBASE 655	
4	12000	V12001 IS PRES OK	DBASE 656	
4	12000	MYD OPERATED CANOPY	DBASE 657	

4	12000	MSG DICELLO LUKE PH 2753 SWEET MDL	03ASE	659
4	12000	MSG JENSEN LUKE EGR-SS	03ASE	659
4	12000	SSG SCHMEIDER EDWARDS EXPRESS	03ASE	660
4	12000	STAGING CANOPY MUCH LARGER JCR THAN	03ASE	661
4	12000	F4 CANOPY ASSY WILL BE DOUBLE F4E	03ASE	662
4	12000	CANOPY MAT APPROX 2 FEET FROM 1000M	03ASE	663
4	12000	AFTER THAT A HAND PUMP UP OF HYD TUBE	03ASE	664
4	12000	F4E MSGMA 42	03ASE	665
4	12000	CANOPY ASSY F15	03ASE	666
A2C11	12000	25 12000 21	03ASE	667
A2C11	12000	53 12000 21	03ASE	668
A2C11	12000	53 12000 21	03ASE	669
A2C11	12000	24 12000 21 12 29L 2421X2 1TU228	03ASE	670
A2C11	12000	24 12000 21 22 29L 2431X1 1TU228	03ASE	671
A2C11	12000	24 12000 21 24 29L 2422X1	03ASE	672
A2C11	12000	24 12000 21 24 29L 2431X1	03ASE	673
A2C11	12000	24 12000 21 24 29L 2422X1	03ASE	674
A2C11	12000	24 12000 21 24 29L 2431X1	03ASE	675
A2C11	12000	24 12000 21 24 29L 2431X1	03ASE	676
A2C11	12000	24 12000 21 24 29L 2431X1	03ASE	677
A2C11	12000	24 12000 21 24 29L 2431X1	03ASE	678
A2C11	12000	24 12000 21 24 29L 2421X2 1TU228	03ASE	679
A2C11	12000	24 12000 21 24 29L 2421X2 1TU228	03ASE	680
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	681
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	682
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	683
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	684
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	685
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	686
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	687
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	688
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	689
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	690
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	691
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	692
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	693
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	694
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	695
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	696
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	697
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	698
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	699
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	700
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	701
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	702
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	703
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	704
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	705
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	706
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	707
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	708
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	709
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	710
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	711
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	712
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	713
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	714
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	715
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	716
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	717
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	718
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	719
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	720
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	721
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	722
A2C11	12000	24 12000 21 24 29L 2422X1 1TU228	03ASE	723

A3A11	W13A13	E	05	13A02	21	06 29L 1431Y1	DBASE	724
A3A12	W13A13	E	27	13A02	21	17 29L 2531Y1	DBASE	725
A3A12	VJACK	A3A05	0	13A02	21	17 29L 4431Y1 1360	DBASE	726
A3A13	VJACK	A3A05	0	13A02	21		DBASE	727
A3A14	VJACK	A3A05	0	13A02	21		DBASE	728
A3A15	VJACK	A3A05	0	13A02	21	15 29L 2431Y1 1360	DBASE	729
A3A16	VJACK	A3A05	0	13A02	21		DBASE	730
A3A17	VJACK	A3A05	0	13A02	21		DBASE	731
A3A18	SHOP	SAB00	0	13A02	21		DBASE	732
SAB00	L13A02	A3A05	0	13A02	21		DBASE	733
L13A02						MAIN LG MECH COMPTS 13A1 THRU 13A6	DBASE	734
IA3A01	W13A02	E	57	13A02	23	15 29L 2421Y2	DBASE	735
IA3A02	W13A02	E	25	13A02	23	01 29L 2531Y1	DBASE	736
IA3A03	W13A02	E	25	13A02	23	21 29L 1531Y1	DBASE	737
IA3A04	W13A02	E		13A02	21	24 29L 2421Y2	DBASE	738
SAB00	L13A02	A3A05	0	13A02	23		DBASE	739
L13A02						UPATCH MECH ETC 13A1	DBASE	740
IA3A05	W13A02	E	07	13A02	23	06 29L 1531Y1	DBASE	741
IA3A06	W13A02	E	03	13A02	23	03 29L 2531Y1	DBASE	742
IA3A07	W13A02	E		13A02	21		DBASE	743
		M		13A02		NOSE GEAR TO INCLUDE STEERING	DBASE	744
		M		13A02		F4E 133 DATA USED	DBASE	745
		M		13A02		V TASK APP FOR JACKING / RETRACT OK	DBASE	746
		M		13A02		F15 MSBMA 149	DBASE	747
		M		13A02		MOSE GEAR / STEP COMPTS	DBASE	748
		M		13A02		SHIMMY PROBLEM STARTING	DBASE	749
		M		13A02		NOSE LG / STEP F15	DBASE	750
A3B11	F13B11	A3B11	E	25	13B02	21	DBASE	751
A3B12	F13B11	A3B11	E	15	13B02	21	DBASE	752
A3B13	F13B11	A3B11	E		13B02	21	DBASE	753
A3B14	F13B11	A3B11	E		13B02	21	DBASE	754
A3B15	F13B11	A3B11	E		13B02	21	DBASE	755
A3B16	F13B11	A3B11	E	05	13B02	21	DBASE	756
A3B17	F13B11	A3B11	E		13B02	21	DBASE	757
A3B18	F13B11	A3B11	E		13B02	21	DBASE	758
A3B19	F13B11	A3B11	E	04	13B02	21	DBASE	759
A3B20	F13B11	A3B11	E		13B02	21	DBASE	760
A3B21	F13B11	A3B11	E		13B02	21	DBASE	761
A3B22	F13B11	A3B11	E		13B02	21	DBASE	762
A3B23	F13B11	A3B11	E		13B02	21	DBASE	763
A3B24	F13B11	A3B11	E		13B02	21	DBASE	764
A3B25	F13B11	A3B11	E		13B02	21	DBASE	765
A3B26	F13B11	A3B11	E		13B02	21	DBASE	766
A3B27	F13B11	A3B11	E		13B02	21	DBASE	767
A3B28	F13B11	A3B11	E		13B02	21	DBASE	768
A3B29	F13B11	A3B11	E		13B02	21	DBASE	769
A3B30	F13B11	A3B11	E		13B02	21	DBASE	770
A3B31	F13B11	A3B11	E		13B02	21	DBASE	771
A3B32	F13B11	A3B11	E		13B02	21	DBASE	772
A3B33	F13B11	A3B11	E		13B02	21	DBASE	773
A3B34	F13B11	A3B11	E		13B02	21	DBASE	774
A3B35	F13B11	A3B11	E		13B02	21	DBASE	775
A3B36	F13B11	A3B11	E		13B02	21	DBASE	776
A3B37	F13B11	A3B11	E		13B02	21	DBASE	777
A3B38	F13B11	A3B11	E		13B02	21	DBASE	778
A3B39	F13B11	A3B11	E		13B02	21	DBASE	779
A3B40	F13B11	A3B11	E		13B02	21	DBASE	780
A3B41	F13B11	A3B11	E		13B02	21	DBASE	781
A3B42	F13B11	A3B11	E		13B02	21	DBASE	782
A3B43	F13B11	A3B11	E		13B02	21	DBASE	783
A3B44	F13B11	A3B11	E		13B02	21	DBASE	784
A3B45	F13B11	A3B11	E		13B02	21	DBASE	785
A3B46	F13B11	A3B11	E		13B02	21	DBASE	786
A3B47	F13B11	A3B11	E		13B02	21	DBASE	787
A3B48	F13B11	A3B11	E		13B02	21	DBASE	788
A3B49	F13B11	A3B11	E		13B02	21	DBASE	789
A3B50	F13B11	A3B11	E		13B02	21	DBASE	790
A3B51	F13B11	A3B11	E		13B02	21	DBASE	791
A3B52	F13B11	A3B11	E		13B02	21	DBASE	792
A3B53	F13B11	A3B11	E		13B02	21	DBASE	793
A3B54	F13B11	A3B11	E		13B02	21	DBASE	794
A3B55	F13B11	A3B11	E		13B02	21	DBASE	795
A3B56	F13B11	A3B11	E		13B02	21	DBASE	796
A3B57	F13B11	A3B11	E		13B02	21	DBASE	797
A3B58	F13B11	A3B11	E		13B02	21	DBASE	798
A3B59	F13B11	A3B11	E		13B02	21	DBASE	799
A3B60	F13B11	A3B11	E		13B02	21	DBASE	800
A3B61	F13B11	A3B11	E		13B02	21	DBASE	801
A3B62	F13B11	A3B11	E		13B02	21	DBASE	802
A3B63	F13B11	A3B11	E		13B02	21	DBASE	803
A3B64	F13B11	A3B11	E		13B02	21	DBASE	804
A3B65	F13B11	A3B11	E		13B02	21	DBASE	805
A3B66	F13B11	A3B11	E		13B02	21	DBASE	806
A3B67	F13B11	A3B11	E		13B02	21	DBASE	807
A3B68	F13B11	A3B11	E		13B02	21	DBASE	808
A3B69	F13B11	A3B11	E		13B02	21	DBASE	809
A3B70	F13B11	A3B11	E		13B02	21	DBASE	810
A3B71	F13B11	A3B11	E		13B02	21	DBASE	811
A3B72	F13B11	A3B11	E		13B02	21	DBASE	812
A3B73	F13B11	A3B11	E		13B02	21	DBASE	813
A3B74	F13B11	A3B11	E		13B02	21	DBASE	814
A3B75	F13B11	A3B11	E		13B02	21	DBASE	815
A3B76	F13B11	A3B11	E		13B02	21	DBASE	816
A3B77	F13B11	A3B11	E		13B02	21	DBASE	817
A3B78	F13B11	A3B11	E		13B02	21	DBASE	818
A3B79	F13B11	A3B11	E		13B02	21	DBASE	819
A3B80	F13B11	A3B11	E		13B02	21	DBASE	820
A3B81	F13B11	A3B11	E		13B02	21	DBASE	821
A3B82	F13B11	A3B11	E		13B02	21	DBASE	822
A3B83	F13B11	A3B11	E		13B02	21	DBASE	823
A3B84	F13B11	A3B11	E		13B02	21	DBASE	824
A3B85	F13B11	A3B11	E		13B02	21	DBASE	825
A3B86	F13B11	A3B11	E		13B02	21	DBASE	826
A3B87	F13B11	A3B11	E		13B02	21	DBASE	827
A3B88	F13B11	A3B11	E		13B02	21	DBASE	828
A3B89	F13B11	A3B11	E		13B02	21	DBASE	829
A3B90	F13B11	A3B11	E		13B02	21	DBASE	830
A3B91	F13B11	A3B11	E		13B02	21	DBASE	831
A3B92	F13B11	A3B11	E		13B02	21	DBASE	832
A3B93	F13B11	A3B11	E		13B02	21	DBASE	833
A3B94	F13B11	A3B11	E		13B02	21	DBASE	834
A3B95	F13B11	A3B11	E		13B02	21	DBASE	835
A3B96	F13B11	A3B11	E		13B02	21	DBASE	836
A3B97	F13B11	A3B11	E		13B02	21	DBASE	837
A3B98	F13B11	A3B11	E		13B02	21	DBASE	838
A3B99	F13B11	A3B11	E		13B02	21	DBASE	839
A3B00	F13B11	A3B11	E		13B02	21	DBASE	840
A3B01	F13B11	A3B11	E		13B02	21	DBASE	841
A3B02	F13B11	A3B11	E		13B02	21	DBASE	842
A3B03	F13B11	A3B11	E		13B02	21	DBASE	843
A3B04	F13B11	A3B11	E		13B02	21	DBASE	844
A3B05	F13B11	A3B11	E		13B02	21	DBASE	845
A3B06	F13B11	A3B11	E		13B02	21	DBASE	846
A3B07	F13B11	A3B11	E		13B02	21	DBASE	847
A3B08	F13B11	A3B11	E		13B02	21	DBASE	848
A3B09	F13B11	A3B11	E		13B02	21	DBASE	849
A3B10	F13B11	A3B11	E		13B02	21	DBASE	850
A3B11	F13B11	A3B11	E		13B02	21	DBASE	851
A3B12	F13B11	A3B11	E		13B02	21	DBASE	852
A3B13	F13B11	A3B11	E		13B02	21	DBASE	853
A3B14	F13B11	A3B11	E		13B02	21	DBASE	854
A3B15	F13B11	A3B11	E		13B02	21	DBASE	855
A3B16	F13B11	A3B11	E		13B02	21	DBASE	856
A3B17	F13B11	A3B11	E		13B02	21	DBASE	857
A3B18	F13B11	A3B11	E		13B02	21	DBASE	858
A3B19	F13B11	A3B11	E		13B02	21	DBASE	859
A3B20	F13B11	A3B11	E		13B02	21	DBASE	860
A3B21	F13B11	A3B11	E		13B02	21	DBASE	861
A3B22	F13B11	A3B11	E		13B02	21	DBASE	862
A3B23	F13B11	A3B11	E		13B02	21	DBASE	863
A3B24	F13B11	A3B11	E		13B02	21	DBASE	864
A3B25	F13B11	A3B11	E		13B02	21	DBASE	865
A3B26	F13B11	A3B11	E		13B02	21	DBASE	866
A3B27	F13B11	A3B11	E		13B02	21	DBASE	867
A3B28	F13B11	A3B11	E		13B02	21	DBASE	868
A3B29	F13B11	A3B11	E		13B02	21	DBASE	869
A3B30	F13B11	A3B11	E		13B02	21	DBASE	870
A3B31	F13B11	A3B11	E		13B02	21	DBASE	871
A3B32	F13B11	A3B11	E		13B02	21	DBASE	872
A3B33	F13B11	A3B11	E		13B02	21	DBASE	873
A3B34	F13B11	A3B11	E		13B02	21	DBASE	874
A3B35	F13B11	A3B11	E		13B02	21	DBASE	875
A3B36	F13B11	A3B11	E		13B02	21	DBASE	876
A3B37	F13B11	A3B11	E		13B02	21	DBASE	877
A3B38	F13B11	A3B11	E		13B02	21	DBASE	878
A3B39	F13B11	A3B11	E		13B02	21	DBASE	879
A3B40	F13B11	A3B11	E		13B02	21	DBASE	880
A3B41	F13B11	A3B11	E		13B02	21	DBASE	881
A3B42	F13B11	A3B11	E		13B02	21	DBASE	882
A3B43	F13B11	A3B11	E		13B02	21	DBASE	883
A3B44	F13B11	A3B11	E		13B02	21	DBASE	884
A3B45	F13B11	A3B11	E		13B02	21	DBASE	885
A3B46	F13B11	A3B11	E		13B02	21	DBASE	886
A3B47	F13B11	A3B11	E		13B02	21	DBASE	887
A3B48	F13B11	A3B11	E		13B02	21	DBASE	888
A3B49	F13B11	A3B11	E		13B02	21	DBASE	889
A3								

A3C01	F13C01	A3C01	F	16	13C00	21			DBASE	791
A3C01	F13C01	A3C01	F	4	13C00	21	33	29L 2-21X2	DBASE	791
A3C01	F13C01	A3C01	F	12	13C00	21	16	29L 2-21X2	DBASE	792
A3C01	F13C01	A3C01	F	03	13C00	21	09	29L 2-23X0	DBASE	793
A3C01	F13C01	A3C01	F	04	13C00	21	22	29L 1-31X1	DBASE	794
A3C01	F13C01	A3C01	F	05	13C00	21	13	29L 1-31X1	DBASE	795
A3C01	F13C01	A3C01	F	21	13C00	21	19	29L 1531X0	DBASE	796
A3C01	F13C01	A3C01	F	02	13C00	21	16	29L 2631X3	DBASE	797
A3C01	F13C01	A3C01	F	03	13C00	23			DBASE	798
A3C01	F13C01	A3C01	F	04	13C00	23			DBASE	799
A3C01	F13C01	A3C01	F	05	13C00	23			DBASE	800
A3C01	F13C01	A3C01	F	06	13C00	23			DBASE	801
A3C01	F13C01	A3C01	F	07	13C00	23			DBASE	802
A3C01	F13C01	A3C01	F	08	13C00	23			DBASE	803
A3C01	F13C01	A3C01	F	09	13C00	23			DBASE	804
A3C01	F13C01	A3C01	F	10	13C00	23			DBASE	805
A3C01	F13C01	A3C01	F	11	13C00	23			DBASE	806
A3C01	F13C01	A3C01	F	12	13C00	23			DBASE	807
A3C01	F13C01	A3C01	F	13	13C00	23			DBASE	808
A3C01	F13C01	A3C01	F	14	13C00	23			DBASE	809
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A3C01	F13C01	A3C01	F	16	13C00	23			DBASE	811
A3C01	F13C01	A3C01	F	17	13C00	23			DBASE	812
A3C01	F13C01	A3C01	F	18	13C00	23			DBASE	813
A3C01	F13C01	A3C01	F	19	13C00	23			DBASE	814
A3C01	F13C01	A3C01	F	20	13C00	23			DBASE	815
A3C01	F13C01	A3C01	F	21	13C00	23			DBASE	816
A3C01	F13C01	A3C01	F	22	13C00	23			DBASE	817
A3C01	F13C01	A3C01	F	23	13C00	23			DBASE	818
A3C01	F13C01	A3C01	F	24	13C00	23			DBASE	819
A3C01	F13C01	A3C01	F	25	13C00	23			DBASE	820
A3C01	F13C01	A3C01	F	26	13C00	23			DBASE	821
A3C01	F13C01	A3C01	F	27	13C00	23			DBASE	822
A3C01	F13C01	A3C01	F	28	13C00	23			DBASE	823
A3C01	F13C01	A3C01	F	29	13C00	23			DBASE	824
A3C01	F13C01	A3C01	F	30	13C00	23			DBASE	825
A3C01	F13C01	A3C01	F	31	13C00	23			DBASE	826
A3C01	F13C01	A3C01	F	32	13C00	23			DBASE	827
A3C01	F13C01	A3C01	F	33	13C00	23			DBASE	828
A3C01	F13C01	A3C01	F	34	13C00	23			DBASE	829
A3C01	F13C01	A3C01	F	35	13C00	23			DBASE	830
A3C01	F13C01	A3C01	F	36	13C00	23			DBASE	831
A3C01	F13C01	A3C01	F	37	13C00	23			DBASE	832
A3C01	F13C01	A3C01	F	38	13C00	23			DBASE	833
A3C01	F13C01	A3C01	F	39	13C00	23			DBASE	834
A3C01	F13C01	A3C01	F	40	13C00	23			DBASE	835
A3C01	F13C01	A3C01	F	41	13C00	23			DBASE	836
A3C01	F13C01	A3C01	F	42	13C00	23			DBASE	837
A3C01	F13C01	A3C01	F	43	13C00	23			DBASE	838
A3C01	F13C01	A3C01	F	44	13C00	23			DBASE	839
A3C01	F13C01	A3C01	F	45	13C00	23			DBASE	840
A3C01	F13C01	A3C01	F	46	13C00	23			DBASE	841
A3C01	F13C01	A3C01	F	47	13C00	23			DBASE	842
A3C01	F13C01	A3C01	F	48	13C00	23			DBASE	843
A3C01	F13C01	A3C01	F	49	13C00	23			DBASE	844
A3C01	F13C01	A3C01	F	50	13C00	23			DBASE	845
A3C01	F13C01	A3C01	F	51	13C00	23			DBASE	846
A3C01	F13C01	A3C01	F	52	13C00	23			DBASE	847
A3C01	F13C01	A3C01	F	53	13C00	23			DBASE	848
A3C01	F13C01	A3C01	F	54	13C00	23			DBASE	849
A3C01	F13C01	A3C01	F	55	13C00	23			DBASE	850
A3C01	F13C01	A3C01	F	56	13C00	23			DBASE	851
A3C01	F13C01	A3C01	F	57	13C00	23			DBASE	852
A3C01	F13C01	A3C01	F	58	13C00	23			DBASE	853
A3C01	F13C01	A3C01	F	59	13C00	23			DBASE	854
A3C01	F13C01	A3C01	F	60	13C00	23			DBASE	855

A3F13 R13F11	E	23	13F01 21	07 29L 232682 1060	DBASE 856
A3F12 V13F11	J		13F01 21	11 29L 2-21X2 1060 1421X1	DBASE 857
A3F15 V13F12	E	1	13F01 21	09 29L 1-31X1 1060	DBASE 858
A3F13 S40F	J		13F01 21		DBASE 859
S43F11 L13F11 IA3F01	J		13F01 23		DBASE 860
L13F11	J		13F01	110 CONT MARY / F450G SYS	DBASE 861
IA3F01 V13F11	J		13F01*23	12 29L 1-21X2	DBASE 862
IA3F11 V13F11	J		13F01 21		DBASE 863
	M		13M00	SKID CONT SYS	DBASE 864
	M		13M00	F15 1161 DATA USED	DBASE 865
	M		13M00	F15 MS14A 33 AUG 75	DBASE 866
	M		13M00	SKID CONT SYS F15	DBASE 867
A3M01 F13M01 A3M11	F	237	13M01 21		DBASE 868
A3M11 V13M01	J		13M01 21	31 29L 2-23X0 1-31X1 1-21X2	DBASE 869
A3M11 F13M01	E	02	13M01 21	34 29L 2-21X2	DBASE 870
A3M11 V13M01	E	1	13M01 21	11 29L 2-21X2	DBASE 871
A3M11 F13M01	E	35	13M01 21	14 29L 2-23X0	DBASE 872
A3M11 V13M01	E	55	13M01 21	12 29L 2-23X0	DBASE 873
A3M12 S40F	J		13M01 23		DBASE 874
S43M11 L13M01	J		13M01 23		DBASE 875
L13M01	J		13M01	CONT SYS	DBASE 876
IA3M11 V13M01	J		13M01*23	10 29L 1-23X0	DBASE 877
IA3M11 V13M01	I		13M01 21	14 29L 2-23X0	DBASE 878
	M		13J01	WHEEL / TIRE	DBASE 879
	M		13J00	F15 1333 1325 1326 FOR F15 13AJ 3J	DBASE 880
	M		13J00	ASSUME F15 13AJ2142 CHGS EQUAL F15	DBASE 881
	M		13J00	WARTIME CHGS	DBASE 882
	M		13J00	F15 MS14A 15	DBASE 883
	M		13J00	WHEEL / TIRE F15	DBASE 884
A3J01 F13J01	F	19	13J01 21		DBASE 885
A3J01 F13J01	J		13J01 21	09 29L 2-23X1	DBASE 886
A3J01 S40F	J		13J01 23		DBASE 887
S43J01 L13J01	J		13J01 23		DBASE 888
L13J01	J		13J01	WHEEL / TIRE	DBASE 889
IA3J01 V13J01	E	61	13J01*23	02 29L 1-23X1	DBASE 890
IA3J01 V13J01	E	99	13J01*23	12 29L 1-23X1	DBASE 891
IA3J01 V13J01	J		13J01 23	20 29L 2-23X1	DBASE 892
IA3J01 V13J01	J		13J01 21	15 29L 2-23X1	DBASE 893
	M		14AA0	CONTROL STICK	DBASE 894
	M		14AA0	F15 MS14A 21	DBASE 895
	M		14AA0	SSG THOMPSON FLT CONT EDWARDS	DBASE 896
	M		14AA0	TSG PYLE LUKE FLT CONT	DBASE 897
	M		14AA0	TSG FULTON EDWARDS	DBASE 898
	M		14AA0	TSG MCNALLY LUKE HYO	DBASE 899
	M		14AA0	SSG SAMPLE EDWARDS HYO	DBASE 900
	M		14AA0	SSG TWEED EDWARDS APG	DBASE 901
	M		14AA0	TSG SWEEBE LUKE APG 2464	DBASE 902
	M		14AA0	F111F 14AA0 DATA USED	DBASE 903
	M		14AA0	CONTROL STICK F15	DBASE 904
A4AA1 F14AA1	F	97	14AA1 21		DBASE 905
A4AA1 F14AA1	J		14AA1 21		DBASE 906
A4AA1 F14AA1	J		14AA1 21		DBASE 907
A4AA1 F14AA1	J		14AA1 21		DBASE 908
A4AA1 F14AA1	J		14AA1 21		DBASE 909
A4AA1 F14AA1	J		14AA1 21	23 29L 2-23X0 1060 17U228	DBASE 910
A4AA1 F14AA1	J	55	14AA1 21	06 29L 232682	DBASE 911
A4AA1 F14AA1	J	45	14AA1 21	15 29L 2-23X0 1060 17U228	DBASE 912
A4AA1 F14AA1	J		14AA1 21	18 29L 232682 1060 17U228	DBASE 913
A4AA1 S40F	J		14AA1 23		DBASE 914
S44AA1 L14AA1	J		14AA1 23		DBASE 915
L14AA1	J		14AA1	CONTROL STICK ASSY	DBASE 916
IA4AA1 V14AA1	J	21	14AA1*23	04 29L 1-23X0	DBASE 917
IA4AA1 V14AA1	E	60	14AA1 23	11 29L 132631	DBASE 918
IA4AA1 V14AA1	J		14AA1*23	20 G	DBASE 919
IA4AA1 V14AA1	I		14AA1 21	15 29L 2-23X0	DBASE 920
	M		14AA0	F15 DATA USED	DBASE 921

M	14430	NO COMPARIBILITY	09ASE	922
M	14431	T007 F00LE L0KE	09ASE	923
M	14432	T007 FULTON EDWARDS	09ASE	924
M	14433	F15 MSPMA 420	09ASE	925
M	14434	PITCH & ROLL CHANNEL ASY F15	09ASE	926
A4431 F14431 14431 F 711 14431 21			09ASE	927
A4431 F14431 14432 D	14431 21	54 29L 2421X2	09ASE	928
A4432 V14431 14432 D	14431 21	40 29L 1-21X2 232632 243101 1060	09ASE	929
A4433 S40P S44401 D	14432 23		09ASE	930
SA4431 LI4431 144401 D	14432 23		09ASE	931
LI4431	14433	PITCH & ROLL CHANNEL ASY	09ASE	932
IA4431 NI4431	14433 23	19 29L 1-21X2	09ASE	933
IA4431 Q14431	14433 21	54 29L 2-21X2	09ASE	934
	14433	STAR SYS DATA	09ASE	935
	14433	F111F 1407A + 37% 14HAB + 14003 C 10	09ASE	936
	14433	F4E 14311 FOR APG & 11% OF SHEET MOL	09ASE	937
	14433	F15 MSPMA 420	09ASE	938
	14433	STAR SYS F15	09ASE	939
A4001 F14001 14001 F 150 14001 21			09ASE	940
A4001 00R407 14001 D	14001 21		09ASE	941
A4001 01LGPU 14001 D	14001 21		09ASE	942
A4001 00R407 14001 D	14001 21		09ASE	943
A4001 01LTTU 14001 D	14001 21		09ASE	944
A4001 01L01	54 14001 21	26 29L 2-31X1 1060 170224	09ASE	945
A4001 01L01	24 14001 21	17 29L 1431X1 1060 170225	09ASE	946
A4001 01L01	05 14001 21	20 29L 232632 1060 170224	09ASE	947
A4001 01L013 14001 E 1 14001 21		57 29L 2421X2 170226	09ASE	948
A4001 S40P S44001 D	14001 23		09ASE	949
SA4001 LI4001 14001 D	14001 23		09ASE	950
LI4001	14001	STAR SYS	09ASE	951
IA4001 NI4001	14001 23	15 29L 2421X2	09ASE	952
IA4001 Q14001	14001 21	26 29L 2431X1	09ASE	953
	14001	RUDDER	09ASE	954
	14001	F111F 14400 23X F4E 1442 C 10 14400	09ASE	955
	14001	FOR APG	09ASE	956
	14001	F15 MSPMA 32	09ASE	957
	14001	RUDDER F15	09ASE	958
A4001 F14001 14001 F 21 14001 21			09ASE	959
A4001 00R407 14001 D	14001 21		09ASE	960
A4001 00R407 14001 D	14001 21		09ASE	961
A4001 01LGPU 14001 D	14001 21		09ASE	962
A4001 01LTTU 14001 D	14001 21		09ASE	963
A4001 01L01	20 14001 21	35 29L 2431X1 1060 170224	09ASE	964
A4001 01L01 14001 E 61 14001 21		30 29L 2431X2 1060 170224	09ASE	965
A4001 01L01	05 14001 21	12 29L 1431X1	09ASE	966
A4001 01L01	05 14001 21	20 29L 232632 1060 170225	09ASE	967
A4001 01L012	02 14001 21	20 29L 243101	09ASE	968
A4001 S40P S44001 D	14001 23		09ASE	969
SA4001 LI4001 14001 D	14001 23		09ASE	970
LI4001	14001	RUDDER COMPTS	09ASE	971
IA4001 NI4001	97 14001 23	10 29L 2421X2	09ASE	972
IA4001 NI4001	03 14001 23	16 29L 2421X2	09ASE	973
IA4001 Q14001	14001 21	27 29L 2421X2	09ASE	974
	14001	SPEED BRAKE SYS	09ASE	975
	14001	F4E 14001 00S 14001 DATA 0000	09ASE	976
	14001	F15 MSPMA 210	09ASE	977
	14001	SPEED BRAKE SYS F15	09ASE	978
A4E01 F14E01 14E01 F 67 14E01 21			09ASE	979
A4E01 00R407 14E01 D	14E01 21		09ASE	980
A4E01 01LGPU 14E01 D	14E01 21		09ASE	981
A4E01 00R407 14E01 D	14E01 21		09ASE	982
A4E01 01LTTU 14E01 D	14E01 21		09ASE	983
A4E01 01L01 14E01 E 05 14E01 21		40 29L 2421X2 1060 170228	09ASE	984
A4E01 01L01	56 14E01 21	16 29L 2421X2 1060 170228	09ASE	985
A4E01 01L012 14E01 E 03 14E01 21		17 29L 2421X3 1060 170228	09ASE	986
A4E01 01L01	05 14E01 21	11 29L 2423X0 1060 170228	09ASE	987

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83104	023P4M	83106	0	23100	21	3 29L 1431X1	0BASE	1054	
			4	23100		023P40 INSTALL OF REMOVE ACFT FROM PAC	0BASE	1055	
83105	023P40	83106	0	23100	21	3 29L 1432X0 1431X1	0BASE	1056	
			4	23100		T23100 TROUBLESHOOT, FLY, TRIM, AND LEAK	0BASE	1057	
			4	23100		NO PARTS REPLACEMENT	0BASE	1058	
83105	T23101	83107	E	25	23100	21	30 29L 1432X0 1431X1	0BASE	1059
			4	23100		M23100 MINOR REPAIR WITH PART CHANGES	0BASE	1060	
			4	23100		ON TRIM PAD	0BASE	1061	
83105	M23100	83106	E	50	23100	21	50 29L 1432X0 1431X1	0BASE	1062
83105	M23100	83106	E	25	23100	21		0BASE	1063
83105	023P40	83106	0	23100	21		0BASE	1064	
83105	023P4M	83106	0	23100	21		0BASE	1065	
83105	023P4M	83106	0	23100	21		0BASE	1066	
			4	23100		023P40 ENGINE LEAK CHECK	0BASE	1067	
83105	023P4M	83106	0	23100	21	5 29L 2432X0 1431X1	0BASE	1068	
83105	SHOP	83106	0	23100	21		0BASE	1069	
83105	023P40	83106	0	23100	21		0BASE	1070	
83105	023P4M	83106	0	23100	21		0BASE	1071	
			4	23100		M23100 MINOR REPAIR WITH PART CHANGE	0BASE	1072	
			4	23100		ON FLIGHT LINE	0BASE	1073	
83105	M23100	83106	E	90	23100	21	10 29L 2432X0	0BASE	1074
83105	M23100	83106	E	25	23100	21		0BASE	1075
83105	023P4M	83106	0	23100	21		0BASE	1076	
83105	SHOP	83106	0	23100	21		0BASE	1077	
83105	023P4M	83106	0	23100	21		0BASE	1078	
83105	023P4M	83106	0	23100	21	15 29L 4432X0	0BASE	1079	
83105	023P4M	83106	0	23100	21	15 29L 4432X0	0BASE	1080	
83105	023P4M	83106	0	23100	21		0BASE	1081	
83105	023P4M	83106	0	23100	21		0BASE	1082	
83105	023P4M	83106	E	95	23100	21		0BASE	1083
83105	023P4M	83106	E	65	23100	21		0BASE	1084
			4	23100		ENGINE IN SHOP AND TEST CELL	0BASE	1085	
83105	023P40	83106	0	23100	23	35 29L 3432X0 133000	0BASE	1086	
			4	23100		DTOW23 TOW ENGINE TO TEST CELL	0BASE	1087	
83105	DTOW23	83106	E	20	23100	23	1 29L 2432T0	0BASE	1088
83105	SHOP	83106	E	75	23100	23		0BASE	1089
			4	23100		023100 CONNECT AND DISCONNECT TEST CELL	0BASE	1090	
83105	023P40	83106	0	23100	23	5 29L 3432T0	0BASE	1091	
			4	23100		T23100 TROUBLESHOOT AND TRIM TEST CELL	0BASE	1092	
83105	T23102	83106	0	23100	23	50 29L 4432T0	0BASE	1093	
			4	23100		T23100 TEND AND SOAP TEST CELL	0BASE	1094	
83105	T23102	83106	E	65	23100	23	5 29L 4432T0	0BASE	1095
83105	023P40	83106	E	35	23100	23		0BASE	1096
83105	023P40	83106	0	23100	23		0BASE	1097	
83105	SHOP	83106	0	23100	23		0BASE	1098	
83105	DTOW23	83106	0	23100	23		0BASE	1099	
			4	23100		M23100 FINAL SHOP WORK GOOD ENGINE OUT	0BASE	1100	
83105	M23100	83106	0	23100	23	40 29L 4432X0	0BASE	1101	
83105	DTOW23	83106	0	23100	23		0BASE	1102	
			4	23100		M23100 ENGINE SHOP WORK	0BASE	1103	
83105	M23100	83106	0	23100	23	50 29L 4432X0	0BASE	1104	
			4	23100		M23100 ENGINE SHOP WORK	0BASE	1105	
83105	M23100	83106	E	90	23100	23	60 29L 4432X0	0BASE	1106
			4	23100		M23100 ENGINE SHOP WORK	0BASE	1107	
83105	M23100	83106	E	10	23100	23	320 29L 4432X0	0BASE	1108
			4	23100		INLET FAN MODULE	0BASE	1109	
83105	L23100	83106	E	10516	23100	23		0BASE	1110
83105	L23100	83106	E	27	23100	23	40 29L 3432X0	0BASE	1111
83105	M23100	83106	E	2	23100	23	22 29L 1431X1	0BASE	1112
83105	M23100	83106	E	55	23100	23	5 29L 2432X0	0BASE	1113
83105	M23100	83106	E	04	23100	23	5 29L 2432T0	0BASE	1114
83105	L23100	83106	0	23100	21		0BASE	1115	
			4	23100		CORE ENGINE MODULE	0BASE	1116	
83105	L23100	83106	E	03967	23100	23		0BASE	1117
83105	M23100	83106	E	10	23100	23	13 29L 1432X0	0BASE	1118
83105	M23100	83106	E	15	23100	23	16 29L 1432X0	0BASE	1119

84431	0034H7	84431	0	24400	21		0BASE	1186
84431	0034H7	84431	0	24400	21		0BASE	1187
84431	0034H7	84431	0	24400	21	25 29L 1-23X0 1-32X0 1-31X1	0BASE	1188
84431	0034H7	84431	0	24400	21	3 29L 1-31X1	0BASE	1189
84431	0034H7	84431	0	24400	21	4 29L 2-31X1	0BASE	1190
84431	0034H7	84431	0	24400	21	33 29L 2-32X1 1TJ225	0BASE	1191
84431	0034H7	84431	0	24400	21	17 29L 2-31X2 1TJ225	0BASE	1192
84431	0034H7	84431	0	24400	21	15 29L 2-32X1 1TJ225	0BASE	1193
84431	0034H7	84431	0	24400	21	24 29L 1-32X0	0BASE	1194
84431	0034H7	84431	0	24400	21	33 29L 2-32X1	0BASE	1195
84431	0034H7	84431	0	24400	21	21 29L 2-32X0	0BASE	1196
84431	0034H7	84431	0	24400	23		0BASE	1197
84431	0034H7	84431	0	24400	23		0BASE	1198
84431	0034H7	84431	0	24400	23	JFS SYS	0BASE	1199
84431	0034H7	84431	0	24400	23	15 29L 1-32X0	0BASE	1200
84431	0034H7	84431	0	24400	23	ACC OF GEARBOXES	0BASE	1201
84431	0034H7	84431	0	24400	23	F15 DATA USED	0BASE	1202
84431	0034H7	84431	0	24400	23	NO WAY TO TEST 44405	0BASE	1203
84431	0034H7	84431	0	24400	23	NEA PTO SHAFT SEAL IS WORKING	0BASE	1204
84431	0034H7	84431	0	24400	23	MSBMA ACC FROM 25 TO 75 FOR CORREC-	0BASE	1205
84431	0034H7	84431	0	24400	23	TIVE ACTIONS	0BASE	1206
84431	0034H7	84431	0	24400	23	ACC OF GEARBOX F15	0BASE	1207
84431	0034H7	84431	0	24400	21		0BASE	1208
84431	0034H7	84431	0	24400	21		0BASE	1209
84431	0034H7	84431	0	24400	21	5 29L 1-31X1	0BASE	1210
84431	0034H7	84431	0	24400	21		0BASE	1211
84431	0034H7	84431	0	24400	21	20 29L 2-31X1	0BASE	1212
84431	0034H7	84431	0	24400	21	24 29L 2-32X0 1TJ225	0BASE	1213
84431	0034H7	84431	0	24400	21	10 29L 1-31X1	0BASE	1214
84431	0034H7	84431	0	24400	21	23 29L 2-32X0 1TJ225	0BASE	1215
84431	0034H7	84431	0	24400	23		0BASE	1216
84431	0034H7	84431	0	24400	23		0BASE	1217
84431	0034H7	84431	0	24400	23	ACC OF GEARBOX	0BASE	1218
84431	0034H7	84431	0	24400	23	15 29L 1-32X0	0BASE	1219
84431	0034H7	84431	0	24400	21	23 29L 2-32X1	0BASE	1220
84431	0034H7	84431	0	24400	21	JFS STARTING SYS	0BASE	1221
84431	0034H7	84431	0	24400	21	NO COMPATIBILITY AVAILABLE	0BASE	1222
84431	0034H7	84431	0	24400	21	USED F15 DATA	0BASE	1223
84431	0034H7	84431	0	24400	21	JFS START SYS F15	0BASE	1224
84431	0034H7	84431	0	24400	21		0BASE	1225
84431	0034H7	84431	0	24400	21	14 29L 2-31X2 1TJ225 1-31X1	0BASE	1226
84431	0034H7	84431	0	24400	23		0BASE	1227
84431	0034H7	84431	0	24400	23		0BASE	1228
84431	0034H7	84431	0	24400	23	JFS START SYS	0BASE	1229
84431	0034H7	84431	0	24400	23	22 29L 2-31X2	0BASE	1230
84431	0034H7	84431	0	24400	21		0BASE	1231
84431	0034H7	84431	0	41400	21	ENV CONT SYS	0BASE	1232
84431	0034H7	84431	0	41400	21	MSG DEVLAF10K LUKE ENV FM 2701	0BASE	1233
84431	0034H7	84431	0	41400	21	SGG JAMES EDWARDS ENV	0BASE	1234
84431	0034H7	84431	0	41400	21	F15 DATA USED	0BASE	1235
84431	0034H7	84431	0	41400	21	ENV CONT SYS F15	0BASE	1236
84431	0034H7	84431	0	41400	21		0BASE	1237
84431	0034H7	84431	0	41400	21	13 29L 2-32X1 1-31X1	0BASE	1238
84431	0034H7	84431	0	41400	21	24 29L 2-32X1	0BASE	1239
84431	0034H7	84431	0	41400	21	27 29L 1-32X1	0BASE	1240
84431	0034H7	84431	0	41400	21	82 29L 2-31X2	0BASE	1241
84431	0034H7	84431	0	41400	23		0BASE	1242
84431	0034H7	84431	0	41400	23		0BASE	1243
84431	0034H7	84431	0	41400	23	PLEED / SERVICE AIR	0BASE	1244
84431	0034H7	84431	0	41400	23	16 29L 1-32X1	0BASE	1245
84431	0034H7	84431	0	41400	21		0BASE	1246
84431	0034H7	84431	0	41400	23		0BASE	1247
84431	0034H7	84431	0	41400	23	AVN EOP COOLING	0BASE	1248
84431	0034H7	84431	0	41400	23	20 29L 1-32X1	0BASE	1249
84431	0034H7	84431	0	41400	21		0BASE	1250
84431	0034H7	84431	0	41400	21		0BASE	1251

10501	L-5000	4	45000	NO 2 HYD SYS PWR	09ASE 1334
10502	4-5000	3	45000*23	26 29L 2-21Y2	09ASE 1335
10503	4-5000	3	45000*23	15 29L 1-21Y2	09ASE 1336
10504	4-5000	3	45000*23	15 29L 1-21Y2	09ASE 1337
10505	Q-5000	1	45000 21	29 29L 2-21Y2	09ASE 1338
			45000	UTILITY HYD SYS	09ASE 1339
		M	45000	F4E 4513 F11F 45A2A 2 FOR 4500E /	09ASE 1390
		M	45000	45000	09ASE 1391
		M	45000	F15 MSRNA 31	09ASE 1392
		M	45000	EXPECTED TO BE CORRE UNLESS AMAD SYS	09ASE 1393
		M	45000	PROBLEMS CORRECTED	09ASE 1394
		M	45000	UTILITY HYD SYS F15	09ASE 1395
05001	F-5000	05001	F	23 45000 21	09ASE 1396
05002	4-5000	05002	F	45000 21	09ASE 1397
05003	CALIT	05003	F	45000 21	09ASE 1398
05004	4-5000	05004	F	26 45000 21	09ASE 1399
05005	4-5000	05005	F	67 45000 21	09ASE 1400
05006	4-5000	05006	F	67 45000 21	09ASE 1401
05007	4-5000	05007	F	61 45000 21	09ASE 1402
05008	4-5000	05008	F	61 45000 21	09ASE 1403
05009	4-5000	05009	F	62 45000 21	09ASE 1404
05010	4-5000	05010	F	62 45000 21	09ASE 1405
05011	4-5000	05011	F	62 45000 21	09ASE 1406
05012	4-5000	05012	F	62 45000 21	09ASE 1407
	L-5000	4	45000	UTILITY HYD SYS	09ASE 1408
10501	4-5000	3	45000*23	26 29L 2-21Y2	09ASE 1409
10502	4-5000	3	45000*23	15 29L 1-21Y2	09ASE 1410
10503	4-5000	3	45000*23	15 29L 1-21Y2	09ASE 1411
10504	4-5000	3	45000*23	13 29L 2-21Y2	09ASE 1412
10505	4-5000	3	45000*23	13 29L 2-21Y2	09ASE 1413
		4	46000	INTERNAL FUEL SYS	09ASE 1414
		4	46000	F4E 451 DATA USED	09ASE 1415
		4	46000	TSS POOLE LUKE INST	09ASE 1416
		4	46000	MSG WILLIAMS LUKE FUEL	09ASE 1417
		4	46000	SSG PRIN LUKE FUEL	09ASE 1418
		M	46000	F15 MSRNA 115	09ASE 1419
		4	46000	INTERNAL FUEL SYS F15	09ASE 1420
06A01	F-5000	06A01	F	32 46000 21	09ASE 1421
06A02	0044Y	06A02	F	56 46000 21	09ASE 1422
06A03	FUEL	06A03	F	46000 21	09ASE 1423
06A04	0FUEL	06A04	F	46000 21	09ASE 1424
06A05	4-5000	06A05	F	20 46000 21	09ASE 1425
06A06	4-5000	06A06	F	51 46000 21	09ASE 1426
06A07	4-5000	06A07	F	21 46000 21	09ASE 1427
06A08	0044Y	06A08	F	44 46000 21	09ASE 1428
06A09	4-5000	06A09	F	33 46000 21	09ASE 1429
06A10	4-5000	06A10	F	33 46000 21	09ASE 1430
06A11	4-5000	06A11	F	34 46000 21	09ASE 1431
06A12	0044Y	06A12	F	46000 21	09ASE 1432
06A13	4-5000	06A13	F	46000 21	09ASE 1433
06A14	4-5000	06A14	F	46000 21	09ASE 1434
06A15	4-5000	06A15	F	46000 21	09ASE 1435
06A16	4-5000	06A16	F	46000 21	09ASE 1436
06A17	4-5000	06A17	F	46000 21	09ASE 1437
06A18	4-5000	06A18	F	46000 21	09ASE 1438
06A19	4-5000	06A19	F	46000 21	09ASE 1439
06A20	4-5000	06A20	F	46000 21	09ASE 1440
06A21	4-5000	06A21	F	46000 21	09ASE 1441
06A22	4-5000	06A22	F	46000 21	09ASE 1442
06A23	4-5000	06A23	F	46000 21	09ASE 1443
06A24	4-5000	06A24	F	46000 21	09ASE 1444
06A25	4-5000	06A25	F	46000 21	09ASE 1445
06A26	4-5000	06A26	F	46000 21	09ASE 1446
06A27	4-5000	06A27	F	46000 21	09ASE 1447
06A28	4-5000	06A28	F	46000 21	09ASE 1448
06A29	4-5000	06A29	F	46000 21	09ASE 1449
06A30	4-5000	06A30	F	46000 21	09ASE 1450
06A31	4-5000	06A31	F	46000 21	09ASE 1451
06A32	4-5000	06A32	F	46000 21	09ASE 1452
06A33	4-5000	06A33	F	46000 21	09ASE 1453
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06A35	4-5000	06A35	F	46000 21	09ASE 1455
06A36	4-5000	06A36	F	46000 21	09ASE 1456
06A37	4-5000	06A37	F	46000 21	09ASE 1457
06A38	4-5000	06A38	F	46000 21	09ASE 1458
06A39	4-5000	06A39	F	46000 21	09ASE 1459
06A40	4-5000	06A40	F	46000 21	09ASE 1460
06A41	4-5000	06A41	F	46000 21	09ASE 1461
06A42	4-5000	06A42	F	46000 21	09ASE 1462
06A43	4-5000	06A43	F	46000 21	09ASE 1463
06A44	4-5000	06A44	F	46000 21	09ASE 1464
06A45	4-5000	06A45	F	46000 21	09ASE 1465
06A46	4-5000	06A46	F	46000 21	09ASE 1466
06A47	4-5000	06A47	F	46000 21	09ASE 1467
06A48	4-5000	06A48	F	46000 21	09ASE 1468
06A49	4-5000	06A49	F	46000 21	09ASE 1469
06A50	4-5000	06A50	F	46000 21	09ASE 1470
06A51	4-5000	06A51	F	46000 21	09ASE 1471
06A52	4-5000	06A52	F	46000 21	09ASE 1472
06A53	4-5000	06A53	F	46000 21	09ASE 1473
06A54	4-5000	06A54	F	46000 21	09ASE 1474
06A55	4-5000	06A55	F	46000 21	09ASE 1475
06A56	4-5000	06A56	F	46000 21	09ASE 1476
06A57	4-5000	06A57	F	46000 21	09ASE 1477
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06A59	4-5000	06A59	F	46000 21	09ASE 1479
06A60	4-5000	06A60	F	46000 21	09ASE 1480
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06A62	4-5000	06A62	F	46000 21	09ASE 1482
06A63	4-5000	06A63	F	46000 21	09ASE 1483
06A64	4-5000	06A64	F	46000 21	09ASE 1484
06A65	4-5000	06A65	F	46000 21	09ASE 1485
06A66	4-5000	06A66	F	46000 21	09ASE 1486
06A67	4-5000	06A67	F	46000 21	09ASE 1487
06A68	4-5000	06A68	F	46000 21	09ASE 1488
06A69	4-5000	06A69	F	46000 21	09ASE 1489
06A70	4-5000	06A70	F	46000 21	09ASE 1490
06A71	4-5000	06A71	F	46000 21	09ASE 1491
06A72	4-5000	06A72	F	46000 21	09ASE 1492
06A73	4-5000	06A73	F	46000 21	09ASE 1493
06A74	4-5000	06A74	F	46000 21	09ASE 1494
06A75	4-5000	06A75	F	46000 21	09ASE 1495
06A76	4-5000	06A76	F	46000 21	09ASE 1496
06A77	4-5000	06A77	F	46000 21	09ASE 1497
06A78	4-5000	06A78	F	46000 21	09ASE 1498
06A79	4-5000	06A79	F	46000 21	09ASE 1499
06A80	4-5000	06A80	F	46000 21	09ASE 1500

06801	F+6801	06901	F	355	4681L	21		03ASE	1451
06802	072427	06902	E	40	4682L	21		03ASE	1452
06803	CALGPJ	06903	C		4683L	21		03ASE	1453
06804	072427	06904	C		4684L	21	45 29L 2424X0 1060	03ASE	1454
06805	072427	06905	C		4685L	21	45 29L 2424X0 1060	03ASE	1455
06806	072427	06906	C		4686L	21	17 29L 5431X1	03ASE	1456
06807	072427	06907	C		4687L	21	18 29L 2432X1	03ASE	1457
06808	072427	06908	C		4688L	21	11 29L 1531X0	03ASE	1458
06809	072427	06909	C		4689L	21	13 29L 2531X3	03ASE	1459
06810	072427	06910	C		4690L	23		03ASE	1460
06811	072427	06911	C		4691L	23	EXTERNAL WG TANKS	03ASE	1461
06812	072427	06912	C		4692L	23	57 29L 2424X0	03ASE	1462
06813	072427	06913	C		4693L	23	14 29L 2424X0	03ASE	1463
06814	072427	06914	C		4694L	23	06 29L 1424X0	03ASE	1464
06815	072427	06915	C		4695L	23	23 29L 2531X0	03ASE	1465
06816	072427	06916	C		4696L	23	09 29L 1531X1	03ASE	1466
06817	072427	06917	C		4697L	23	21 29L 2531X3	03ASE	1467
06818	072427	06918	C		4698L	23	03 29L 2536X0	03ASE	1468
06819	072427	06919	C		4699L	23		03ASE	1469
06820	072427	06920	C		4700L	23	REFUEL NTWK	03ASE	1470
06821	072427	06921	C		4701L	23	F4E 4631 DATA USED	03ASE	1471
06822	072427	06922	C		4702L	23	F15 MSGMA NO FAILURE	03ASE	1472
06823	072427	06923	C		4703L	23	REFUEL SYS F15	03ASE	1473
06824	072427	06924	C		4704L	23		03ASE	1474
06825	072427	06925	C		4705L	23		03ASE	1475
06826	072427	06926	C		4706L	23		03ASE	1476
06827	072427	06927	C		4707L	23		03ASE	1477
06828	072427	06928	C		4708L	23		03ASE	1478
06829	072427	06929	C		4709L	23	16 29L 2423X0 1424X0 170228 1060	03ASE	1479
06830	072427	06930	C		4710L	23	60 29L 2424X0 1060 170228	03ASE	1480
06831	072427	06931	C		4711L	23	15 29L 2424X0 1060 170228 1431X1	03ASE	1481
06832	072427	06932	C		4712L	23	16 29L 2424X0 1060 170228	03ASE	1482
06833	072427	06933	C		4713L	23	30 29L 2421X2 1060 170228	03ASE	1483
06834	072427	06934	C		4714L	23	60 29L 2424X0	03ASE	1484
06835	072427	06935	C		4715L	23	18 29L 2424X0 1431X1	03ASE	1485
06836	072427	06936	C		4716L	23	22 29L 2424X0	03ASE	1486
06837	072427	06937	C		4717L	23	27 29L 2531X3	03ASE	1487
06838	072427	06938	C		4718L	23		03ASE	1488
06839	072427	06939	C		4719L	23		03ASE	1489
06840	072427	06940	C		4720L	23	AIR REFUEL SYS	03ASE	1490
06841	072427	06941	C		4721L	23	15 29L 1531X0	03ASE	1491
06842	072427	06942	C		4722L	23	10 29L 1421X2	03ASE	1492
06843	072427	06943	C		4723L	23	10 29L 1424X0	03ASE	1493
06844	072427	06944	C		4724L	23		03ASE	1494
06845	072427	06945	C		4725L	23	FUEL CONT & WING INDICATING SYS	03ASE	1495
06846	072427	06946	C		4726L	23	F4E 464	03ASE	1496
06847	072427	06947	C		4727L	23	FUEL CONT & WG INDICATING SYS F15	03ASE	1497
06848	072427	06948	C		4728L	23		03ASE	1498
06849	072427	06949	C		4729L	23		03ASE	1499
06850	072427	06950	C		4730L	23		03ASE	1500
06851	072427	06951	C		4731L	23	10 29L 2326X2 1060	03ASE	1501
06852	072427	06952	C		4732L	23	42 29L 2424X0	03ASE	1502
06853	072427	06953	C		4733L	23	14 29L 2424X0 1431X1	03ASE	1503
06854	072427	06954	C		4734L	23		03ASE	1504
06855	072427	06955	C		4735L	23		03ASE	1505
06856	072427	06956	C		4736L	23	FUEL CONT & WG IND SYS	03ASE	1506
06857	072427	06957	C		4737L	23	03 29L 1424X0	03ASE	1507
06858	072427	06958	C		4738L	23	25 29L 2326X1	03ASE	1508
06859	072427	06959	C		4739L	23	10 29L 2326X1	03ASE	1509
06860	072427	06960	C		4740L	23		03ASE	1510
06861	072427	06961	C		4741L	23	THE FOL IS LOX NTWK	03ASE	1511
06862	072427	06962	C		4742L	23	F11F 47A DATA USED	03ASE	1512
06863	072427	06963	C		4743L	23	LOX F15	03ASE	1513
07A01	F+7A01	07A01	F	61	47A01	21		03ASE	1514
07A02	R47A02	07A02	E	47	47A02	21	11 29L 2422X1	03ASE	1515

07A01	07A01	07A02	E	12	47A00	21	15	29L	132632	08ASE	1516
07A01	07A02	07A02	E	21	47A01	21	15	29L	132632	09ASE	1517
07A01	07A03	07A03	E	3	47A01	21	9	29L	2422X1	08ASE	1519
07A01	07A03	07A03	E	3	47A02	21	10	29L	232632	09ASE	1519
07A03	07A03	07A03	O		47A03	21	05	29L	2422X1	09ASE	1521
07A03	07A03	07A03	E	04	47A03	21	5	29L	1-31X1	09ASE	1521
07A02	07A03	07A03	O		47A03	23				08ASE	1522
07A03	07A03	07A03	O		47A04	23				08ASE	1523
	07A03	07A03	4		47A00				LCX SYS	09ASE	1524
07A03	07A03	07A03	E	11	47A03*23		21	29L	2-22X1	09ASE	1525
07A03	07A03	07A03	E	09	47A03*23		17	29L	1-22X1	09ASE	1526
07A03	07A03	07A03	I		47A04	21	5	29L	2431X1	09ASE	1527
			4		49A00				FIRE DETECT & WARNING SYS	09ASE	1528
			4		49A00				FIRE DETECT & WARNING ENG & AMMO BAY	09ASE	1529
			M		49A00				FIRE DETECT & WARNING ENG & AMMO BAY	09ASE	1530
09A01	09A01	09A01	E	05	49A00	21				09ASE	1531
09A01	09A02	09A02	O		49A00	21	24	29L	2423X0	08ASE	1532
09A02	09A02	09A02	E	46	49A00	21	13	29L	2423X0	09ASE	1533
09A02	09A02	09A02	E	33	49A00	21	19	29L	1423X0	09ASE	1534
09A02	09A02	09A02	E	03	49A00	21	11	29L	1-31X1	09ASE	1535
09A02	09A02	09A02	E	17	49A00	21	06	29L	2-31X1	09ASE	1536
09A03	09A03	09A03	O		49A00	21	08	29L	1-23X0	09ASE	1537
09A03	09A03	09A03	O		49A00	21				08ASE	1538
			4		51A00				THIS IS LAUNCH FOR 51A00 AP58	09ASE	1539
51A00	51A00	51A00	E	15	51A00	21				08ASE	1540
51A00	51A00	51A00	E	10	51A00	21	4	29L	1326L2	09ASE	1541
51A00	51A00	51A00	E	06	51A00	21	2	29L	1326L2	08ASE	1542
51A00	51A00	51A00	E	10	51A00	21	2	29L	1326L2	08ASE	1543
51A00	51A00	51A00	E	14	51A00	21	3	29L	1326L2	08ASE	1544
51A00	51A00	51A00	E	05	51A00	21	3	29L	1326L2	09ASE	1545
51A00	51A00	51A00	E	15	51A00	21	3	29L	1326L2	08ASE	1546
			4		51A00				VERIFIED BY IS POOLE USE F15 DATA	08ASE	1547
			4		51A00				F15 INSTRUMENTS 51A00	09ASE	1548
51A00	51A00	51A00	E	50	51A00	21				08ASE	1549
51A00	51A00	51A00	O		51A00	21				08ASE	1550
51A00	51A00	51A00	O		51A00	21				09ASE	1551
51A02	51A02	51A02	E	75	51A00	21	15	29L	232632 1060 105	09ASE	1552
51A02	51A02	51A02	E	25	51A00	21	15	29L	232632 1-31X1 1050 105	09ASE	1553
51A03	51A03	51A03	O		51A00	23				08ASE	1554
			4		51A00				FOR SEPARATE CAPABILITY TO MARTIN FEELS	08ASE	1555
			M		51A00				AUTOMATIC TEST STATION FEELS	08ASE	1556
			4		51A00				THAT ITEMS THAT ARE NOTS ONLY WILL BE	08ASE	1557
			M		51A00				ABOUT 90 PERCENT N ACTIONS	08ASE	1558
			4		51A00				G CODE COMP DATA F11F	08ASE	1559
			M		51A00				F15 INSTRUMENT MOST HAVE NO SHOP DATA	08ASE	1560
51A00	51A00	51A00	E	10549	51A00	23				08ASE	1561
51A00	51A00	51A00	E		51A00	21	10	29L	232632 1050 105	08ASE	1562
51A00	51A00	51A00	O		51A00*23					08ASE	1563
51A00	51A00	51A00	O		51A00	23				08ASE	1564
51A02	51A00	51A00	E	10	51A00	23	15	29L	132641 1PTS24	08ASE	1565
51A02	51A00	51A00	E	90	51A00	23	5	29L	132641 1PTS24	08ASE	1566
51A02	51A00	51A00	O	10238	51A00	23				08ASE	1567
			4		51A00				F15 AIRSPEED IND 51A00 G FROM F15	08ASE	1568
51A00	51A00	51A00	E	10	51A00*23		22	29L	132641	08ASE	1569
51A00	51A00	51A00	E	90	51A00*23		15	29L	132641	08ASE	1570
51A00	51A00	51A00	O		51A00	21	10	29L	232632 1060 105	08ASE	1571
51A00	51A00	51A00	O	10017	51A00	23				08ASE	1572
			4		51A00				F15 VERTICAL SPEED IND 51A00 G NO DATA	08ASE	1573
51A00	51A00	51A00	E	10	51A00*23		15	29L	132641	08ASE	1574
51A00	51A00	51A00	E	90	51A00*23		15	29L	132641	08ASE	1575
51A00	51A00	51A00	O		51A00	21	10	29L	232632 1060 105	08ASE	1576
51A00	51A00	51A00	O	10119	51A00	23				08ASE	1577
			4		51A00				F15 STAY AIRSPEED IND 51A00 G FROM F15	08ASE	1578
51A00	51A00	51A00	E		51A00	21	20	29L	232632 1060 105	08ASE	1579
51A00	51A00	51A00	O		51A00*23					08ASE	1580
51A00	51A00	51A00	O		51A00	23				08ASE	1581

IE1A02	N51A00	E	9	51A00	23	10 29L 132641 1PTS2	03ASE	1592
IE1A02	N51A00	E	1	51A00	23	5 29L 132641 1PTS2	03ASE	1593
SE1A00	N51A00	G	1169	51A00	23		03ASE	1594
		M		51A00	23	F15 PRESSURE ALTIMETER 51A00 G-F111F	03ASE	1595
IE1A40	N51A00	I		51A00	21	20 29L 232632 1060 105	03ASE	1596
IE1A40	N51A00	I		51A00	23		03ASE	1597
IE1A40	N51A00	I		51A00	23		03ASE	1598
IE1A42	N51A00	E	1	51A00	23	10 29L 132641 1PTS1	03ASE	1599
IE1A42	N51A00	E	9	51A00	23	5 29L 132641 1PTS1	03ASE	1600
SE1A00	N51A00	G	10290	51A00	23		03ASE	1601
		M		51A00	23	F15 STRY GYRO INC G FROM F5E	03ASE	1602
IE1A00	N51A00	I		51A00	21	20 29L 232632 1060 105	03ASE	1603
IE1A00	N51A00	I		51A00	23		03ASE	1604
IE1A00	N51A00	I		51A00	23		03ASE	1605
IE1A02	N51A00	E	1	51A00	23	30 29L 132641 1PTS10	03ASE	1606
IE1A02	N51A00	E	9	51A00	23	30 29L 132641 1PTS10	03ASE	1607
SE1A00	N51A00	G	10180	51A00	23		03ASE	1608
		M		51A00	23	F15 ALTITUDE INC 51A00 G FROM F5E	03ASE	1609
IE1A00	N51A00	E	1	51A00	23	15 29L 132641	03ASE	1610
IE1A00	N51A00	E	9	51A00	23	10 29L 132641	03ASE	1611
IE1A00	N51A00	I		51A00	21	10 29L 232632 1060 105	03ASE	1612
SE1A00	N51A00	G	10110	51A00	23		03ASE	1613
		M		51A00	23	F15 ANGLE OF ATTACK INC 51A00 G NO DATA	03ASE	1614
IE1A00	N51A00	E	1	51A00	23	15 29L 132631	03ASE	1615
IE1A00	N51A00	E	9	51A00	23	10 29L 132631	03ASE	1616
IE1A00	N51A00	I		51A00	21	10 29L 232632 1060 105	03ASE	1617
SE1A00	N51A00	G	10197	51A00	23		03ASE	1618
		M		51A00	23	F15 ACCELEROMETER INC 51A00 G FROM F4E	03ASE	1619
IE1A40	N51A00	I		51A00	21	10 29L 232632 1060 105	03ASE	1620
IE1A40	N51A00	I		51A00	23		03ASE	1621
IE1A40	N51A00	I		51A00	23		03ASE	1622
IE1A42	N51A00	E	1	51A00	23	10 29L 132641 1PTS26	03ASE	1623
IE1A42	N51A00	E	9	51A00	23	5 29L 132641 1PTS26	03ASE	1624
		M		51E00	23	F111F AND F4E DATA USED	03ASE	1625
		M		51E00	23	VERIFIED BY TS POOLE IF PROBE FIXED	03ASE	1626
		M		51E00	23	F15 AIR DATA SYS 51E00 F15=40	03ASE	1627
E1E00	F51E00	E	51	51E00	21		03ASE	1628
E1E00	F51E00	E	51	51E00	21		03ASE	1629
E1E00	F51E00	E	51	51E00	21		03ASE	1630
E1E02	F51E00	E	6	51E00	21	15 29L 232632 1060 105	03ASE	1631
E1E02	F51E00	E	40	51E00	21	10 29L 1431X1 1060 105	03ASE	1632
E1E02	F51E00	E	40	51E00	21	10 29L 1431X1 1060 105	03ASE	1633
SE1E00	N51E00	G	11190	51E00	23		03ASE	1634
		M		51E00	23	USED FOR G SELECT WORK AROUND	03ASE	1635
		M		51E00	23	F111F 52344 FOR E SEL AND TIMES	03ASE	1636
		M		51E00	23	F15 AIR DATA COMPUTER 51E00 F15 DATA	03ASE	1637
IE1E00	N51E00	I		51E00	21	20 29L 232632 1060 105	03ASE	1638
IE1E00	N51E00	I		51E00	23		03ASE	1639
IE1E00	N51E00	I		51E00	23		03ASE	1640
IE1E02	N51E00	E	42	51E00	23	10 29L 132641 1PTS25 1TSC	03ASE	1641
IE1E02	N51E00	E	45	51E00	23	45 29L 132641 1PTS25 1TSC	03ASE	1642
IE1E02	N51E00	E	49	51E00	23	89 29L 132641 1PTS25 1TSC	03ASE	1643
SE1E00	N51E00	G	10250	51E00	23		03ASE	1644
		M		51E00	23	F4E 51330 DATA USED	03ASE	1645
		M		51E00	23	F15 ANGLE OF ATTACK TRANS 51E00	03ASE	1646
IE1E00	N51E00	E	10	51E00	23	15 29L 132641	03ASE	1647
IE1E00	N51E00	E	9	51E00	23	10 29L 132641	03ASE	1648
IE1E00	N51E00	I		51E00	21	20 29L 232632 1060 105	03ASE	1649
		M		51M00	23	VERIFIED BY TS POOLE SUGGEST NO SWING	03ASE	1650
		M		51M00	23	F15 STRY COMPASS 51M00 F111F USED	03ASE	1651
E1M00	F51M00	E	42	51M00	21		03ASE	1652
E1M00	F51M00	E	42	51M00	21		03ASE	1653
E1M00	F51M00	E	42	51M00	21		03ASE	1654
E1M02	F51M00	E	60	51M00	21	40 29L 232632 1060 105	03ASE	1655
E1M02	F51M00	E	40	51M00	21	10 29L 1431X1 1060 105	03ASE	1656
E1M03	F51M00	E	40	51M00	21	10 29L 1431X1 1060 105	03ASE	1657

SE1M30	LS1M30	IE1M30	0	51M00	23				DBASE 1648
			4	51M00		F111F DATA USED			DBASE 1649
			4	51M00		F15 STBY COMPASS 51M00			DBASE 1650
IE1M30	OS1M30		I	51M00	21	40 29L 232632 1060	105		DBASE 1651
IE1M30	OS1M30		0	51M00	23				DBASE 1652
			4	51M00		VERIFIED BY TS POOLE SET CLOCK=75			DBASE 1653
			4	51M00		F15 INDICATOR SET 51M00 F15=20			DBASE 1654
51M01	OS1M01	51M01	F	27	51M01	21			DBASE 1655
51M01	OS1M01	51M01	0	51M01	21				DBASE 1656
51M01	OS1M01	51M01	0	51M01	21				DBASE 1657
51M02	OS1M02	51M02	E	29	51M02	21	20 29L 232632 1060	105	DBASE 1658
51M02	OS1M02	51M02	E	13	51M02	21	13 29L 143141 1260	105	DBASE 1659
51M02	OS1M02	51M02	E	52	51M02	21	10 29L 232632 1060	105	DBASE 1660
51M03	OS1M03	51M03	0	51M03	23				DBASE 1661
SE1M30	LS1M30	IE1M30	G	0119	51M00	23			DBASE 1662
			4	51M01		F SEL AND TIMES FM IS ROUGHARD			DBASE 1663
			4	51M00		F15 HORIZ SITUATION IND 51M01 G=F15			DBASE 1664
IE1M30	OS1M30		I	51M01	21	15 29L 232632 1060	105		DBASE 1665
IE1M30	OS1M30	IE1M30	0	51M00	23				DBASE 1666
IE1M30	OS1M30	IE1M30	0	51M02	23				DBASE 1667
IE1M32	OS1M32		E	10	51M03	23	20 29L 132641 1PT540 1T50		DBASE 1668
IE1M32	OS1M32		E	01	51M03	23	20 29L 132641 1PT540 1T50		DBASE 1669
SE1M30	LS1M30	IE1M30	G	05595	51M00	23			DBASE 1670
			4	51M01		TIMES FM F111F 51M01			DBASE 1671
			4	51M01		THIS IS WORK AROUND			DBASE 1672
			4	51M00		F15 FLT DIRECTOR ADAPTOR 51M01 G=F15			DBASE 1673
IE1M30	OS1M30		I	51M00	21	15 29L 232632 1060	105		DBASE 1674
IE1M30	OS1M30	IE1M30	0	51M01	23				DBASE 1675
IE1M30	OS1M30	IE1M30	0	51M00	23				DBASE 1676
IE1M30	OS1M30		E	1	51M00	23	25 29L 132641 1PT540 1T50		DBASE 1677
IE1M32	OS1M32		E	97	51M03	23	26 29L 132641 1PT540 1T50		DBASE 1678
			4	52A00		DATA 52A00-52A00-52A00 USED FOR MSEA			DBASE 1679
			4	52A00		F15 DATA AUG-75 MSEA 420 CK 170			DBASE 1680
			4	52A00		VERIFIED BY TS POOLE			DBASE 1681
			4	52A00		F15 AUTO FLT CONT SET ASW35 F111F			DBASE 1682
E2A01	OS2A01	E2A01	F	35	52A01	21			DBASE 1683
E2A01	OS2A01	E2A01	0	52A00	21				DBASE 1684
E2A01	OS2A01	E2A01	0	52A01	21				DBASE 1685
E2A02	OS2A02	E2A02	E	74	52A00	21	24 29L 232632 1060	1TU228	DBASE 1686
E2A02	OS2A02	E2A02	E	5	52A01	21	10 29L 143141 1260	1TU228	DBASE 1687
E2A02	OS2A02	E2A02	E	12	52A00	21	15 29L 143141 1260	1TU228	DBASE 1688
E2A02	OS2A02	E2A02	E	17	52A00	21	17 29L 232632 1060	1TU228	DBASE 1689
E2A03	OS2A03	E2A03	0	52A00	23				DBASE 1690
SE2A01	LS2A01	IE2A01	G	00110	52A00	23			DBASE 1691
			4	52A00		TS ROUGHARD-THIS IS PRESENTLY WORK			DBASE 1692
			4	52A00		AROUND ITEM COULD NOT GIVE ESTIMATES			DBASE 1693
			4	52A00		F15 PITCH FLT CONT COMPUTER 52A00			DBASE 1694
IE2A01	OS2A01		I	52A01	21	25 29L 232632 1060	1TU228		DBASE 1695
IE2A01	OS2A01	IE2A01	0	52A00	23				DBASE 1696
IE2A01	OS2A01	IE2A01	0	52A01	23				DBASE 1697
IE2A02	OS2A02		E	33	52A00	23	23 29L 132641 1PT512 1T50		DBASE 1698
IE2A02	OS2A02		E	34	52A01	23	25 29L 132641 1PT512 1T50		DBASE 1699
IE2A02	OS2A02		E	33	52A00	23	40 29L 132641 1PT512 1T50		DBASE 1700
SE2A01	LS2A01	IE2A01	G	00110	52A00	23			DBASE 1701
			4	52A01		TS ROUGHARD-WORK AROUND			DBASE 1702
			4	52A01		F15 FOLL-YAW FLT CONT COMPUTER 52A01			DBASE 1703
IE2A01	OS2A01		I	52A01	21	25 29L 232632 1060	1TU228		DBASE 1704
IE2A01	OS2A01	IE2A01	0	52A00	23				DBASE 1705
IE2A01	OS2A01	IE2A01	0	52A00	23				DBASE 1706
IE2A02	OS2A02		E	33	52A00	23	40 29L 132641 1PT512 1T50		DBASE 1707
IE2A02	OS2A02		E	33	52A01	23	23 29L 132641 1PT512 1T50		DBASE 1708
IE2A02	OS2A02		E	34	52A00	23	25 29L 132641 1PT512 1T50		DBASE 1709
SE2A01	LS2A01	IE2A01	G	00110	52A00	23			DBASE 1710
			4	52A00		TS ROUGHARD GAVE TIME ESTIMATES BUT			DBASE 1711
			4	52A00		WAS UNSURE OF E SELECT AND M TASK			DBASE 1712
			4	52A00		USED F111F FOR THESE			DBASE 1713

IE2A7	052A0		4	52A00	F15 RATE SENSOR ASSY 52A00 G=F111F	ORASE	1714
IE2A7	052A0	I		52A00 21	25 29L 232692 1000 1T0228	ORASE	1715
IE2A00	052A00	IE2A01	0	52A00*23		ORASE	1716
IE2A01	052A00	IE2A02	0	52A00 23		ORASE	1717
IE2A02	052A00		E	43 52A00 23	20 29L 132641 1PTS4 1TSC	ORASE	1718
IE2A02	052A00		E	31 52A00 23	20 29L 132641 1PTS4 1TSC	ORASE	1719
IE2A02	052A00		E	27 52A00 23	20 29L 132641 1PTS4 1TSC	ORASE	1720
SE2A01	052A01	IE2A01	G	0011 52A00 23		ORASE	1721
			4	52A00	TS ROUGHARD GAVE TIME ESTIMATES G=F111F	ORASE	1722
			4	52A00	F15 ACCELEROMETER SENSOR ASSY 52A00	ORASE	1723
IE2A00	052A00	I		52A00 21	25 29L 232692 1000 1T0228	ORASE	1724
IE2A01	052A00	IE2A01	0	52A00*23		ORASE	1725
IE2A01	052A00	IE2A02	0	52A00 23		ORASE	1726
IE2A02	052A00		E	07 52A00 23	20 29L 132641 1PTS27 1TSC	ORASE	1727
IE2A02	052A00		E	21 52A00 23	20 29L 132641 1PTS27 1TSC	ORASE	1728
IE2A02	052A00		E	77 52A00 23	20 29L 132641 1PTS27 1TSC	ORASE	1729
SE2A01	052A01	IE2A01	G	0011 52A00 23		ORASE	1730
			4	52A00	TS ROUGHARD COULD NOT EST-NO W TASK	ORASE	1731
			4	52A00	F15 DYNAMIC PRESSURE SENSOR ASSY 52A00	ORASE	1732
IE2A00	052A00	I		52A00 21	25 29L 232692 1000 1T0228	ORASE	1733
IE2A00	052A00	IE2A01	0	52A00*23		ORASE	1734
IE2A01	052A00	IE2A02	0	52A00 23		ORASE	1735
IE2A02	052A00		E	17 52A00 23	5 29L 132641 1PTS17 1TSC	ORASE	1736
IE2A02	052A00		E	91 52A00 23	5 29L 132641 1PTS17 1TSC	ORASE	1737
			4	55A00	THIS IS LAUNCH FOR 55A00 AREA	ORASE	1738
55A00	055A00	55A01	E	42 55A00 21		ORASE	1739
55A01	055A00	IE5A01	0	55A00 21	3 29L 1326L2	ORASE	1740
			4	55A00	THERE IS NO COMP EQUIP F15 DATA USED	ORASE	1741
			4	55A00	THIS IS NETWORK FOR BIT ON F15 55A00	ORASE	1742
55A00	055A00	55A01	E	237 55A00 21		ORASE	1743
55A01	055A00	55A02	0	55A00 21		ORASE	1744
55A02	055A00	55A03	0	55A00 21		ORASE	1745
55A03	055A00	55A04	E	05 55A00 21	20 29L 232632 1000 105	ORASE	1746
55A04	055A00	55A05	E	5 55A00 21	20 29L 232692 1000 105	ORASE	1747
55A05	055A00	55A06	0	55A00 21		ORASE	1748
SE5A01	055A01	IE5A01	G	0011 55A00 23		ORASE	1749
			4	55A00	VERIFIED BY TS OBERLY	ORASE	1750
			4	55A00	F15 ASP 55A00	ORASE	1751
IE5A00	055A00	I		55A00*23	25 29L 132691	ORASE	1752
IE5A01	055A00		E	91 55A00*23	20 29L 132691	ORASE	1753
IE5A02	055A00		E	55A00 21	20 29L 232632 1000 105	ORASE	1754
SE5A01	055A01	IE5A01	G	0011 55A00 23		ORASE	1755
			4	55A00	VERIFIED BY TS OBERLY	ORASE	1756
			4	55A00	F15 BIT CONT 55A00	ORASE	1757
IE5A00	055A00	I		55A00*23	40 29L 132681	ORASE	1758
IE5A01	055A00		E	1 55A00*23	30 29L 132681	ORASE	1759
IE5A02	055A00		E	25 55A00*23	30 29L 132681	ORASE	1760
IE5A03	055A00		E	55A00 21	10 29L 232692 1000 105	ORASE	1761
			4	55A00	F111F 55A00 AND 55A01 ARE USED AS COMP DATA	ORASE	1762
			4	55A00	THIS IS NETWORK FOR F15 SIG DATA RECORD	ORASE	1763
55A00	055A00	55A01	E	65 55A00 21		ORASE	1764
55A01	055A00	55A02	0	55A00 21		ORASE	1765
55A02	055A00	55A03	0	55A00 21		ORASE	1766
55A03	055A00	55A04	0	55A00 21	10 29L 232632 1000 105	ORASE	1767
55A04	055A00	55A05	0	55A00 23		ORASE	1768
SE5A01	055A01	IE5A01	G	00357 55A00 23		ORASE	1769
			4	55A00	SELECT AND TASK TIME ESTIMATES GIVEN	ORASE	1770
			4	55A00	BY TSOT ROUGHARD CHECK F111F	ORASE	1771
			4	55A00	F15 SIG DATA RECORDER FROM F15 DATA	ORASE	1772
IE5A00	055A00	I		55A00 21	240 29L 232692	ORASE	1773
IE5A01	055A00	IE5A01	0	55A00*23		ORASE	1774
IE5A02	055A00	IE5A02	0	55A00 23		ORASE	1775
IE5A03	055A00		E	30 55A00 23	20 29L 232641 1PTS3 1TSC	ORASE	1776
IE5A04	055A00		E	30 55A00 23	05 29L 232641 1PTS3 1TSC	ORASE	1777
IE5A05	055A00		E	41 55A00 23	06 29L 232641 1PTS3 1TSC	ORASE	1778
SE5A01	055A01	IE5A01	G	00366 55A00 23		ORASE	1779

	4	55800	VERIFIED BY TS ROUCHARD	DBASE 1780
	M	55800	F15 CASSETTE FROM F111F 55AAA DATA	DBASE 1781
IES021 055800	I	55800 21	24 29L 232692	DBASE 1782
IES021 055800	I	55800*23		DBASE 1783
	4	55800	F111F 55A00 USED F15 MS9MA=213	DBASE 1784
	4	55800	VERIFIED BY TS POOLE 1733	DBASE 1785
	4	55800	F15 ACCELEROMETER COUNTER 55000	DBASE 1786
ES001 55800 55001 F	75	55000 21		DBASE 1787
ES001 00RMG7 55001 D		55000 21		DBASE 1788
ES001 00LGP2 55002 D		55000 21		DBASE 1789
ES002 055000 55003 E	97	55000 21	10 29L 232692 1060 105	DBASE 1790
	4	55000	F SELECT FROM F15 DATA	DBASE 1791
ES002 055000 55003 E	3	55000 21	10 29L 232692 1060 105	DBASE 1792
ES002 SHOP 55003 D		55000 23		DBASE 1793
SE5000 055000 IES001 0 0337		55000 23		DBASE 1794
	4	55000	F15 DATA USED NO F111F SHOP DATA	DBASE 1795
	4	55000	TASK TIME EST BY TS ROUCHARD	DBASE 1796
	4	55000	DIGITAL HEADOUT ELECT COUNTER 55000	DBASE 1797
IES001 055000	I	55000 21	25 29L 232692 1060 105	DBASE 1798
IES001 055000 IES001 D		55000*23		DBASE 1799
IES001 055000 IES002 D		55000 23		DBASE 1800
IES002 055000	E	5 55000 23	40 29L 132641 1PTS19 1TSC	DBASE 1801
IES002 055000	E	2 55000 23	25 29L 132641 1PTS19 1TSC	DBASE 1812
IES002 055000	E	97 55000 23	25 29L 132641 1PTS19 1TSC	DBASE 1813
SE5000 055000 IES000 0 01119		55000 23		DBASE 1814
	M	55000	F15 DATA USED NO F111F DATA AVAIL	DBASE 1815
	M	55000	NO M TASK TIME EST BY TS ROUCHARD	DBASE 1816
	M	55000	LINEAR ELECT ACCELEROMETER 55000	DBASE 1817
IES003 055000	I	55000 21	20 29L 232692 1060 105	DBASE 1818
IES003 055000 IES003 D		55000*23		DBASE 1819
IES003 055000 IES002 D		55000 23		DBASE 1820
IES003 055000	E	85 55000 23	10 29L 132641 1PTS16 1TSC	DBASE 1821
IES003 055000	E	15 55000 23	10 29L 132641 1PTS16 1TSC	DBASE 1822
	4	57000	THIS IS LAUNCH FOR 57000 AREA	DBASE 1823
57000 57000 57001 F	71	57000 21		DBASE 1824
57001 57000 57000 D		57000 21	2 29L 132642	DBASE 1825
	4	57000	THIS IS NETWORK FOR F15 CENTRAL	DBASE 1826
	4	57000	COMPUTER 57000 THERE IS NO COAP	DBASE 1827
	4	57000	DATA F15 DATA USED	DBASE 1828
	4	57000	VERIFIED BY TS FAY	DBASE 1829
	M	57000	F15 CENTRAL COMPUTER	DBASE 1830
57000 57000 57001 F	21	57000 21		DBASE 1831
57001 00RMG7 57001 D		57000 21		DBASE 1832
57001 00LGP2 57002 D		57000 21		DBASE 1833
57002 057000 57003 E	17	57000 21	8 29L 232642 1060 105 1431X1	DBASE 1834
57002 057000	E	83 57000 21	10 29L 232642 1060 105	DBASE 1835
57003 SHOP 57003 D		57000 23		DBASE 1836
SE5000 057000 IES001 0		57000 23		DBASE 1837
	4	57000	WORK AROUND	DBASE 1838
	4	57000	F15 57000 CENT COMP F15 DATA USED	DBASE 1839
IES004 057000	I	57000 21	8 29L 232642	DBASE 1840
IES004 057000 IES004 D		57000*23		DBASE 1841
IES004 057000 IES002 D		57000 23		DBASE 1842
IES004 057000	E	65 57000 23	45 29L 132641 1PTS20 1TSC	DBASE 1843
IES004 057000	E	29 57000 23	35 29L 132641 1PTS20 1TSC	DBASE 1844
IES004 057000	E	6 57000 23	25 29L 132641 1PTS20 1TSC	DBASE 1845
	4	63000	THIS IS LAUNCH FOR 63000 AREA	DBASE 1846
F3000 063000 F3000 F	12	63000 21		DBASE 1847
F3000 063000 F3000 D	39	63000 21	1 29L 132642	DBASE 1848
F3000 063000 F3000 D	31	63000 21	2 29L 132642	DBASE 1849
F3000 063000 F3000 D	62	63000 21	1 29L 132642	DBASE 1850
F3000 063000 F3000 D	01	63000 21	3 29L 132642	DBASE 1851
	4	63000	COMP DATA FROM F111F AND A70 USED	DBASE 1852
	M	63000	VERIFIED BY TSOT FIELD 7305	DBASE 1853
	M	63000	THIS NETWORK IS FOR THE 63A AREA F15	DBASE 1854
	M	63000	UNF COMM SET AND 149 F15	DBASE 1855

F3A11	F63A11	F3A11	F	27	63A11	21				DBASE	1346	
F3A11	2254G7	F3A11	2		63A11	21				DBASE	1347	
F3A11	CA.GPJ	F3A11	2		63A11	21				DBASE	1348	
F3A11	63A11	F3A11	2	58	63A11	21	13	29L	232602 1060	105	DBASE	1349
F3A11	63A11	F3A11	2	45	63A11	21	12	29L	232602 1060	105	DBASE	1350
F3A11	63A11	F3A11	2		63A11	23					DBASE	1351
SF3A11	L63A11	IF3A11	G	12335	63A11	23					DBASE	1352
					63A11				COMP F111F 63A11		DBASE	1353
					63A11				F15 UHF RT 63A11		DBASE	1354
IF3A11	63A11	IF3A11	E	77	63A11	*23	51	29L	132691		DBASE	1355
IF3A11	63A11		E	10	63A11	*23	30	29L	132691		DBASE	1356
IF3A11	63A11		E	17	63A11	*23	20	29L	132691		DBASE	1357
IF3A11	63A11		I		63A11	21	6	29L	232602		DBASE	1358
					63A11				63A11 INDICATES UHF LEAK CHECK		DBASE	1359
IF3A11	63A11		G		63A11	23	40		G		DBASE	1360
SF3A11	L63A11	IF3A11	G	10057	63A11	23					DBASE	1361
					63A11				COMP A70 63A11		DBASE	1362
					63A11				63A11 DATA REFLECTED AT PERCENT FIV		DBASE	1363
					63A11				EXPERIENCE AND CAPABILITY WILL MAKE A		DBASE	1364
					63A11				65 PERCENT REPAIRS POSSIBLE		DBASE	1365
					63A11				F15 UHF BACKUP RECEIVER		DBASE	1366
IF3A11	63A11		E	59	63A11	*23	30	29L	132691		DBASE	1367
IF3A11	63A11		E	15	63A11	*23	20	29L	132691		DBASE	1368
IF3A11	63A11		I		63A11	21	6	29L	232602		DBASE	1369
					63A11				THERE IS NO DATA FOR SECURE VOICE OR		DBASE	1370
					63A11				IN SMOP ANTENNA REPAIR		DBASE	1371
					63A11				THIS NETWORK IS FOR THE 632 AREA F15		DBASE	1372
					63A11				IT COVERS ALL CONTROL PANELS		DBASE	1373
					63A11				CONF DATA FROM F111F AND F15		DBASE	1374
					63A11				VERIFIED BY TEST FIELD 7312		DBASE	1375
					63A11				INTEG ONI CONT SET F15		DBASE	1376
F3B11	F63B11	F3B11	F	25	63B11	21					DBASE	1377
F3B11	2254G7	F3B11	2		63B11	21					DBASE	1378
F3B11	CA.GPJ	F3B11	2		63B11	21					DBASE	1379
F3B11	63B11	F3B11	2	58	63B11	21	25	29L	232602 1060	105	DBASE	1380
F3B11	63B11	F3B11	2	45	63B11	21	16	29L	232602 1060	105	DBASE	1381
F3B11	63B11	F3B11	2	15	63B11	21	10	29L	243141		DBASE	1382
F3B11	63B11	F3B11	2		63B11	23					DBASE	1383
SF3B11	L63B11	IF3B11	G	11203	63B11	23					DBASE	1384
					63B11				632 AREA FOR SMOP WORK VERIFIED BY		DBASE	1385
					63B11				TEST OFFICER 7312		DBASE	1386
					63B11				ADDED 63B11 AND ADJ E SELECT MODES		DBASE	1387
					63B11						DBASE	1388
IF3B11	63B11		E	71	63B11	*23	60	29L	132691		DBASE	1389
IF3B11	63B11		E	15	63B11	*23	30	29L	132691		DBASE	1390
IF3B11	63B11		E	15	63B11	*23	30	29L	132691		DBASE	1391
IF3B11	63B11		I		63B11	21	20	29L	232602 1060	105	DBASE	1392
SF3B11	L63B11	IF3B11	G	10022	63B11	23					DBASE	1393
					63B11				ADDED 63B11 AND ADJ E SELECT MODES		DBASE	1394
					63B11						DBASE	1395
IF3B11	63B11		E	75	63B11	*23	15	29L	132691		DBASE	1396
IF3B11	63B11		E	15	63B11	*23	10	29L	132691		DBASE	1397
IF3B11	63B11		E	10	63B11	*23	10	29L	132691		DBASE	1398
IF3B11	63B11		I		63B11	21	10	29L	232602		DBASE	1399
					63B11				F15 ONI CONTROL USED 63B11 AND 64000		DBASE	1400
					63B11				FROM F111F AS COMP		DBASE	1401
					63B11				F15 NAVATION CONT USED 7100A AND 7100C		DBASE	1402
					63B11				FROM F111F AS COMP		DBASE	1403
					63B11						DBASE	1404
SF3B11	L63B11	IF3B11	G	10169	63B11	23					DBASE	1405
					63B11				F15 IFF USED 64000 FROM F111F AS COMP		DBASE	1406
IF3B11	63B11		E	64	63B11	*23	15	29L	132691		DBASE	1407
IF3B11	63B11		E	15	63B11	*23	10	29L	132691		DBASE	1408
IF3B11	63B11		E	16	63B11	*23	10	29L	132691		DBASE	1409
IF3B11	63B11		I		63B11	21	12	29L	232602		DBASE	1410
SF3B11	L63B11	IF3B11	G	10267	63B11	23					DBASE	1411

	4	63900	F15 MAIN COM CONTROL USED 63900 AND	09ASE 1912
	M	63900	ADDED 63900 AND ADJ E SELECT MODES	09ASE 1913
	M	63900	63900 FROM F111F AS COMP	09ASE 1914
	M	63900		09ASE 1915
IF3940	63900	E	55 63900*23 15 29L 132601	09ASE 1916
IF3940	63900	E	05 63900*23 15 29L 132601	09ASE 1917
IF3940	63900	E	10 63900*23 15 29L 132601	09ASE 1918
IF3940	63900	E	15 63900*23 15 29L 132602	09ASE 1919
SF3900	63900	G	0595 63900 23	09ASE 1920
	4	63900	ADDED 63900 AND 63900 AND ADJ SELECT	09ASE 1921
	M	63900	MODES	09ASE 1922
	M	63900		09ASE 1923
IF3900	63900	E	80 63900*23 15 29L 132601	09ASE 1924
IF3900	63900	E	10 63900*23 15 29L 132601	09ASE 1925
IF3900	63900	E	11 63900*23 15 29L 132601	09ASE 1926
IF3900	63900	E	15 63900*23 15 29L 132602	09ASE 1927
	M	63900	THE AAI CONT BCK IS F15 DATA USED	09ASE 1928
	M	63900	THIS IS LAUNCH FOR 63900 AREA	09ASE 1929
F5000	F5000	F	63 65000 21	09ASE 1930
F5000	F5000	F	65000 21	09ASE 1931
	4	65000	F111F 65000-65000 IS USED AS COMP	09ASE 1932
	4	65000	VERIFIED BY TSGT FIELD	09ASE 1933
	M	65000	THIS IS IFF TRANSPONDER APX101 FOR F15	09ASE 1934
F5000	F5000	F	65000 21	09ASE 1935
F5000	F5000	F	65000 21	09ASE 1936
F5000	F5000	F	65000 21	09ASE 1937
F5000	F5000	F	91 65000 21 18 29L 132602 1050 105	09ASE 1938
F5000	F5000	F	1 65000 21 18 29L 132602 1050 105	09ASE 1939
F5000	F5000	F	20 65000 21 20 29L 143101	09ASE 1940
F5000	F5000	F	65000 21	09ASE 1941
SF5000	F5000	F	65000 23	09ASE 1942
	4	65000	THERE IS NO DATA TO INDICATE 65000	09ASE 1943
	M	65000	WORK EITHER F15 OR COMP ACFT	09ASE 1944
	M	65000	VERIFIED S40P WORK WITH TSGT OVERLEY	09ASE 1945
	4	65000	PH#7302	09ASE 1946
	4	65000	F15 RY/RY F111F 65000 AS COMP	09ASE 1947
IF5000	65000	E	70 65000*23 16L 29L 132601	09ASE 1948
IF5000	65000	E	5 65000*23 70 29L 132601	09ASE 1949
IF5000	65000	E	25 65000*23 60 29L 132601	09ASE 1950
IF5000	65000	E	15 65000*23 15 29L 132602	09ASE 1951
	M	65000	THIS IS NETWORK FOR AAI IFF F15 DATA	09ASE 1952
	M	65000	USED AS COMP DATA NOT AVAILABLE	09ASE 1953
	4	65000	AAI IFF	09ASE 1954
F5000	F5000	F	51 65000 21	09ASE 1955
F5000	F5000	F	65000 21	09ASE 1956
F5000	F5000	F	65000 21	09ASE 1957
F5000	F5000	F	79 65000 21 23 29L 132602 1050 105	09ASE 1958
F5000	F5000	F	21 65000 21 7 29L 132602 1050 105	09ASE 1959
F5000	F5000	F	30 65000 21 17 29L 143101	09ASE 1960
F5000	F5000	F	65000 21 10 29L 132602 1050 105	09ASE 1961
F5000	F5000	F	65000 23	09ASE 1962
SF5000	F5000	F	65000 23	09ASE 1963
	4	65000	F15 AAI RTAG6/APX75 F15 DATA USED	09ASE 1964
	M	65000	ADDED 65000 AND ADJ E SELECT MODES	09ASE 1965
	M	65000	VERIFIED S40P WORK WITH TSGT OVERLEY	09ASE 1966
	4	65000	PH#7302	09ASE 1967
	4	65000	TSGT OVERLEY GAVE BEST ESTIMATES OF	09ASE 1968
	4	65000	TASK TIME REQUIREMENTS ALL CREW STAFF	09ASE 1969
	M	65000	ARE 1	09ASE 1970
	M	65000	F15 AAI RTAG6/APX75	09ASE 1971
IF5000	65000	E	71 65000*23 100 29L 132601	09ASE 1972
IF5000	65000	E	5 65000*23 45 29L 132601	09ASE 1973
IF5000	65000	E	24 65000*23 50 29L 132601	09ASE 1974
IF5000	65000	E	23 29L 132602	09ASE 1975
SF5000	65000	G	00333 65000 23	09ASE 1976
	4	65000	F15 AAI TARGET PROCESSOR F15 DATA USED	09ASE 1977

IF5640 0659M3	I	65900	21	23 29L 232602	ORASE 1978
IF5341 0659M3	IF5341 2	65900	23		ORASE 1979
IF5341 0659M3	IF5341 2	65900	23		ORASE 1980
IF5342 0659M3	E	33 65900	23	71 29L 132641 1PT534 1T50	ORASE 1981
IF5342 0659M3	E	67 65900	23	15 29L 232641 1PT534 1T50	ORASE 1982
		71000		THIS IS LAUNCH FOR 71000 AFSA	ORASE 1983
G1030 F71000 G1001 F	1 71000	21			ORASE 1984
G1030 F71000 G1001 F	1 71000	21	1 29L 232602		ORASE 1985
G1001 061000 G1001 E	75 71000	21	3 29L 232602		ORASE 1986
G1001 061000 G1001 E	1 71000	21	3 29L 232602		ORASE 1987
	4	71000		A70 WAS GIVEN AS COMPASSABLE BUT THIS	ORASE 1988
	4	71000		SYSTEM SHOULD BE MUCH BETTER THE	ORASE 1989
	4	71000		ENGINEER HADV BROWN COULD NOT ESTIMATE	ORASE 1990
	4	71000		HOW MUCH BETTER COULD A70 A70	ORASE 1991
	4	71000		73FAC+73000+73FOL+73FAC+73FOL THE LAST	ORASE 1992
	4	71000		BEING FOR THE INS UNIT IND F15 71000	ORASE 1993
	4	71000		VERIFIED BY TSGT RAY A70 17 F15=1-	ORASE 1994
	4	71000		THIS IS NETWORK FOR F15 INS 71000	ORASE 1995
G1000 F71000 G1001 F	13 71000	21			ORASE 1996
G1000 061000 G1001 F	71000	21			ORASE 1997
G1000 061000 G1001 F	71000	21			ORASE 1998
G1000 061000 G1001 F	1 71000	21	17 29L 232642 1060 105		ORASE 1999
G1000 061000 G1001 F	16 71000	21	22 29L 232642 1060 105		ORASE 2000
G1000 061000 G1001 F	2 71000	21	29 29L 232642		ORASE 2001
G1000 061000 G1001 F	71000	23			ORASE 2002
G1000 061000 G1001 F	71000	23			ORASE 2003
	4	71000		F15 INS UNIT USED A70 71FAC+73FOL	ORASE 2004
	4	71000		73FAC+73000 THE F15 HAS EVERYTHING IN	ORASE 2005
	4	71000		ONE UNIT E SELECT AND TIMES AND	ORASE 2006
	4	71000		VERIFIED BY TS TOUCHARD WORK AROUND	ORASE 2007
	4	71000		E SEL AND TIMES FM A70	ORASE 2008
	4	71000		F15 INS UNIT	ORASE 2009
IG1000 071000	I	71000	21	10 29L 232642 1060 105	ORASE 2010
IG1000 071000 IG1000	71000	23			ORASE 2011
IG1000 071000 IG1000	71000	23			ORASE 2012
IG1000 071000 IG1000	4 71000	23	96 29L 132641 1PT59 1T50		ORASE 2013
IG1000 071000 IG1000	26 71000	23	75 29L 132641 1PT59 1T50		ORASE 2014
IG1000 071000 IG1000	26 71000	23	54 29L 132641 1PT59 1T50		ORASE 2015
SG1000 071000 IG1000	71000	23			ORASE 2016
	4	71000		F15 INS CONT-IND A70 71FAC+73FOL	ORASE 2017
	4	71000		E SELECT AND TASK TIMES AND DATA	ORASE 2018
	4	71000		VERIFIED BY TS TOUCHARD WORK AROUND	ORASE 2019
	4	71000		F15 INS CONT	ORASE 2020
IG1000 071000	I	71000	21	10 29L 232642 1060 105	ORASE 2021
IG1000 071000 IG1000	71000	23			ORASE 2022
IG1000 071000 IG1000	71000	23			ORASE 2023
IG1000 071000 IG1000	54 71000	23	46 29L 132641 1PT56 1T50		ORASE 2024
IG1000 071000 IG1000	21 71000	23	10 29L 132641 1PT56 1T50		ORASE 2025
IG1000 071000 IG1000	25 71000	23	10 29L 132641 1PT56 1T50		ORASE 2026
	4	71000		F111F 71000 DATA USED	ORASE 2027
	4	71000		VERIFIED BY TSGT FIELD	ORASE 2028
	4	71000		THIS IS NETWORK FOR F15 ACF 71000	ORASE 2029
G1300 F71300 G1301 F	305 71000	21			ORASE 2030
G1300 061000 G1301 F	71000	21			ORASE 2031
G1300 061000 G1301 F	71000	21			ORASE 2032
G1300 061000 G1301 F	85 71000	21	25 29L 232602 1060 105		ORASE 2033
G1300 061000 G1301 F	15 71000	21	20 29L 232602 1060 105		ORASE 2034
	4	71000		THERE IS NO SIGNIFICANT SHOR DATA FOR	ORASE 2035
	4	71000		THIS SUBSYSTEM DATA BY TO DRIFT	ORASE 2036
	4	71000		THIS IS NETWORK FOR F15 ACF 71000	ORASE 2037
G1300 061000 IG1300	71000	23			ORASE 2038
IG1300 071000	71000	23	30 29L 132641		ORASE 2039
IG1300 071000	20 71000	23	20 29L 132641		ORASE 2040
IG1300 071000	10 71000	23	20 29L 132641		ORASE 2041
IG1300 071000	71000	21	20 29L 232642 1060 105		ORASE 2042
	4	71000		F111F 71000 DATA USED F15 MSB-4 1000	ORASE 2043

	4	71000	VERIFIED BY TSGT FIELD	09ASE 2044
	4	71001	THIS IS NETWORK FOR F15 ILS 71001	09ASE 2045
G1001 F71001 G1001 F	533	71001 21		09ASE 2046
G1001 000007 G1001 0		71001 21		09ASE 2047
G1001 000007 G1001 0		71001 21		09ASE 2048
G1001 000007 G1001 0	31	71001 21	21 29L 232602 1000 105	09ASE 2049
G1001 000007 G1001 0	11	71001 21	11 29L 232602 1000 105 1431X1	09ASE 2050
G1001 000007 G1001 0		71001 21		09ASE 2051
SG1001 L71001 IG1001 0		71001 23		09ASE 2052
	4	71001	F15 ILS FC/F 71001 USED F111F 71001	09ASE 2053
	4	71001	VERIFIED BY TS OBERLY	09ASE 2054
	4	71001	F15 ILS FC/F	09ASE 2055
IG1001 071001	E	75 71001*23	30 29L 232601	09ASE 2056
IG1001 071001	E	15 71001*23	20 29L 232601	09ASE 2057
IG1001 071001	E	10 71001*23	20 29L 232601	09ASE 2058
IG1001 071001	I	71001 21	11 29L 232602 1000 105	09ASE 2059
	4	71001	F111F 71001 DATA USED F15 0904 76	09ASE 2060
	4	71001	VERIFIED BY TSGT FIELD 403 37 FOR F111F	09ASE 2061
	4	71001	THIS IS NETWORK FOR F15 TACAN 71001	09ASE 2062
G1001 000007 G1001 0	55	71001 21		09ASE 2063
G1001 000007 G1001 0		71001 21		09ASE 2064
G1001 000007 G1001 0		71001 21		09ASE 2065
G1001 000007 G1001 0	92	71001 21	25 29L 232602 1000 105	09ASE 2066
G1001 000007 G1001 0	1	71001 21	15 29L 232602 1000 105 1431X1	09ASE 2067
G1001 000007 G1001 0		71001 23		09ASE 2068
SG1001 L71001 IG1001 0		71001 23		09ASE 2069
	4	71001	F15 TACAN ROVF 71001 F111F 71001 USED	09ASE 2070
	4	71001	F15 TACAN ROVF	09ASE 2071
IG1001 071001	E	80 71001*23	20 29L 232601	09ASE 2072
IG1001 071001	E	15 71001*23	15 29L 232601	09ASE 2073
IG1001 071001	E	5 71001*23	15 29L 232601	09ASE 2074
IG1001 071001	I	71001 21	20 29L 232602 1000 105	09ASE 2075
	4	71001	THIS IS NETWORK FOR F15 ATTITUDE HEAD	09ASE 2076
	4	71001	ING REF F111F 510 DATA USED F15 20	09ASE 2077
	4	71001	VERIFIED BY TS POOLE	09ASE 2078
	4	71001	ATTITUDE/HEADING REF	09ASE 2079
G1F01 F71F01 G1F01 F	52	71F01 21		09ASE 2080
G1F01 000007 G1F01 0		71F01 21		09ASE 2081
G1F01 000007 G1F01 0		71F01 21		09ASE 2082
G1F01 000007 G1F01 0	56	71F01 21	31 29L 232602 1000 105	09ASE 2083
G1F01 000007 G1F01 0	1	71F01 21	11 29L 232602 1000 105	09ASE 2084
G1F01 000007 G1F01 0	25	71F01 21	18 29L 1431X1	09ASE 2085
G1F01 000007 G1F01 0		71F01 23		09ASE 2086
SG1F01 L71F01 IG1F01 0	00-65	71F01 23		09ASE 2087
	4	71F01	F15 ELEC-CONT AMP 71F01 F111F 51000	09ASE 2088
	4	71F01	DATA USED WORK AROUND	09ASE 2089
	4	71F01	VERIFIED BY TS BOULHARD	09ASE 2090
	4	71F01	F15 ELEC-CONT AMP	09ASE 2091
IG1F01 071F01	E	71F01 21	15 29L 232602 1000 105	09ASE 2092
IG1F01 071F01 IG1F01 0		71F01*23		09ASE 2093
IG1F01 071F01 IG1F01 0		71F01 23		09ASE 2094
IG1F01 071F01	E	55 71F01 23	40 29L 232601 1000 105	09ASE 2095
IG1F01 071F01	E	11 71F01 23	30 29L 232601 1000 105	09ASE 2096
IG1F01 071F01	E	27 71F01 23	36 29L 232601 1000 105	09ASE 2097
SG1F01 L71F01 IG1F01 0	00-65	71F01 23		09ASE 2098
	4	71F01	F15 DISPLACEMENT GYRO F111F 51000 DATA USED	09ASE 2099
	4	71F01	USED FOR RATE SELECT AND TASK TIMES	09ASE 2100
	4	71F01	VERIFIED BY TS BOULHARD	09ASE 2101
	4	71F01	F15 DISPLACEMENT GYRO	09ASE 2102
IG1F01 071F01	E	71F01 21	15 29L 232602 1000 105	09ASE 2103
SG1F01 L71F01 IG1F01 0	00-65	71F01 23		09ASE 2104
IG1F01 071F01 IG1F01 0		71F01*23		09ASE 2105
IG1F01 071F01 IG1F01 0		71F01 23		09ASE 2106
IG1F01 071F01	E	10 71F01 23	70 29L 232601 1000 105	09ASE 2107
IG1F01 071F01	E	90 71F01 23	70 29L 232601 1000 105	09ASE 2108
	4	71F01	F15 COMPASS CONT F111F 51000 DATA USED	09ASE 2109

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IG4F10	N7-F10	E	52	74F00*23	90	29L	232691		DBASE	2176
IG4F10	K7-F10	E	2	74F10*23	51	29L	232691		DBASE	2177
IG4F10	N7-F10	E	46	74F10*23	52	29L	232691		DBASE	2178
IG4F10	N7-F10	E		74F00 21	30	29L	232692 1060	105	DBASE	2179
SG4F10	L7-F00	IG4F00	G	10531	74F00 23				DBASE	2181
				74F00	F15 RADAR RCVR 74F00 USED F111F 73VAC				DBASE	2181
				74F00	AS COMP G SELECT IS 1/3 OF F111F DATA				DBASE	2182
				74F00	F111F USED F SELECT TIME ESTIMATES BY				DBASE	2183
				74F00	TS BOUCHARD				DBASE	2184
				74F00	F15 RADAR RCVR				DBASE	2185
IG4F10	N7-F00	I		74F00 21	10	29L	232692 1060	105	DBASE	2186
IG4F10	N7-F00	IG4F00	G	74F00*23					DBASE	2187
IG4F10	N7-F00	IG4F00	G	74F00 23					DBASE	2188
IG4F10	N7-F00	E	72	74F00 23	59	29L	132641 1PTS31 1TSM		DBASE	2189
IG4F10	N7-F00	E	14	74F00 23	30	29L	132641 1PTS31 1TSM		DBASE	2190
IG4F10	N7-F00	E	14	74F00 23	30	29L	132641 1PTS31 1TSM		DBASE	2191
SG4F10	L7-F00	IG4F00	G	10531	74F00 23				DBASE	2192
				74F00	F15 RD FREQ OSC 74F00 USED F111F				DBASE	2193
				74F00	73VAC AS COMP G SELECT IS 1/3 OF				DBASE	2194
				74F00	F111F DATA				DBASE	2195
				74F00	AND VERIFIED BY TS BOUCHARD				DBASE	2196
				74F00	F15 RD FREQ OSC				DBASE	2197
IG4F10	N7-F00	I		74F00 21	10	29L	232692 1060	105	DBASE	2198
IG4F10	N7-F00	IG4F00	G	74F00*23					DBASE	2199
IG4F10	N7-F00	IG4F00	G	74F00 23					DBASE	2200
IG4F10	N7-F00	E	72	74F00 23	55	29L	132641 1PTS31 1TSM		DBASE	2201
IG4F10	N7-F00	E	13	74F00 23	40	29L	132641 1PTS31 1TSM		DBASE	2202
IG4F10	N7-F00	E	15	74F00 23	40	29L	132641 1PTS31 1TSM		DBASE	2203
				74F00	F15 ANT 74F00 F111F 73VAC DATA USED				DBASE	2204
				74F00	VERIFIED BY TS BOUCHARD F111 TIME USED				DBASE	2205
				74F00	F15 ANT				DBASE	2206
SG4F10	L7-F00	IG4F00	G	10531	74F00 23				DBASE	2207
IG4F10	N7-F00	E	67	74F00*23	60	29L	232691		DBASE	2208
IG4F10	N7-F00	E	16	74F00*23	30	29L	232691		DBASE	2209
IG4F10	N7-F00	E	17	74F00*23	46	29L	232691		DBASE	2210
IG4F10	N7-F00	E		74F00 21	35	29L	232692 1060	105	DBASE	2211
SG4F10	L7-F00	IG4F00	G	11690	74F00 23				DBASE	2212
				74F00	F15 RADAR TGT PROCESSOR 74F00 F111F				DBASE	2213
				74F00	73VAC DATA USED WORK AROUND				DBASE	2214
				74F00	VERIFIED BY TS BOUCHARD				DBASE	2215
				74F00	F15 RADAR TGT PROCESSOR				DBASE	2216
IG4F10	N7-F00	E		74F00 21	10	29L	232692 1060	105	DBASE	2217
IG4F10	N7-F00	IG4F00	G	74F00*23					DBASE	2218
IG4F10	N7-F00	IG4F00	G	74F00 23					DBASE	2219
IG4F10	N7-F00	E	59	74F00 23	81	29L	132641 1PTS43 1TSO		DBASE	2220
IG4F10	N7-F00	E	24	74F00 23	45	29L	132641 1PTS43 1TSO		DBASE	2221
IG4F10	N7-F00	E	17	74F00 23	45	29L	132641 1PTS43 1TSO		DBASE	2222
SG4F10	L7-F00	IG4F00	G	12122	74F00 23				DBASE	2223
				74F00	VERIFIED BY WORK AROUND				DBASE	2224
				74F00	F15 DATA PROCESSOR 74F00 F15 DATA				DBASE	2225
IG4F10	N7-F00	I		74F00 21	10	29L	232692 1060	105	DBASE	2226
IG4F10	N7-F00	IG4F00	G	74F00*23					DBASE	2227
IG4F10	N7-F00	IG4F00	G	74F00 23					DBASE	2228
IG4F10	N7-F00	E	72	74F00 23	69	29L	132641 1PTS32 1TSM		DBASE	2229
IG4F10	N7-F00	E	13	74F00 23	40	29L	132641 1PTS32 1TSM		DBASE	2230
IG4F10	N7-F00	E	49	74F00 23	40	29L	132641 1PTS32 1TSM		DBASE	2231
SG4F10	L7-F00	IG4F00	G	12619	74F00 23				DBASE	2232
				74F00	VERIFIED BY WORK AROUND				DBASE	2233
				74F00	F15 ANALOG PROCESSOR 74F00 F15 DATA				DBASE	2234
IG4F10	N7-F00	I		74F00 21	10	29L	232692 1060	105	DBASE	2235
IG4F10	N7-F00	IG4F00	G	74F00*23					DBASE	2236
IG4F10	N7-F00	IG4F00	G	74F00 23					DBASE	2237
IG4F10	N7-F00	E	43	74F00 23	90	29L	132641 1PTS33 1TSM		DBASE	2238
IG4F10	N7-F00	E	14	74F00 23	64	29L	132641 1PTS33 1TSM		DBASE	2239
IG4F10	N7-F00	E	43	74F00 23	64	29L	132641 1PTS33 1TSM		DBASE	2240
SG4F10	L7-F00	IG4F00	G	10119	74F00 23				DBASE	2241

	4	74F00	F15 RACAR SET CONT 74FK F111F	0BASE 2242
	M	74F00	VERIFIED BY TS OFFLEY	0BASE 2243
	4	74F00	F15 RACAR SET CONT	0BASE 2244
IG4FK: 47-FK:	E	1 74F00*23	27 29L 132631	0BASE 2245
IG4FK: 47-FK:	E	9 74F00*23	26 29L 132631	0BASE 2246
IG4FK: 07-FK:	I	74F00 21	13 29L 232642 1060 105	0BASE 2247
SG4FK: L7-FK: IG-FK:	S	11786 74F00 23		0BASE 2248
	4	74F00	F15 RWP SPLY 74F00 F15 DATA G SELECT	0BASE 2249
	M	74F00	TIMES AND E SELECT GIVEN BY TS BOUCHARD	0BASE 2250
	M	74F00	F15 RWP SPLY 74F00	0BASE 2251
IG4FK: 47-FK:	E	57 74F00*23	30 29L 132631	0BASE 2252
IG4FK: 47-FK:	E	24 74F00*23	20 29L 132631	0BASE 2253
IG4FK: 47-FK:	E	1 74F00*23	12 29L 132631	0BASE 2254
IG4FK: 07-FK:	I	74F00 21	13 29L 232642 1060 105	0BASE 2255
	4	74J00	F15 INDICATOR GROUP A7D 73AEC+73EB	0BASE 2256
	M	74J00	USED F15 153MA 3-	0BASE 2257
	M	74J00	VERIFIED BY TSOT FAY	0BASE 2258
	M	74J00	F15 INDICATOR GROUP	0BASE 2259
G4J00 F7-J00 G4J01	F	35 74J00 21		0BASE 2260
G4J01 22-MGT G4J02	D	74J00 21		0BASE 2261
G4J02 24-LGP G4J03	D	74J00 21		0BASE 2262
G4J03 27-J00 G4J04	E	47 74J00 21	20 29L 232642 1060 105	0BASE 2263
G4J04 47-J00	E	17 74J00 21	12 29L 232642 1060 105	0BASE 2264
G4J05 SHOP SG4J00	D	74J00 23		0BASE 2265
SG4J00 L7-J00 IG4J00	S	12263 74J00 23		0BASE 2266
	4	74J00	F15 MULT TWO A7D 73AEC DATA USED	0BASE 2267
	M	74J00	VERIFIED BY TS BOUCHARD	0BASE 2268
	4	74J00	F15 MULT IND	0BASE 2269
IG4J00 07-J00	I	74J00 21	20 29L 232642 1060 105	0BASE 2270
IG4J01 07-J00 IG4J02	D	74J00*23		0BASE 2271
IG4J02 07-J00 IG4J03	D	74J00 23		0BASE 2272
IG4J03 47-J00	E	8 74J00 23	43 29L 132641 1PTS46 1TSD	0BASE 2273
IG4J04 47-J00	E	16 74J00 23	15 29L 132641 1PTS46 1TSD	0BASE 2274
IG4J05 47-J00	E	74J00 23	15 29L 132641 1PTS46 1TSD	0BASE 2275
SG4J00 L7-J00 IG4J00	S	12291 74J00 23		0BASE 2276
	4	74J00	F15 SIG DATA PROCESSOR 74J00 A7D 73EB	0BASE 2277
	M	74J00	DATA USED WORK AROUND	0BASE 2278
	M	74J00	VERIFIED BY TS BOUCHARD	0BASE 2279
	M	74J00	F15 SIG DATA PROCESSOR	0BASE 2280
IG4J00 07-J00	I	74J00 21	8 29L 232642 1060 105	0BASE 2281
IG4J01 07-J00 IG4J02	D	74J00*23		0BASE 2282
IG4J02 07-J00 IG4J03	D	74J00 23		0BASE 2283
IG4J03 47-J00	E	57 74J00 23	66 29L 132641 1PTS37 1TSD	0BASE 2284
IG4J04 47-J00	E	21 74J00 23	40 29L 132641 1PTS37 1TSD	0BASE 2285
IG4J05 47-J00	E	23 74J00 23	40 29L 132641 1PTS37 1TSD	0BASE 2286
	4	74K00	F15 HUD NETWORK A7D 73AEC+73EB DATA	0BASE 2287
	M	74K00	USED F15 40EMA 16 A7D 13 USE F15	0BASE 2288
	M	74K00	VERIFIED BY TSOT FAY	0BASE 2289
	M	74K00	F15 HUD	0BASE 2290
G4K00 F7-K00 G4K01	F	14 74K00 21		0BASE 2291
G4K01 22-MGT G4K02	D	74K00 21		0BASE 2292
G4K02 24-LGP G4K03	D	74K00 21		0BASE 2293
G4K03 27-K00 G4K04	E	8 74K00 21	23 29L 232642 1060 105	0BASE 2294
G4K04 47-K00	E	21 74K00 21	10 29L 232642 1060 105	0BASE 2295
G4K05 SHOP SG4K00	D	74K00 23		0BASE 2296
SG4K00 L7-K00 IG4K00	S	12291 74K00 23		0BASE 2297
	4	74K00	F15 SIG DATA PROCESSOR 74K00 A7D 73EB	0BASE 2298
	M	74K00	DATA USED WORK AROUND	0BASE 2299
	M	74K00	VERIFIED BY TS BOUCHARD	0BASE 2300
	M	74K00	F15 SIG DATA PROCESSOR	0BASE 2301
IG4K00 07-K00	I	74K00 21	8 29L 232642 1060 105	0BASE 2302
IG4K01 07-K00 IG4K02	D	74K00*23		0BASE 2303
IG4K02 07-K00 IG4K03	D	74K00 23		0BASE 2304
IG4K03 47-K00	E	57 74K00 23	66 29L 132641 1PTS36 1TSD	0BASE 2305
IG4K04 47-K00	E	20 74K00 23	40 29L 132641 1PTS36 1TSD	0BASE 2306
IG4K05 47-K00	E	23 74K00 23	20 29L 132681	0BASE 2307

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		M	75C00	VERIFIED BY MS GIBELYOU 2937/2454	ORASE 2374
		M	75C00	F15 MRP NETWORK A7D 75C00 DATA USED	ORASE 2375
G5C01	F75C01	G5C01	F	135 75C00 21	ORASE 2376
G5C02	75C02	G5C02	D	75C00 21	ORASE 2377
G5C03	04LGPJ	G5C03	C	75C00 21	ORASE 2378
G5C04	475C04			15 29L 3462Y0 1060 105	ORASE 2379
				PANEL WILL FAIL 10X AS OFTEN AS A7D	ORASE 2380
				VERIFIED BY MS GIBELYOU	ORASE 2381
				F15 M59A AUG 75 IS 210	ORASE 2382
				F15 AFM CONT SET AMS 20 A7D 74C00 USED	ORASE 2383
G5M01	F75M01	G5M01	F	213 75M00 21	ORASE 2384
G5M02	002M02	G5M02	D	75M00 21	ORASE 2385
G5M03	04LGPJ	G5M03	C	75M00 21	ORASE 2386
G5M04	475M04	G5M04	F	90 75M00 21	ORASE 2387
G5M05	475M05	G5M05	E	2 75M00 21	ORASE 2388
G5M06	540P	G5M06	D	75M00 23	ORASE 2389
G5M07	L75M07	G5M07	F	9107 75M00 23	ORASE 2390
				ESTIMATES BY WORK AROUND	ORASE 2391
				F15 AFM CONT PANEL 75M00	ORASE 2392
IG5M01	475M01	IG5M01	I	21 29L 3462Y0 1060 105	ORASE 2393
IG5M02	075M02	IG5M02	D	75M00 23	ORASE 2394
IG5M03	075M03	IG5M03	C	75M00 23	ORASE 2395
IG5M04	475M04	IG5M04	E	21 29L 1326A1 1PTS45 1TS0	ORASE 2396
IG5M05	475M05	IG5M05	E	31 29L 1326A1 1PTS45 1TS0	ORASE 2397
IG5M06	475M06	IG5M06	E	13 29L 1326A1 1PTS45 1TS0	ORASE 2398
IG5M07	L75M07	IG5M07	F	9107 75M00 23	ORASE 2399
				ESTIMATES BY WORK AROUND	ORASE 2400
				F15 CONVERTER PROGRAMMER 75M00	ORASE 2401
IG5M01	075M01	IG5M01	I	15 29L 2462Y0 1060 105	ORASE 2402
IG5M02	075M02	IG5M02	D	75M00 23	ORASE 2403
IG5M03	075M03	IG5M03	C	75M00 23	ORASE 2404
IG5M04	475M04	IG5M04	E	20 29L 1326A1 1PTS45 1TS0	ORASE 2405
IG5M05	475M05	IG5M05	E	31 29L 1326A1 1PTS45 1TS0	ORASE 2406
IG5M06	475M06	IG5M06	E	40 29L 1326A1 1PTS45 1TS0	ORASE 2407
				VERIFIED BY JURSINK ONLY ONCE A7D 10	ORASE 2408
				F15 DATA=56 MCATA=12 75C00 F111F17	ORASE 2409
				F15 M61A1 GUN NETWORK 75M00	ORASE 2410
G5M01	F75M01	G5M01	F	2000 75M00 21	ORASE 2411
G5M02	002M02	G5M02	D	75M00 21	ORASE 2412
G5M03	04LGPJ	G5M03	C	75M00 21	ORASE 2413
G5M04	475M04	G5M04	E	01 75M00 21	ORASE 2414
G5M05	475M05	G5M05	E	13 29L 2462Y0 1060 105	ORASE 2415
G5M06	475M06	G5M06	E	12 29L 2462Y0 1060 105	ORASE 2416
G5M07	475M07	G5M07	E	07 75M00 21	ORASE 2417
G5M08	475M08	G5M08	E	16 29L 2462Y0 1060 105	ORASE 2418
G5M09	475M09	G5M09	E	13 29L 3462Y0 1060 105	ORASE 2419
G5M10	540P	G5M10	D	75M00 23	ORASE 2420
				F15 M51A1 GUN 75M00	ORASE 2421
G5M01	L75M01	IG5M01	F	1246 75M00 23	ORASE 2422
IG5M02	475M02	IG5M02	E	06 75M00 23	ORASE 2423
IG5M03	475M03	IG5M03	E	5 75M00 23	ORASE 2424
IG5M04	475M04	IG5M04	E	9 75M00 23	ORASE 2425
IG5M05	475M05	IG5M05	I	75M00 21	ORASE 2426
IG5M06	L75M06	IG5M06	F	0307 75M00 23	ORASE 2427
				F15 CPU ASSY 75ME6	ORASE 2428
IG5M01	475M01	IG5M01	E	77 75M00 23	ORASE 2429
IG5M02	475M02	IG5M02	E	23 75M00 23	ORASE 2430
IG5M03	475M03	IG5M03	I	75M00 21	ORASE 2431
G5M04	L75M04	IG5M04	F	14167 75M00 23	ORASE 2432
				F15 CONVEYOR SYS 75M00	ORASE 2433
IG5M01	475M01	IG5M01	D	75M00 23	ORASE 2434
IG5M02	475M02	IG5M02	I	75M00 21	ORASE 2435
G5M03	L75M03	IG5M03	F	03192 75M00 23	ORASE 2436
				F15 MYD COMP GUN 75MLM	ORASE 2437
IG5M01	475M01	IG5M01	D	75M00 23	ORASE 2438
IG5M02	475M02	IG5M02	I	75M00 21	ORASE 2439

61A3J3	GPTS5	3	TESTC*23	DBASE 2536
71AK1	PTSN K 71AK1	34	TESTC 23	DBASE 2537
671E1	PTSN K	66	TESTC 23	DBASE 2538
671E1	PTSC	2	TESTC 23	DBASE 2539
71AK1	LPTS6 71AK1	3	TESTC 23	DBASE 2540
	LPTS6	4	TESTC	DBASE 2541
			LFU 71AK1 T/S	
71AK1	GPTS5 71AK1	3	TESTC 23	DBASE 2542
71AK1	GPTS6	3	TESTC*23	DBASE 2543
671E1	PTSN K 71FE1	16	TESTC 23	DBASE 2544
671E1	PTSN K	84	TESTC 23	DBASE 2545
671E1	PTSC	3	TESTC 23	DBASE 2546
71FE1	LPTS7 71FE1	3	TESTC 23	DBASE 2547
	LPTS7	4	TESTC	DBASE 2548
			LFU 71FE1 T/S	
71FE1	GPTS7 71FE1	3	TESTC 23	DBASE 2549
71FE1	GPTS7	3	TESTC*23	DBASE 2550
671E1	PTSN K 71E31	37	TESTC 23	DBASE 2551
671E1	PTSN K	63	TESTC 23	DBASE 2552
671E1	PTSC	7	TESTC 23	DBASE 2553
71E31	LPTS4 71E31	3	TESTC 23	DBASE 2554
	LPTS4	4	TESTC	DBASE 2555
			LFU 71E31 T/S	
71E31	GPTS3 71E31	3	TESTC 23	DBASE 2556
71E31	GPTS3	3	TESTC*23	DBASE 2557
671E1	PTSN K 71AE1	39	TESTC 23	DBASE 2558
671E1	PTSN K	62	TESTC 23	DBASE 2559
671E1	PTSC	3	TESTC 23	DBASE 2560
71AE1	LPTS9 71AE1	3	TESTC 23	DBASE 2561
	LPTS9	4	TESTC	DBASE 2562
			LFU 71AE1 T/S	
71AE1	GPTS3 71AE1	3	TESTC 23	DBASE 2563
71AE1	GPTS3	3	TESTC*23	DBASE 2564
651A1	PTSN K 51AJ1	16	TESTC 23	DBASE 2565
651A1	PTSN K	84	TESTC 23	DBASE 2566
651A1	PTSC	3	TESTC 23	DBASE 2567
51AJ1	LPTS10 51AJ1	3	TESTC 23	DBASE 2568
	LPTS10	4	TESTC	DBASE 2569
			LFU 51AJ1 T/S	
51AJ1	GPTS10 51AJ1	3	TESTC 23	DBASE 2570
51AJ1	GPTS10	3	TESTC*23	DBASE 2571
652A1	PTSN K 52A31	69	TESTC 23	DBASE 2572
652A1	PTSN K	91	TESTC 23	DBASE 2573
652A1	PTSC	3	TESTC*23	DBASE 2574
52A31	LPTS11 52A31	3	TESTC 23	DBASE 2575
	LPTS11	4	TESTC	DBASE 2576
			LFU 52A31 T/S	
52A31	GPTS11 52A31	3	TESTC 23	DBASE 2577
52A31	GPTS11	3	TESTC*23	DBASE 2578
652A1	PTSN K 52A11	69	TESTC 23	DBASE 2579
652A1	PTSN K	91	TESTC 23	DBASE 2580
652A1	PTSC	3	TESTC 23	DBASE 2581
52A11	LPTS12 52A11	3	TESTC 23	DBASE 2582
	LPTS12	4	TESTC	DBASE 2583
			LFU 52A11 T/S	
52A11	GPTS12 52A11	3	TESTC 23	DBASE 2584
52A11	GPTS12	3	TESTC*23	DBASE 2585
649CA1	PTSN K 49CAA1	20	TESTC 23	DBASE 2586
649CA1	PTSN K	81	TESTC 23	DBASE 2587
649CA1	PTSC	3	TESTC 23	DBASE 2588
49CAA1	LPTS13 49CAA1	3	TESTC 23	DBASE 2589
	LPTS13	4	TESTC	DBASE 2590
			LFU 49CAA1 T/S	
49CAA1	GPTS13 49CAA1	3	TESTC 23	DBASE 2591
49CAA1	GPTS13	3	TESTC*23	DBASE 2592
671FA1	PTSN K 71FA1	47	TESTC 23	DBASE 2593
671FA1	PTSN K	60	TESTC 23	DBASE 2594
671FA1	PTSC	3	TESTC 23	DBASE 2595
71FA1	LPTS14 71FA1	3	TESTC 23	DBASE 2596
	LPTS14	4	TESTC	DBASE 2597
			LFU 71FA1 T/S	
71FA1	GPTS14 71FA1	3	TESTC 23	DBASE 2598
71FA1	GPTS14	3	TESTC*23	DBASE 2599
611F1	PTSN K 11F1	37	TESTC 23	DBASE 2600
611F1	PTSN K	63	TESTC 23	DBASE 2601

011P00	CTSC	0	TESTC 23	09ASE 2572
11P011	LPTS15	0	TESTC 23	09ASE 2573
	LPTS15	4	TESTC LRU 11P01 T/S	09ASE 2574
11P012	QPTS15	0	TESTC 23	09ASE 2575
11P013	QPTS15	0	TESTC*23	09ASE 2576
055C01	PTSN.K	15	TESTC 23	09ASE 2577
055C01	PTSN.K	82	TESTC 23	09ASE 2578
055C01	CTSC	0	TESTC 23	09ASE 2579
55C011	LPTS15	0	TESTC 23	09ASE 2580
	LPTS15	4	TESTC LRU 55C01 T/S	09ASE 2581
55C012	QPTS15	0	TESTC 23	09ASE 2582
55C013	QPTS15	0	TESTC*23	09ASE 2583
052A01	PTSN.K	16	TESTC 23	09ASE 2584
052A01	PTSN.K	84	TESTC 23	09ASE 2585
052A01	CTSC	0	TESTC 23	09ASE 2586
52A011	LPTS17	0	TESTC 23	09ASE 2587
	LPTS17	4	TESTC LRU 52A01 T/S	09ASE 2588
52A012	QPTS17	0	TESTC 23	09ASE 2589
52A013	QPTS17	0	TESTC*23	09ASE 2590
071F01	PTSN.K	19	TESTC 23	09ASE 2591
071F01	PTSN.K	91	TESTC 23	09ASE 2592
071F01	CTSC	0	TESTC 23	09ASE 2593
71F011	LPTS19	0	TESTC 23	09ASE 2594
	LPTS19	4	TESTC LRU 71F01 T/S	09ASE 2595
71F012	QPTS19	0	TESTC 23	09ASE 2596
71F013	QPTS19	0	TESTC*23	09ASE 2597
055C01	PTSN.K	19	TESTC 23	09ASE 2598
055C01	PTSN.K	85	TESTC 23	09ASE 2599
055C01	CTSC	0	TESTC 23	09ASE 2600
55C011	LPTS19	0	TESTC 23	09ASE 2601
	LPTS19	4	TESTC LRU 55C01 T/S	09ASE 2602
55C012	QPTS19	0	TESTC 23	09ASE 2603
55C013	QPTS19	0	TESTC*23	09ASE 2604
057A01	PTSN.K	36	TESTC 23	09ASE 2605
057A01	PTSN.K	64	TESTC 23	09ASE 2606
057A01	CTSC	0	TESTC 23	09ASE 2607
57A011	LPTS22	0	TESTC 23	09ASE 2608
	LPTS22	4	TESTC LRU 57A01 T/S	09ASE 2609
57A012	QPTS22	0	TESTC 23	09ASE 2610
57A013	QPTS22	0	TESTC*23	09ASE 2611
041A01	PTSN.K	20	TESTC 23	09ASE 2612
041A01	PTSN.K	81	TESTC 23	09ASE 2613
041A01	CTSC	0	TESTC 23	09ASE 2614
41A011	LPTS22	0	TESTC 23	09ASE 2615
	LPTS22	4	TESTC LRU 41A01 T/S	09ASE 2616
41A012	QPTS22	0	TESTC 23	09ASE 2617
41A013	QPTS22	0	TESTC*23	09ASE 2618
041A01	PTSN.K	20	TESTC 23	09ASE 2619
041A01	PTSN.K	81	TESTC 23	09ASE 2620
041A01	CTSC	0	TESTC 23	09ASE 2621
41A011	LPTS23	0	TESTC 23	09ASE 2622
	LPTS23	4	TESTC LRU 41A01 T/S	09ASE 2623
41A012	QPTS23	0	TESTC 23	09ASE 2624
41A013	QPTS23	0	TESTC*23	09ASE 2625
051A01	PTSN.K	22	TESTC 23	09ASE 2626
051A01	PTSN.K	71	TESTC 23	09ASE 2627
051A01	CTSC	0	TESTC 23	09ASE 2628
51A011	LPTS24	0	TESTC 23	09ASE 2629
	LPTS24	4	TESTC LRU 51A01 T/S	09ASE 2630
51A012	QPTS24	0	TESTC 23	09ASE 2631
51A013	QPTS24	0	TESTC*23	09ASE 2632
051E01	PTSN.K	33	TESTC 23	09ASE 2633
051E01	PTSN.K	67	TESTC 23	09ASE 2634
051E01	CTSC	0	TESTC 23	09ASE 2635
51E011	LPTS25	0	TESTC 23	09ASE 2636
	LPTS25	4	TESTC LRU 51E01 T/S	09ASE 2637

51E412	QPTS25	51E413	0	TESTC 23	12 29L	DBASE 2639
51E413	QPTS25		0	TESTC*23		DBASE 2639
51E414	PTSN K	51E415	E	16 TESTC 23		DBASE 2640
51E415	PTSN K		E	84 TESTC 23		DBASE 2641
51E416	QTSK		0	TESTC 23		DBASE 2642
51E417	LPTS25	51E418	0	TESTC 23		DBASE 2643
	LPTS26		4	TESTC	LPU 51E419 T/S	DBASE 2644
51E419	QPTS25	51E420	0	TESTC 23	14 29L	DBASE 2645
51E420	QPTS26		0	TESTC*23		DBASE 2646
52E411	PTSN K	52E412	E	17 TESTC 23		DBASE 2647
52E412	PTSN K		E	83 TESTC 23		DBASE 2648
52E413	QTSK		0	TESTC 23		DBASE 2649
52E414	LPTS27	52E415	0	TESTC 23		DBASE 2650
52E415	QPTS27	52E416	0	TESTC 23		DBASE 2651
52E416	QPTS27		0	TESTC 23		DBASE 2652
			4	TESTM	T/S FOR MICROWAVE EQUIP	DBASE 2653
74FJ11	PTSN K	74FJ12	E	36 TESTM 23		DBASE 2654
74FJ12	PTSN K		E	64 TESTM 23		DBASE 2655
74FJ13	QTSK		0	TESTM 23		DBASE 2656
74FJ14	LPTS31	74FJ15	0	TESTM 23		DBASE 2657
	LPTS32		4	TESTM	LPU 74FJ16 T/S	DBASE 2658
74FJ16	QPTS31	74FJ17	0	TESTM 23	15 29L	DBASE 2659
74FJ17	QPTS32		0	TESTM*23		DBASE 2660
74FJ18	PTSN K	74FJ19	E	36 TESTM 23		DBASE 2661
74FJ19	PTSN K		E	64 TESTM 23		DBASE 2662
74FJ20	QTSK		0	TESTM 23		DBASE 2663
74FJ21	LPTS31	74FJ22	0	TESTM 23		DBASE 2664
	LPTS32		4	TESTM	LPU 74FJ23 T/S	DBASE 2665
74FJ23	QPTS31	74FJ24	0	TESTM 23	15 29L	DBASE 2666
74FJ24	QPTS32		0	TESTM*23		DBASE 2667
74FJ25	PTSN K	74FJ26	E	66 TESTM 23		DBASE 2668
74FJ26	PTSN K		E	94 TESTM 23		DBASE 2669
74FJ27	QTSK		0	TESTM 23		DBASE 2670
74FJ28	LPTS32	74FJ29	0	TESTM 23		DBASE 2671
	LPTS33		4	TESTM	LPU 74FJ30 T/S	DBASE 2672
74FJ30	QPTS32	74FJ31	0	TESTM 23	25 29L	DBASE 2673
74FJ31	QPTS33		0	TESTM*23		DBASE 2674
74FJ32	PTSN K	74FJ33	E	17 TESTM 23		DBASE 2675
74FJ33	PTSN K		E	83 TESTM 23		DBASE 2676
74FJ34	QTSK		0	TESTM 23		DBASE 2677
74FJ35	LPTS33	74FJ36	0	TESTM 23		DBASE 2678
	LPTS34		4	TESTM	LPU 74FJ37 T/S	DBASE 2679
74FJ37	QPTS33	74FJ38	0	TESTM 23	14 29L	DBASE 2680
74FJ38	QPTS34		0	TESTM*23		DBASE 2681
76CA11	PTSN K	76CA12	E	38 TESTM 23		DBASE 2682
76CA12	PTSN K		E	94 TESTM 23		DBASE 2683
76CA13	QTSK		0	TESTM 23		DBASE 2684
76CA14	LPTS34	76CA15	0	TESTM 23		DBASE 2685
	LPTS35		4	TESTM	LPU 76CA16 T/S	DBASE 2686
76CA16	QPTS34	76CA17	0	TESTM 23	25 29L	DBASE 2687
76CA17	QPTS35		0	TESTM*23		DBASE 2688
			4	TESTD	T/S FOR DISPLAYS	DBASE 2689
13HA11	PTSN K	13HA12	E	17 TESTD 23		DBASE 2690
13HA12	PTSN K		E	83 TESTD 23		DBASE 2691
13HA13	QTSK		0	TESTD 23		DBASE 2692
13HA14	LPTS35	13HA15	0	TESTD 23		DBASE 2693
	LPTS36		4	TESTD	LPU 13HA16 T/S	DBASE 2694
13HA16	QPTS35	13HA17	0	TESTD 23	13 29L	DBASE 2695
13HA17	QPTS36		0	TESTD*23		DBASE 2696
74KC11	PTSN K	74KC12	E	30 TESTD 23		DBASE 2697
74KC12	PTSN K		E	68 TESTD 23		DBASE 2698
74KC13	QTSK		0	TESTD 23		DBASE 2699
74KC14	LPTS36	74KC15	0	TESTD 23		DBASE 2700
	LPTS37		4	TESTD	LPU 74KC16 T/S	DBASE 2701
74KC16	QPTS36	74KC17	0	TESTD 23	12 29L	DBASE 2702
74KC17	QPTS37		0	TESTD*23		DBASE 2703

G74J01	PTSNK 7-JC01	E	19	TESTO 23	DBASE 2704
G74J02	PTSNK	E	91	TESTO 23	DBASE 2705
G74J03	PTSD	C		TESTO 23	DBASE 2706
74J01	LPTS37 74JC02	J		TESTO 23	DBASE 2707
	LPTS37	4		TESTO LRU 7-JC01 T/S	DBASE 2708
74J02	QPTS37 74JC03	J		TESTO 23 12 29L	DBASE 2709
74J03	GPTS37	J		TESTO*23	DBASE 2710
G6534	PTSNK 653M01	E	1	TESTO 23	DBASE 2711
G6534	PTSNK	E	91	TESTO 23	DBASE 2712
G6534	PTSD	C		TESTO 23	DBASE 2713
653M11	LPTS39 653M02	J		TESTO 23	DBASE 2714
	LPTS39	4		TESTO LRU 653M01 T/S	DBASE 2715
653M12	QPTS39 653M03	J		TESTO 23 12 29L	DBASE 2716
653M13	GPTS39	J		TESTO*23	DBASE 2717
6463FA	PTSNK 6463FA1	E	16	TESTO 23	DBASE 2718
6463FA	PTSNK	E	94	TESTO 23	DBASE 2719
6463FA	PTSD	C		TESTO 23	DBASE 2720
6463FA	LPTS39 6463FA2	J		TESTO 23	DBASE 2721
	LPTS39	4		TESTO LRU 6463FA T/S	DBASE 2722
6463FA2	QPTS39 6463FA3	J		TESTO 23 13 29L	DBASE 2723
6463FA3	GPTS39	J		TESTO*23	DBASE 2724
51N11	PTSNK 51N11	E	12	TESTO 23	DBASE 2725
51N11	PTSNK	E	63	TESTO 23	DBASE 2726
51N11	PTSD	C		TESTO 23	DBASE 2727
51N11	LPTS-1 51N112	J		TESTO 23	DBASE 2728
	LPTS-1	4		TESTO LRU 51N11 T/S	DBASE 2729
51N112	QPTS-1 51N113	J		TESTO 23 12 29L	DBASE 2730
51N113	GPTS-1	J		TESTO*23	DBASE 2731
G74K1	PTSNK 74KA1	E	24	TESTO 23	DBASE 2732
G74K1	PTSNK	E	76	TESTO 23	DBASE 2733
G74K1	PTSD	C		TESTO 23	DBASE 2734
74KA1	LPTS-1 74KA02	J		TESTO 23	DBASE 2735
	LPTS-1	4		TESTO LRU 74KA1 T/S	DBASE 2736
74KA12	QPTS-1 74KA13	J		TESTO 23 13 29L	DBASE 2737
74KA13	GPTS-1	J		TESTO*23	DBASE 2738
G51N3	PTSNK 51N301	E	32	TESTO 23	DBASE 2739
G51N3	PTSNK	E	68	TESTO 23	DBASE 2740
G51N3	PTSD	C		TESTO 23	DBASE 2741
51N31	LPTS-2 51N302	J		TESTO 23	DBASE 2742
	LPTS-2	4		TESTO LRU 51N301 T/S	DBASE 2743
51N312	QPTS-2 51N303	J		TESTO 23 12 29L	DBASE 2744
51N313	GPTS-2	J		TESTO*23	DBASE 2745
G74FF1	PTSNK 74FF1	E	19	TESTO 23	DBASE 2746
G74FF1	PTSNK	E	91	TESTO 23	DBASE 2747
G74FF1	PTSD	C		TESTO 23	DBASE 2748
74FF1	LPTS-3 74FF12	J		TESTO 23	DBASE 2749
	LPTS-3	4		TESTO LRU 74FF1 T/S	DBASE 2750
74FF12	QPTS-3 74FF13	J		TESTO 23 12 29L	DBASE 2751
74FF13	GPTS-3	J		TESTO*23	DBASE 2752
G75M1	PTSNK 75M01	E	35	TESTO 23	DBASE 2753
G75M1	PTSNK	E	91	TESTO 23	DBASE 2754
G75M1	PTSD	C		TESTO 23	DBASE 2755
75M01	LPTS-4 75M02	J		TESTO 23	DBASE 2756
	LPTS-4	4		TESTO LRU 75M01 T/S	DBASE 2757
75M012	QPTS-4 75M03	J		TESTO 23 12 29L	DBASE 2758
75M013	GPTS-4	J		TESTO*23	DBASE 2759
G75M1	PTSNK 75M01	E	39	TESTO 23	DBASE 2760
G75M1	PTSNK	E	91	TESTO 23	DBASE 2761
G75M1	PTSD	C		TESTO 23	DBASE 2762
75M11	LPTS-5 75M12	J		TESTO 23	DBASE 2763
	LPTS-5	4		TESTO LRU 75M10 T/S	DBASE 2764
75M112	QPTS-5 75M13	J		TESTO 23 12 29L	DBASE 2765
75M113	GPTS-5	J		TESTO*23	DBASE 2766
G74J1	PTSNK 74JA1	E	37	TESTO 23	DBASE 2767
G74J1	PTSNK	E	63	TESTO 23	DBASE 2768
G74J1	PTSD	C		TESTO 23	DBASE 2769

74J411	LOTS46	74J412	0	TEST0 23		ORASE 2777
	LOTS-6		4	TEST0	LEU 74JA T/S	ORASE 2771
74J412	OTS-46	74J413	3	TEST0 23	23 29L	ORASE 2772
74J412	OTS-5		0	TEST0*23		ORASE 2773
			4	TSC	TSC TEST STATION	ORASE 2774
CTSC	DU-TSC	CTSC1	0	TSC - 23	01 C TSC	ORASE 2775
CTSC1	DO-NTA	TSC1	0	TSC 23		ORASE 2776
TS21	FTSC	TS22	F	65 TSC 23		ORASE 2777
TS22	OTSC	TS23	0	TSC 23	53 29L	ORASE 2778
TS23	OTSC		0	TSC *23		ORASE 2779
			4	TSM	TSM TEST STATION	ORASE 2780
CTSM	DU-TSM	CTSM1	0	TSM 23	01 C TSM	ORASE 2781
CTSM1	DO-NTA	TSM1	0	TSM 23		ORASE 2782
TS41	FTSM	TS42	F	65 TSM 23		ORASE 2783
TS42	OTSM	TS43	0	TSM 23	50 29L	ORASE 2784
TS43	OTSM		0	TSM *23		ORASE 2785
			4	TSD	TSD TEST STATION	ORASE 2786
CTSD	DU-TSD	CTSD1	0	TSD 23	01 C TSD	ORASE 2787
CTSD1	DO-NTA	TSD1	0	TSD 23		ORASE 2788
TS21	FTSD	TS22	F	65 TSD 23		ORASE 2789
TS22	OTSD	TS23	0	TSD 23	50 29L	ORASE 2790
TS23	OTSD		0	TSD *23		ORASE 2791

APPENDIX B

F-15 TFTW OPERATIONS DATA FILE

APPENDIX B

F-15 TFW OPERATIONS DATA FILE

1. The operational scenarios contained in this appendix use scheduled aircraft sortie rates of .43, .74, and 1.0. Each scenario schedules aircraft flying and maintenance activity Monday through Friday. The same schedule is repeated each week during the simulation.

2. Explanation of Aircraft Mission Names:

a. PFLTF and PFLTTF are dummy missions that make a specified number of corresponding F-15 and TF-15 aircraft unavailable each day.

b. AAXX designates Air-Air Missions. The third character defines aircraft type: one is a TF-15 and two is an F-15. The fourth character defines the type of aircraft processing and number of times an aircraft flies each day: one is preflight to thruflight, two is thruflight to thruflight, three is thruflight to postflight, and four is preflight to postflight.

c. CONVXX designates conversion missions. The fifth character defines the aircraft type: one is a TF-15 and two is an F-15. The sixth character defines the type of aircraft processing and number of times an aircraft flies each day: one is preflight to thruflight, two is thruflight to postflight, three is thruflight to thruflight, and four is preflight to postflight.

d. PHASF and PHASTF are F-15 and TF-15 aircraft scheduled for Phase Inspection.

e. WASHF and WASHTF are F-15 and TF-15 aircraft scheduled for Washing and Corrosion Control Inspection.

3. Explanation of Column Headings:

- a. TIME - Daily simulation time when an aircraft begins mission processing.
- b. MISSION - Mission name.
- c. A/C TYPE - self explanatory.
- d. SCHED - number of aircraft scheduled for a given mission.
- e. MIN - minimum number of aircraft required to fly a given mission.
- f. SPARE - identifies preparation of spare aircraft for a given mission. If the spare is not used for the mission it is designated for, it then becomes a spare for the next mission.
- g. PRIORITY - LCOM peculiar code that allows an order of importance to mission scheduling.
- h. TAKEOFF - scheduled takeoff time 24 hour clock.
- i. LATENESS - time remaining after scheduled takeoff time before mission cancellation.
- j. SORTIE LENGTH - sortie length in hours and minutes.

43 OPERATIONAL SCENARIO

DAY 1

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	AA21	F15	2	2	1	2	501	2+ 0	1+31
114	CONV21	F15	2	2	1	2	545	2+ 0	1+43
130	CONV11	TF15	2	2	1	2	600	2+ 0	1+13
144	AA11	TF15	1	1	0	2	615	2+ 0	1+ 7
215	AA14	TF15	2	2	0	2	645	2+ 0	2+31
229	AA21	F15	1	1	0	2	700	2+ 0	1+20
329	AA14	TF15	1	1	0	2	800	2+ 0	0+08
349	AA24	F15	3	3	0	2	820	2+ 0	1+19
500	CONV26	F15	2	2	0	2	930	2+ 0	1+23
649	AA24	F15	1	1	0	2	1120	2+ 0	0+54
649	AA14	TF15	2	2	0	2	1120	2+ 0	1+ 7
730	CONV12	TF15	1	1	0	2	1200	2+ 0	1+23
741	PHASF	F15	1	1	0	2	800	5+ 0	2+ 5
741	PHASTF	TF15	1	1	0	2	800	5+ 0	2+ 5
789	PELTYF	TF15	14	2	0	3	1200	6+ 0	12+ 0
799	PELTF	F15	31	2	0	3	1200	6+ 0	12+ 0
1009	AA24	F15	2	2	0	2	1440	2+ 0	1+13
1030	AA13	TF15	1	1	0	2	1500	2+ 0	0+56
1059	AA23	F15	2	2	0	2	1630	2+ 0	1+ 4
1230	AA23	F15	1	1	0	2	1700	2+ 0	1+14
1300	CONV12	TF15	1	1	0	2	1730	2+ 0	1+16
1315	CONV22	F15	2	2	0	2	1745	2+ 0	1+21

DAY 2

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
99	AA11	TF15	2	2	1	2	530	2+ 0	0+57
144	CONV21	F15	2	2	1	2	615	2+ 0	1+18
229	CONV24	F15	2	2	0	2	700	2+ 0	1+25
245	AA14	TF15	2	2	0	2	715	2+ 0	1+ 9
400	AA21	F15	1	1	0	2	730	2+ 0	1+54
430	AA21	F15	2	2	0	2	900	2+ 0	1+ 6
430	AA14	TF15	1	1	0	2	900	2+ 0	1+15
510	CONV11	TF15	1	1	1	2	940	2+ 0	1+13
614	CONV22	F15	2	2	0	2	1045	2+ 0	1+15
620	AA24	F15	2	2	0	2	1050	2+ 0	1+25
645	AA24	F15	2	2	0	2	1115	2+ 0	1+ 3
730	WASHF	F15	1	1	0	2	800	5+ 0	2+ 7
730	AA24	F15	2	2	0	2	1200	2+ 0	1+52
730	AA14	TF15	1	1	0	2	1200	2+ 0	1+10
741	PHASF	F15	1	1	0	2	800	5+ 0	2+ 7
900	PELTYF	TF15	14	2	0	3	1200	6+ 0	12+ 0
900	PELTF	F15	31	2	0	3	1200	6+ 0	12+ 0
929	AA23	F15	2	2	0	2	1300	2+ 0	1+ 3
1100	CONV12	TF15	1	1	0	2	1530	2+ 0	1+32
1310	AA23	F15	1	1	0	2	1740	2+ 0	1+ 1
1310	AA13	TF15	2	2	0	2	1740	2+ 0	1+13
1600	CONV14	TF15	1	1	0	2	2030	2+ 0	2+20

DAY 3

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	AA21	F15	2	2	1	2	500	2+ 0	0+50
100	CONV11	TF15	1	1	0	2	530	2+ 0	1+20
104	CONV21	F15	2	2	1	2	535	2+ 0	1+14
142	AA11	TF15	2	2	1	2	615	2+ 0	0+57
215	AA14	TF15	1	1	0	2	645	2+ 0	2+25
230	AA21	F15	1	1	0	2	700	2+ 0	1+20
329	AA14	TF15	1	1	0	2	800	2+ 0	1+ 0
350	AA24	F15	3	3	0	2	820	2+ 0	1+10
430	AA21	F15	1	1	1	2	900	2+ 0	0+56
499	CONV24	F15	3	3	0	2	930	2+ 0	1+22
557	AA22	F15	2	2	0	2	1030	2+ 0	1+10
647	AA24	F15	1	1	0	2	1120	2+ 0	1+ 5
650	AA14	TF15	1	1	0	2	1120	2+ 0	0+55
700	CONV14	TF15	1	1	0	2	1130	2+ 0	1+29
730	WASHF	F15	1	1	0	2	800	5+ 0	2+ 6
730	CONV12	TF15	1	1	0	2	1200	2+ 0	1+29
741	PHASF	F15	1	1	0	2	800	5+ 0	2+ 7
799	PELTYF	TF15	16	2	0	3	1200	6+ 0	12+ 0
799	PELTF	F15	29	2	0	3	1200	6+ 0	12+ 0
1010	AA24	F15	1	1	0	2	1440	2+ 0	1+13
1030	AA13	TF15	2	2	0	2	1500	2+ 0	0+51
1229	AA23	F15	2	2	0	2	1700	2+ 0	1+ 5
1314	CONV22	F15	1	1	0	2	1745	2+ 0	1+23
1330	CONV22	F15	1	1	0	2	1800	2+ 0	1+13
1345	AA23	F15	2	2	0	2	1815	2+ 0	1+17

DAY 6

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
100	AA11	TF15	1	1	1	2	930	2+ 0	0+50
145	CONV21	F15	3	3	1	2	615	2+ 0	1+23
169	AA21	F15	2	2	1	2	620	2+ 0	0+55
248	CONV24	F15	1	1	0	2	710	2+ 0	1+24
244	AA14	TF15	2	2	0	2	715	2+ 0	1+12
300	AA21	F15	3	3	0	2	730	2+ 0	2+11
329	AA14	TF15	1	1	0	2	800	2+ 0	0+59
408	CONV14	TF15	2	2	1	2	830	2+ 0	1+58
430	AA21	F15	2	2	0	2	900	2+ 0	1+ 1
430	AA14	TF15	1	1	0	2	900	2+ 0	1+ 3
644	AA24	F15	1	1	0	2	1115	2+ 0	0+55
730	WASHF	F15	1	1	0	2	800	5+ 0	2+ 5
741	PHASF	F15	1	1	0	2	800	5+ 0	2+ 5
759	PFLTTF	F15	31	2	0	3	1200	6+ 0	12+ 0
759	PFLTTF	TF15	14	2	0	3	1200	6+ 0	12+ 0
870	AA23	F15	3	3	0	2	1300	2+ 0	0+57
900	AA24	F15	1	1	0	2	1330	2+ 0	1+24
900	AA14	TF15	1	1	0	2	1330	2+ 0	1+17
919	CONV22	F15	3	3	0	2	1350	2+ 0	1+31
1245	AA21	F15	2	2	0	2	1715	2+ 0	1+19
1310	AA23	F15	1	1	0	2	1740	2+ 0	1+ 4
1310	AA13	TF15	1	1	0	2	1740	2+ 0	1+11
1330	AA23	F15	1	1	0	2	1800	2+ 0	0+58

DAY 5

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
30	AA21	F15	2	2	1	2	500	2+ 0	0+59
99	CONV11	TF15	1	1	0	2	930	2+ 0	1+23
142	AA11	TF15	3	3	1	2	615	2+ 0	1+ 2
200	CONV14	TF15	1	1	0	2	630	2+ 0	1+45
229	AA21	F15	2	2	1	2	700	2+ 0	1+28
300	CONV21	F15	3	3	1	2	730	2+ 0	1+53
390	AA24	F15	3	3	0	2	820	2+ 0	1+17
500	CONV24	F15	1	1	0	2	930	2+ 0	1+16
929	AA24	F15	2	2	0	2	1000	2+ 0	1+ 1
647	AA24	F15	1	1	0	2	1120	2+ 0	1+ 3
650	AA14	TF15	1	1	0	2	1120	2+ 0	0+53
730	WASHF	TF15	1	1	0	2	800	5+ 0	2+ 6
730	CONV12	TF15	1	1	0	2	1200	2+ 0	1+25
742	PHASTF	TF15	1	1	0	2	800	5+ 0	2+ 5
800	PFLTTF	F15	30	2	0	3	1200	6+ 0	12+ 0
800	PFLTTF	TF15	15	2	0	3	1200	6+ 0	12+ 0
1010	AA24	F15	1	1	0	2	1440	2+ 0	1+ 7
1030	AA13	TF15	3	3	0	2	1500	2+ 0	0+55
1100	AA23	F15	2	2	0	2	1530	2+ 0	1+11
1230	AA23	F15	2	2	0	2	1700	2+ 0	1+23
1315	CONV22	F15	3	3	0	2	1745	2+ 0	1+38

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DAY 1

TIME	MISSION	A/C TYPE	SCMD	THIN	ISPA-EI	PRIORITY	TAKEOFF	LATENCY	FO-TIE LENGTH
29	AK21	F15	2	2	1	2	900	200	1000
100	CONV11	TF15	1	1	0	2	530	200	1011
110	CONV21	F15	2	2	1	2	900	200	1012
130	CONV11	TF15	2	2	1	2	600	200	1015
145	AK11	TF15	1	1	0	2	610	200	1020
159	CONV10	TF15	4	2	1	2	630	200	1030
219	AK10	TF15	2	2	0	2	840	200	1027
230	AK21	F15	1	3	0	2	700	200	1020
329	AK10	TF15	1	1	0	2	900	200	1000
350	AK24	F15	3	3	1	2	820	200	1011
400	AK21	F15	2	2	0	2	830	200	1020
414	AK21	F15	2	2	0	2	845	200	1005
459	CONV20	F15	2	2	0	2	900	200	1000
530	AK24	F15	2	2	0	2	1000	200	1053
600	AK22	F15	1	2	0	2	1000	200	1011
650	AK24	F15	1	1	0	2	1120	200	1007
690	AK20	TF15	1	1	0	2	1120	200	1000
700	CONV10	TF15	1	1	0	2	1130	200	1000
730	AK5HP	F15	1	1	0	2	900	200	1000
730	CONV12	TF15	1	1	0	2	1200	200	1013
741	AK10	F15	1	1	0	2	800	200	1000
741	AK45P	F15	1	1	0	2	800	200	1007
741	AK45P	TF15	1	1	0	2	800	200	1000
759	AK17P	TF15	4	2	0	3	1200	600	1000
759	AK17P	F15	10	2	0	3	1200	600	1000
1009	AK20	F15	3	3	0	2	1000	200	1012
1030	AK10	TF15	2	2	0	2	1000	200	1000
1059	AK23	F15	2	2	0	2	1530	200	1008
1139	AK23	F15	3	3	0	2	1610	200	1001
1229	AK23	F15	2	2	0	2	1700	200	1007
1300	CONV12	TF15	1	1	0	2	1700	200	1000
1314	CONV22	F15	2	2	0	2	1745	200	1027
1645	AK23	F15	2	2	0	2	2115	200	1007

DAY 2

TIME	MISSION	A/C TYPE	SCMD	THIN	ISPA-EI	PRIORITY	TAKEOFF	LATENCY	FO-TIE LENGTH
100	AK21	F15	2	2	1	2	530	200	1005
130	CONV20	TF15	2	2	1	2	600	200	1007
145	CONV21	F15	2	2	1	2	610	200	1020
190	AK21	F15	2	2	1	2	630	200	1000
230	CONV20	F15	2	2	0	2	700	200	1020
240	AK10	TF15	2	2	1	2	710	200	1000
300	AK21	F15	3	3	0	2	730	200	1000
349	AK21	F15	2	2	0	2	710	200	1007
430	AK21	F15	1	1	0	2	900	200	1012
430	AK10	TF15	1	1	0	2	900	200	1000
509	CONV11	TF15	2	2	0	2	940	200	1021
600	CONV10	TF15	2	2	0	2	1000	200	1021
615	CONV22	F15	2	2	0	2	1045	200	1001
629	AK20	F15	2	2	0	2	1090	200	1000
645	AK20	F15	2	2	0	2	1115	200	1000
700	AK23	F15	2	2	0	2	1200	200	1000
730	AK5HP	F15	1	1	0	2	900	200	1000
730	AK20	F15	2	2	0	2	1000	200	1000
741	AK10	TF15	1	1	0	2	800	200	1000
741	AK45P	F15	1	1	0	2	800	200	1000
741	AK45P	TF15	1	1	0	2	800	200	1000
759	AK17P	TF15	4	2	0	3	1200	600	1000
759	AK17P	F15	10	2	0	3	1200	600	1000
830	AK23	F15	3	3	0	2	1000	200	1000
900	AK20	F15	1	1	0	2	1330	200	1007
900	AK10	TF15	1	1	0	2	1330	200	1000
1045	CONV22	F15	2	2	0	2	1515	200	1010
1059	CONV12	TF15	2	2	0	2	1530	200	1000
1130	CONV20	F15	2	2	0	2	1600	200	1020
1239	CONV20	F15	1	1	0	2	1700	200	1000
1239	CONV12	TF15	1	1	0	2	1700	200	1012
1300	AK23	F15	2	2	0	2	1700	200	1000
1309	AK23	F15	1	1	0	2	1700	200	1000
1309	AK10	TF15	1	1	0	2	1700	200	1000
1330	AK23	F15	2	2	0	2	1800	200	1000
1600	CONV10	TF15	2	2	0	2	1800	200	1000
1630	CONV12	TF15	2	2	0	2	2100	200	1000

DAY 5										
TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENCY	COAST LENGTH	
30	AA21	P19	2	2	1	2	500	20	1000	
50	CONV11	TF15	1	1	0	2	530	20	1025	
130	CONV11	TF15	2	2	1	2	600	20	1027	
142	AA11	TF15	1	1	0	2	615	20	102	
200	CONV19	TF19	4	4	1	2	630	20	1000	
215	AA14	TF15	2	2	0	2	645	20	2015	
229	AA21	P19	3	3	1	2	700	20	1019	
300	CONV21	P15	2	2	1	2	730	20	1000	
330	AA14	TF19	1	1	0	2	800	20	1000	
349	AA24	P15	3	3	1	2	820	20	106	
399	AA20	P19	2	2	0	2	830	20	1009	
415	AA21	P15	2	2	0	2	845	20	105	
500	CONV20	P15	2	2	0	2	850	20	1015	
529	AA24	P15	2	2	0	2	900	20	1052	
557	AA22	P15	2	2	0	2	910	20	1015	
647	AA20	P15	1	1	0	2	1100	20	103	
649	AA14	TF19	1	1	0	2	1120	20	1053	
659	CONV14	TF15	1	1	0	2	1130	20	1018	
730	AA24	TF19	1	1	0	2	1140	20	1009	
730	CONV12	TF15	1	1	0	2	1200	20	1032	
900	AA14	P19	22	22	0	3	1200	60	1200	
900	AA14	TF15	6	2	0	3	1200	60	1200	
1009	AA24	P15	3	3	0	2	1400	20	1011	
1030	AA13	TF15	1	1	0	2	1500	20	1056	
1100	AA21	P15	2	2	0	2	1500	20	1010	
1129	AA23	P15	3	3	0	2	1610	20	103	
1230	AA21	P15	2	2	0	2	1700	20	1020	
1259	CONV12	TF15	1	1	0	2	1730	20	1033	
1315	CONV22	P15	2	2	0	2	1740	20	1017	
1644	AA23	P15	2	2	0	2	2115	20	2000	

1.0 OPERATIONAL SCENARIO

DAY 1									
TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	AA21	F15	2	2	1	2	500	2+0	1+31
59	PHASF	F15	1	1	0	2	810	5+0	2+7
59	PHASF	F15	1	1	0	2	800	5+0	2+5
99	PHASTF	TF15	1	1	0	2	800	5+0	2+6
99	WASHF	F15	1	1	0	2	800	5+0	2+6
180	CONV11	TF15	1	1	0	2	530	2+0	1+28
109	AA11	TF15	2	2	1	2	540	2+0	0+53
109	AA21	F15	2	2	0	2	540	2+0	1+6
114	CONV21	F15	2	2	1	2	545	2+0	1+23
130	CONV11	TF15	2	2	1	2	600	2+0	1+23
140	AA21	F15	2	2	0	2	610	2+0	2+28
144	AA11	TF15	1	1	0	2	615	2+0	0+59
154	CONV14	TF15	4	2	1	2	630	2+0	1+31
215	AA14	TF15	2	2	0	2	645	2+0	2+6
224	AA21	F15	1	3	0	2	700	2+0	1+31
239	CONV11	TF15	1	1	0	2	710	2+0	1+21
380	CONV24	F15	2	2	1	2	730	2+0	1+15
314	CONV21	F15	1	1	0	2	745	2+0	1+26
329	AA14	TF15	1	1	0	2	800	2+0	0+54
349	AA24	F15	3	3	1	2	820	2+0	1+13
359	AA21	F15	2	2	0	2	830	2+0	1+8
415	AA21	F15	2	2	0	2	845	2+0	0+56
563	CONV24	F15	2	2	0	2	930	2+0	1+25
529	AA24	F15	2	2	0	2	1000	2+0	3+57
545	AA24	F15	1	1	0	2	1015	2+0	1+54
545	AA14	TF15	1	1	0	2	1015	2+0	2+1
680	AA22	F15	2	2	0	2	1030	2+0	1+15
649	AA24	F15	1	1	0	2	1120	2+0	0+52
649	AA14	TF15	1	1	0	2	1120	2+0	0+53
700	CONV14	TF15	1	1	0	2	1130	2+0	1+39
715	AA23	F15	2	2	0	2	1145	2+0	1+16
725	AA13	TF15	2	2	0	2	1155	2+0	1+27
730	CONV12	TF15	1	1	0	2	1200	2+0	1+32
799	PFLTF	TF15	3	2	0	3	1200	6+0	12+0
799	PFLTF	F15	11	2	0	3	1200	6+0	12+0
829	AA23	F15	2	2	0	2	1300	2+0	2+9
1009	AA24	F15	3	3	0	2	1440	2+0	1+29
1030	AA13	TF15	2	2	0	2	1500	2+0	1+3
1344	CONV22	F15	1	1	0	2	1515	2+0	1+32
1059	AA23	F15	2	2	0	2	1530	2+0	1+1
1129	CONV12	TF15	1	1	0	2	1600	2+0	1+26
1139	AA23	F15	3	3	0	2	1610	2+0	1+3
1236	AA23	F15	2	2	0	2	1700	2+0	1+0
1300	CONV12	TF15	1	1	0	2	1730	2+0	1+28
1315	CONV22	F15	2	2	0	2	1745	2+0	1+14
1645	AA23	F15	2	2	0	2	2115	2+0	2+6

DAY 2

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
99	AA21	F15	2	2	1	2	530	2+0	1+5
100	MASHF	F15	1	1	0	2	600	5+0	2+5
100	PHASTF	TF15	1	1	0	2	600	5+0	2+6
100	PHASF	F15	1	1	0	2	600	5+0	2+5
100	PHASF	F15	1	1	0	2	600	5+0	2+5
110	CONV24	F15	1	1	1	2	540	2+0	1+22
111	CONV24	F15	1	1	0	2	542	2+0	1+22
115	CONV24	F15	1	1	0	2	545	2+0	1+31
130	CONV11	TF15	2	2	1	2	600	2+0	1+17
144	CONV21	F15	2	2	1	2	615	2+0	1+29
150	AA21	F15	2	2	1	2	620	2+0	1+0
210	CONV11	TF15	1	1	0	2	640	2+0	1+29
229	CONV24	F15	2	2	0	2	700	2+0	1+39
245	AA14	TF15	2	2	1	2	715	2+0	1+13
300	AA21	F15	3	3	0	2	730	2+0	1+53
345	AA21	F15	2	2	0	2	815	2+0	1+16
359	AA24	F15	2	1	0	2	830	2+0	1+11
359	AA14	TF15	1	1	0	2	830	2+0	1+2
415	AA24	F15	1	1	0	2	845	2+0	1+4
415	AA14	TF15	1	1	0	2	845	2+0	0+50
430	AA21	F15	1	1	0	2	900	2+0	1+11
430	AA14	TF15	1	1	0	2	900	2+0	1+6
510	CONV11	TF15	2	2	0	2	940	2+0	1+24
529	AA21	F15	2	1	0	2	1000	2+0	1+12
529	AA11	TF15	1	1	0	2	1000	2+0	1+11
600	CONV11	TF15	2	2	0	2	1030	2+0	1+8
614	CONV22	F15	2	2	0	2	1045	2+0	1+15
620	AA24	F15	2	2	0	2	1050	2+0	1+1
645	AA24	F15	2	2	0	2	1115	2+0	0+52
659	AA23	F15	2	2	0	2	1136	2+0	0+55
730	AA24	F15	2	2	0	2	1200	2+0	1+40
800	PFLTTF	TF15	5	2	0	3	1200	6+0	12+0
800	PFLTTF	F15	9	2	0	3	1200	6+0	12+0
829	AA23	F15	3	3	0	2	1300	2+0	0+53
900	AA24	F15	1	1	0	2	1330	2+0	1+8
900	AA14	TF15	1	1	0	2	1330	2+0	1+24
930	CONV12	TF15	1	1	0	2	1400	2+0	1+30
1044	CONV22	F15	2	2	0	2	1515	2+0	1+31
1100	CONV12	TF15	2	2	0	2	1530	2+0	1+32
1129	CONV24	F15	2	2	0	2	1600	2+0	1+15
1240	CONV24	F15	1	1	0	2	1710	2+0	1+23
1240	CONV12	TF15	1	1	0	2	1710	2+0	1+21
1300	AA23	F15	2	2	0	2	1730	2+0	1+11
1310	AA23	F15	1	1	0	2	1740	2+0	1+11
1310	AA13	TF15	1	1	0	2	1740	2+0	1+14
1330	AA23	F15	2	2	0	2	1800	2+0	1+2
1400	AA23	F15	2	2	0	2	1830	2+0	2+18
1400	AA13	TF15	1	1	0	2	1830	2+0	2+26
1600	CONV14	TF15	2	2	0	2	2030	2+0	2+22
1630	CONV12	TF15	2	2	0	2	2100	2+0	1+16

DAY 3

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
29	AA21	F15	2	2	1	2	5.0	2+ 0	1+ 1
59	MASHTF	TF15	1	1	0	2	8.0	5+ 0	2+ 6
59	PHASF	F15	1	1	0	2	8.0	5+ 0	2+ 5
59	PHASF	F15	1	1	0	2	8.0	5+ 0	2+ 6
59	PHASTF	TF15	1	1	0	2	8.0	5+ 4	2+ 6
59	MASHF	F15	1	1	0	2	8.0	5+ 0	2+ 5
100	CONV12	TF15	1	1	0	2	53J	2+ 0	1+19
104	CONV21	F15	2	2	0	2	535	2+ 0	1+17
130	CONV11	TF15	2	2	1	2	60J	2+ 0	1+23
142	AA11	TF15	1	1	0	2	615	2+ 0	1+ 9
159	CONV14	TF15	4	2	1	2	630	2+ 0	1+59
215	AA14	TF15	2	2	0	2	645	2+ 0	2+20
230	AA21	F15	3	3	0	2	700	2+ 0	1+23
244	AA24	F15	2	2	0	2	715	2+ 0	1+12
244	AA11	TF15	1	1	0	2	715	2+ 0	1+ 2
250	CONV21	F15	1	1	1	2	720	2+ 0	1+30
300	CONV21	F15	1	1	0	2	730	2+ 0	1+12
315	AA21	F15	2	2	1	2	745	2+ 0	2+14
315	AA11	TF15	1	1	0	2	745	2+ 0	2+25
329	AA14	TF15	1	1	0	2	80J	2+ 0	1+ 5
356	AA24	F15	3	3	0	2	820	2+ 0	1+ 5
430	AA21	F15	3	3	0	2	94J	2+ 0	0+50
459	CONV24	F15	2	2	0	2	93J	2+ 0	1+35
530	AA24	F15	2	2	0	2	100J	2+ 0	0+54
530	CONV24	F15	1	1	0	2	1030	2+ 0	1+22
557	AA22	F15	2	2	0	2	1030	2+ 0	1+ 6
647	AA24	F15	1	1	0	2	112J	2+ 0	0+55
650	AA14	TF15	1	1	0	2	112J	2+ 0	0+57
700	CONV14	TF15	1	1	0	2	1130	2+ 0	1+15
730	CONV12	TF15	1	1	0	2	1200	2+ 0	1+29
735	CONV23	F15	2	2	0	2	1205	2+ 0	1+30
759	PFLTF	TF15	3	2	0	3	1200	6+ 0	12+ 0
759	PFLTF	F15	9	2	0	3	1200	6+ 0	12+ 0
759	AA14	TF15	1	1	0	2	1230	2+ 0	1+ 1
830	AA12	TF15	1	1	1	2	1300	2+ 0	1+10
830	AA24	F15	1	1	0	2	1300	2+ 0	1+14
1310	AA24	F15	3	3	0	2	1440	2+ 0	1+15
1030	AA13	TF15	1	1	0	2	1500	2+ 0	1+11
1130	CONV22	F15	1	1	0	2	1600	2+ 0	1+27
1140	CONV22	F15	1	1	0	2	1610	2+ 0	1+23
1200	AA24	F15	2	1	0	2	1630	2+ 0	0+56
1200	AA13	TF15	1	1	0	2	1630	2+ 0	1+ 2
1229	AA23	F15	2	2	0	2	1700	2+ 0	1+ 7
1300	CONV12	TF15	2	2	0	2	1730	2+ 0	1+25
1314	CONV22	F15	2	2	0	2	1745	2+ 0	1+29
1330	CONV22	F15	2	2	0	2	1800	2+ 0	1+36
1345	AA23	F15	2	2	0	2	1815	2+ 0	1+ 9
1430	AA23	F15	2	1	0	2	1900	2+ 0	0+55
1430	AA13	TF15	1	1	0	2	1900	2+ 0	0+52
1645	AA23	F15	2	2	0	2	2115	2+ 0	2+ 9

DAY 4

TIME	MISSION	A/C TYPE	SCHED (MIN)	(SPARE)	PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
59	WASHYP	TF15	1	1	0	2	800	5+0
59	WASHF	F15	1	1	0	2	800	2+6
59	PHASTF	F15	1	1	0	2	800	2+5
59	PHASTF	TF15	1	1	0	2	800	2+6
100	AA21	F15	2	2	1	2	530	1+3
130	CONV11	TF15	2	2	1	2	600	1+39
139	AA21	F15	2	2	0	2	610	2+31
139	AA11	TF15	1	1	0	2	610	2+5
149	CONV21	F15	2	2	1	2	615	1+24
149	AA21	F15	2	2	1	2	620	1+0
240	CONV24	F15	2	2	0	2	710	1+38
244	AA14	TF15	2	2	1	2	715	1+19
303	AA21	F15	3	3	0	2	730	2+9
315	CONV21	F15	1	1	0	2	745	1+36
329	AA14	TF15	2	2	1	2	800	1+12
345	AA21	F15	1	1	1	2	815	1+12
345	AA14	TF15	1	1	0	2	815	1+29
400	CONV14	TF15	2	2	0	2	830	2+21
430	AA21	F15	1	1	0	2	900	1+1
430	AA14	TF15	1	1	0	2	900	1+5
445	CONV11	TF15	1	1	0	2	915	1+31
459	CONV21	F15	1	1	0	2	930	1+36
630	CONV11	TF15	2	2	0	2	1030	1+16
645	AA24	F15	2	2	0	2	1115	0+57
700	AA22	F15	2	2	0	2	1130	1+3
710	AA22	F15	2	2	0	2	1140	1+3
730	AA24	F15	2	2	0	2	1230	1+49
759	PFLTF	F15	11	2	0	3	1230	12+0
759	PFLTF	TF15	2	2	0	3	1200	12+0
830	AA23	F15	3	3	0	2	1300	1+4
844	CONV24	F15	2	2	0	2	1315	1+33
900	AA24	F15	1	1	0	2	1330	1+13
900	AA14	TF15	1	1	0	2	1330	1+4
919	CONV22	F15	2	2	0	2	1350	1+23
929	AA13	TF15	1	1	0	2	1430	0+52
929	AA24	F15	2	1	0	2	1440	1+0
1030	AA24	F15	1	1	0	2	1500	2+6
1030	AA23	F15	1	1	0	2	1500	2+5
1059	AA24	F15	2	2	0	2	1530	1+18
1130	AA23	F15	2	2	0	2	1600	2+22
1240	CONV24	F15	1	1	0	2	1710	1+33
1240	CONV12	TF15	1	1	0	2	1710	1+23
1245	AA23	F15	2	2	0	2	1715	1+21
1310	AA23	F15	1	1	0	2	1740	1+25
1310	AA13	TF15	1	1	0	2	1740	1+5
1330	AA23	F15	2	2	0	2	1800	0+58
1500	CONV22	F15	1	1	0	2	1930	1+19
1515	CONV12	TF15	1	1	0	2	1945	1+27
1529	CONV22	F15	1	1	0	2	2000	1+28
1600	CONV14	TF15	2	2	0	2	2030	2+11
1630	CONV12	TF15	2	2	0	2	2100	1+25

DAY 5

TIME	MISSION	A/C TYPE	SCHED (MIN) (SPARE)			PRIORITY	TAKEOFF	LATENESS	SORTIE LENGTH
30	AA21	F15	2	2	1	2	500	2+ 0	0+54
59	CONV11	TF15	1	1	0	2	530	2+ 0	1+23
100	PHASF	F15	1	1	0	2	600	5+ 0	2+ 6
108	WASHF	F15	1	1	0	2	600	5+ 0	2+ 5
100	WASHTF	TF15	1	1	0	2	600	5+ 0	2+ 6
130	CONV11	TF15	2	2	1	2	600	2+ 0	1+39
142	AA11	TF15	1	1	0	2	615	2+ 0	0+57
200	CONV14	TF15	2	2	1	2	630	2+ 0	1+31
215	AA14	TF15	2	2	0	2	645	2+ 0	2+ 4
229	AA21	F15	3	3	1	2	700	2+ 0	1+16
300	CONV21	F15	2	2	1	2	730	2+ 0	1+59
314	AA21	F15	2	2	1	2	745	2+ 0	2+19
314	AA11	TF15	1	1	1	2	745	2+ 0	2+ 7
330	AA14	TF15	1	1	0	2	800	2+ 0	0+52
350	AA24	F15	3	3	1	2	820	2+ 0	1+10
359	AA21	F15	2	2	0	2	830	2+ 0	1+15
415	AA21	F15	2	2	0	2	845	2+ 0	1+ 6
430	AA21	F15	3	2	0	2	900	2+ 0	1+51
430	AA11	TF15	1	1	0	2	900	2+ 0	2+14
500	CONV24	F15	2	2	0	2	930	2+ 0	1+18
515	CONV21	F15	1	1	0	2	945	2+ 0	1+14
529	AA24	F15	2	2	0	2	1000	2+ 0	0+54
545	CONV11	TF15	1	1	0	2	1015	2+ 0	1+21
557	AA22	F15	2	2	0	2	1030	2+ 0	1+ 6
647	AA24	F15	1	1	0	2	1120	2+ 0	0+51
650	AA14	TF15	1	1	0	2	1120	2+ 0	0+57
659	CONV14	TF15	1	1	0	2	1130	2+ 0	1+37
730	CONV12	TF15	1	1	0	2	1200	2+ 0	1+25
900	PFLT F	F15	1	2	0	3	1200	6+ 0	12+ 0
900	PFLTTF	TF15	3	2	0	3	1200	6+ 0	12+ 0
929	CONV22	F15	1	1	0	2	1300	2+ 0	1+17
965	CONV24	F15	1	1	0	2	1335	2+ 0	1+21
1010	AA24	F15	3	3	0	2	1440	2+ 0	1+ 4
1030	AA13	TF15	1	1	0	2	1500	2+ 0	1+ 3
1140	AA23	F15	3	2	0	2	1510	2+ 0	1+ 5
1140	AA14	TF15	1	1	0	2	1510	2+ 0	0+52
1100	AA23	F15	2	2	0	2	1530	2+ 0	1+11
1140	AA23	F15	3	3	0	2	1610	2+ 0	0+51
1230	AA23	F15	2	2	0	2	1730	2+ 0	1+ 9
1259	CONV12	TF15	1	1	0	2	1733	2+ 0	1+25
1315	CONV22	F15	2	2	0	2	1745	2+ 0	1+15
1344	AA23	F15	2	1	0	2	1815	2+ 0	1+23
1344	AA13	TF15	2	1	0	2	1815	2+ 0	1+21
1429	CONV12	TF15	1	1	0	2	1900	2+ 0	1+23
1500	CONV24	F15	1	1	0	2	1930	2+ 0	1+20
1644	AA23	F15	2	2	0	2	2115	2+ 0	2+37

APPENDIX C

PERFORMANCE SUMMARY REPORTS AND MATRICES

APPENDIX C

PERFORMANCE SUMMARY REPORTS AND MATRICES

Performance Summary Reports (PSR's) and on/off equipment manpower and backorder matrices are illustrated in this appendix. These statistics reflect the results of the F-15 peacetime simulation based on unconstrained parts, unconstrained avionic test stations, and a .74 scheduled sortie rate. Figures C-1, C-2, and C-3 describe the results of the unconstrained manpower simulation. Figures C-4, C-5, and C-6 contain output statistics for the constrained manpower simulation. Drake (Ref 7 and 8) describes in detail the statistical output of an LCOM simulation.

PERIOD FROM 0000 TO 0000									
SUMMARY									
OPERATIONS									
	TOTAL	CONV	CHRG	ABF	PHASE	WASH	PHASE	WASH	PHASE
1 NUMBER OF REQUESTS	2352.00	1.00	426.00	910.00	350.00	04.00	04.00	50.00	70.00
2 NUMBER OF REQUESTS	22.00	22.00	426.00	910.00	350.00	04.00	04.00	50.00	70.00
3 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
4 NUMBER OF REQUESTS	2352.00	1.00	426.00	910.00	350.00	04.00	04.00	50.00	70.00
5 NUMBER OF REQUESTS	2352.00	1.00	426.00	910.00	350.00	04.00	04.00	50.00	70.00
6 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
TOTAL									
7 NUMBER OF REQUESTS	2352.00	1.00	426.00	910.00	350.00	04.00	04.00	50.00	70.00
8 NUMBER OF REQUESTS	22.00	22.00	426.00	910.00	350.00	04.00	04.00	50.00	70.00
9 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
10 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
11 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
12 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
13 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
14 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
15 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
16 PERCENT REQUESTS	97.00	93.00	98.00	91.00	99.71	100.00	100.00	100.00	100.00
TOTAL									
PERFORMANCE									
17 MANHOURS AVAILABLE	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00
18 MANHOURS AVAILABLE	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00	1278.00
19 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
20 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
21 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
22 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
23 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
24 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
25 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
26 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
27 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
28 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
29 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
30 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
31 PERCENT AVAILABLE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00

Figure C-1. Unconstrained Simulation Performance Summary Report

P E S O N N E L										
	TOTAL	62400	63101	63102	63103	63104	63105	63106	63107	63108
17 MANHOURS AVAILABLE (17)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
18 MANHOURS AVAILABLE (18)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
19 PERCENT UTILIZATION	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
20 MANHOURS USED (20)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
21 PCT OF 24 HRS. AVAILABLE	52.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92
22 PCT OF 24 HRS. AVAILABLE	52.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92
23 NUMBER OF PCT AVAILABLE	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
24 PCT AVAILABLE (24)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
25 PCT AVAILABLE (25)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
26 PCT AVAILABLE (26)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
27 PCT AVAILABLE (27)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
28 PCT AVAILABLE (28)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
29 OVERTIME MANHOURS USED (29)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30 MANHOURS PER FLYING HOUR	4.67	4.67	4.67	4.67	4.67	4.67	4.67	4.67	4.67	4.67
31 MOST TROUBLESPOT DESIG. ITEM	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00

P E S O N N E L										
	TOTAL	62400	63101	63102	63103	63104	63105	63106	63107	63108
17 MANHOURS AVAILABLE (17)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
18 MANHOURS AVAILABLE (18)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
19 PERCENT UTILIZATION	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
20 MANHOURS USED (20)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
21 PCT OF 24 HRS. AVAILABLE	52.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92
22 PCT OF 24 HRS. AVAILABLE	52.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92	27.92
23 NUMBER OF PCT AVAILABLE	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
24 PCT AVAILABLE (24)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
25 PCT AVAILABLE (25)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
26 PCT AVAILABLE (26)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
27 PCT AVAILABLE (27)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
28 PCT AVAILABLE (28)	1270.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00	670.00
29 OVERTIME MANHOURS USED (29)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30 MANHOURS PER FLYING HOUR	4.67	4.67	4.67	4.67	4.67	4.67	4.67	4.67	4.67	4.67
31 MOST TROUBLESPOT DESIG. ITEM	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00

PERFORMANCE SUMMARY

PERFORMANCE SUMMARY

PERFORMANCE SUMMARY

UNIT NUMBER	DESCRIPTION	PERIOD FROM	TO
1	NUMBER OF REQUESTS	100	100
2	NUMBER OF REQUESTS	100	100
3	NUMBER OF REQUESTS	100	100
4	NUMBER OF REQUESTS	100	100
5	NUMBER OF REQUESTS	100	100
6	NUMBER OF REQUESTS	100	100
7	NUMBER OF REQUESTS	100	100
8	NUMBER OF REQUESTS	100	100
9	NUMBER OF REQUESTS	100	100
10	NUMBER OF REQUESTS	100	100
11	NUMBER OF REQUESTS	100	100
12	NUMBER OF REQUESTS	100	100
13	NUMBER OF REQUESTS	100	100
14	NUMBER OF REQUESTS	100	100
15	NUMBER OF REQUESTS	100	100
16	NUMBER OF REQUESTS	100	100
17	NUMBER OF REQUESTS	100	100
18	NUMBER OF REQUESTS	100	100
19	NUMBER OF REQUESTS	100	100
20	NUMBER OF REQUESTS	100	100
21	NUMBER OF REQUESTS	100	100
22	NUMBER OF REQUESTS	100	100
23	NUMBER OF REQUESTS	100	100
24	NUMBER OF REQUESTS	100	100
25	NUMBER OF REQUESTS	100	100
26	NUMBER OF REQUESTS	100	100
27	NUMBER OF REQUESTS	100	100
28	NUMBER OF REQUESTS	100	100
29	NUMBER OF REQUESTS	100	100
30	NUMBER OF REQUESTS	100	100
31	NUMBER OF REQUESTS	100	100

Figure C-4. Constrained Simulation Performance Summary Report

P E F S C M N E L									
MANHOURS AUTHORIZED (11)	4234	43101	43101	43101	43101	43201	46201	46201	46201
17 MANHOURS AVAILABLE (11)	47.4	46.4	47.4	47.4	47.4	47.4	47.4	47.4	47.4
18 PERCENT UTILIZATION	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23
19 MANHOURS USED (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
20 PCT UNASSED. MAINTENANCE	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
21 PCT SCHED. MAINTENANCE	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
22 MINUTES OF MEN DEMAND	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
23 PCT AVAILABLE (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
24 PCT AVAILABLE (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
25 PCT FLOW. BY EXPEDITE	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
26 PCT FLOW. BY PREEMPTION	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
27 PCT DEMANDS NOT SATIS.	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
28 OVERTIME MANHOURS USED (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
29 MANHOURS PER FLYING HOUR	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
30 POST TROUBLESHOOTING PERS. ITEM	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
TOTAL	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23
P E F S C M N E L									
MANHOURS AUTHORIZED (11)	47.4	47.4	47.4	47.4	47.4	47.4	47.4	47.4	47.4
17 MANHOURS AVAILABLE (11)	47.4	47.4	47.4	47.4	47.4	47.4	47.4	47.4	47.4
18 PERCENT UTILIZATION	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23
19 MANHOURS USED (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
20 PCT UNASSED. MAINTENANCE	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
21 PCT SCHED. MAINTENANCE	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
22 MINUTES OF MEN DEMAND	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
23 PCT AVAILABLE (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
24 PCT AVAILABLE (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
25 PCT FLOW. BY EXPEDITE	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
26 PCT FLOW. BY PREEMPTION	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
27 PCT DEMANDS NOT SATIS.	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
28 OVERTIME MANHOURS USED (11)	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
29 MANHOURS PER FLYING HOUR	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
30 POST TROUBLESHOOTING PERS. ITEM	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61	168.61
TOTAL	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23	3517.23

Figure C-4. Constrained Simulation Performance Summary Report (continued)

APPENDIX D

FAILURE CLOCKS

APPENDIX D

FAILURE CLOCKS

This appendix lists the LCOM failure clocks, the respective mean sorties between maintenance action (MSBMA), the decrement tasks, and the decrement values. The MSBMA's are in aircraft sorties unless otherwise specified. DCRMT1, DCRMT2, and DCRMT5 are located in the main flight line networks. DCRMT1 advances the failure clocks prior to a mission launch while DCRMT2 and DCRMT5 advance the clocks after launch. All other decrement tasks are located in the phase and/or corrective maintenance networks.

The cumulative decrement values corresponding to certain failure clocks listed in Table D-I do not equal one. This apparent inconsistency is corrected in respective corrective maintenance network. Tetmeyer (Ref 33) describes in detail the procedures used in designing the corrective maintenance networks and decrementing the corresponding failure clocks.

Table D-I
Failure Clocks

LCOM CLOCK	MSBMA	DECREMENT	
		DCRMT1	DCRMT2
F11A00	18	.02	.98
F11D00	6	.02	.98
F11G00	8	.02	.98
F11K00	20	.02	.98
F11P00	22	.02	.98
F12A00	102	.02	.98
F12B00	125	.02	.98
F12C00	25	.02	.98
F13A00	11	.09	.91
F13B00	26	.09	.91
F13C00	164	.09	.91
F13D00	65	.09	.91
F13F00	178	.09	.91
F13H00	237	.09	.91
F13J00	19	.09	.91
F14AA0	93	.05	.95
F14AB0	711	.05	.95
F14C00	152	.05	.95
F14D00	21	.05	.95
F14E00	67	.05	.95
F14G00	533	.05	.95
F14H00	426	.05	.95
F23000	5	.06	.94
F23100	42	.06	.94
F24A00	44	.14	.86
F24B00	26	.14	.86
F24D00	355	.14	.86
F27000	5	.06	.94
F41A00	20	.05	.95
F42A00	67	.16	.84
F44A00	20	.09	.91
F44B00	267	.09	.91
F44E00	305	.09	.91
F45A00	112	.07	.93
F45B00	133	.07	.93
F45C00	23	.07	.93
F46A00	32	.06	.94
F46B00	355	.06	.94
F46D00	305	.06	.94
F46E00	32	.06	.94
F47A00	63	.10	.90
F49A00	85	.06	.94
F51A00	50		.95
F51E00	51		.95
F51L00	15	.05	
F51M00	426		.95
F51N00	27		.95

Table D-I. Failure Clocks (continued)

LCOM CLOCK	MSBMA	DECREMENT	
		DCRMT1	DCRMT2
F52A00	35	.19	.81
F55A00	237		.99
F55B00	65		.99
F55C00	76		.99
F55L00	420	.01	
F57A00	21		.87
F57L00	70	.13	
F63A00	27		.91
F63B00	25		.91
F63L00	12	.09	
F65A00	142		.98
F65B00	58		.98
F65L00	69	.02	
F71A00	13		.93
F71B00	305		.93
F71C00	533		.93
F71D00	55		.93
F71F00	52		.93
F71L00	8	.07	
F74E00	164		.93
F74F00	4		.93
F74J00	36		.93
F74K00	18		.93
F74L00	6	.07	
F75B00	51		1.00
F75C00	185		1.00
F75D00	152		1.00
F75F00	107		1.00
F75M00	213		1.00
F76A00	18	.11	.89
F76G00	250	.11	.89
F76H00	12		1.00
FCTANK	1333		1.00
FS11PA	590		1.00
FS13HC	1500		1.00
FS14GC	590		1.00
FS2300	33		1.00
FS23HA	89		1.00
FS4700	60	DCRMT3 1.00	
FS7500	30	1.00	

Table D-I. Failure Clocks (continued)

LCOM CLOCK	MSBMA	DECREMENT		
F75H00 FSCGUN FSGUN0	20000 rounds 15000 rounds 25000 rounds	<u>DCRMT5</u> 41.40 rounds 41.40 rounds 41.40 rounds		
FD6000	9	<u>DCRMG2</u> .30	<u>DCRMG3</u> .30	<u>DCRMG7</u> .40
FTTU00	5	<u>DCRMH7</u> .70		
FTSC	65 demands	<u>DCRMTA</u> 1.00 demand		
FTSD	65 demands	<u>DCRMTB</u> 1.00 demand		
FTSM	65 demands	<u>DCRMTC</u> 1.00 demand		
HF	1	<u>DCRMF</u> 1.00		
HTF	1	<u>DCRMTF</u> 1.00		

APPENDIX E

SPARE PART AND AVIONIC TEST STATION CONSTRAINTS

Table E-I. Spare Part Constraints

Work Unit Code	Constrained Quantity	Work Unit Code	Constrained Quantity
13CA0	11	52AB0	7
14AA0	8	52AC0	14
14AB0	1	52AL0	8
23000	37	52AM0	10
24AA0	14	55AC0	3
24B00	31	55AD0	4
51AD0	16	55BC0	5
51AE0	23	55BE0	3
51AF0	11	55CA0	6
51AG0	14	55CB0	33
51AH0	14	57AA0	6
51AK0	18	63AG0	11
51AL0	14	63BC0	14
51AM0	9	63BD0	8
51EA0	4	63BF0	8
51ED0	9	63BH0	7
51NA0	6	65AA0	8
51NB0	10	65BH0	8
52AA0	7	71AE0	14

AD-A156 548 ESTIMATION OF F-15 PEACETIME MAINTENANCE MANPOWER
REQUIREMENTS USING THE (U) AIR FORCE INST OF TECH
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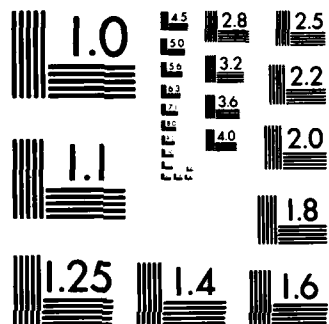


Table E-I. Spare Part Constraints (Continued)

Work Unit Code	Constrained Quantity	Work Unit Code	Constrained Quantity
71AK0	20	74FK0	16
71BD0	6	74FQ0	12
71CA0	7	74FS0	13
71FA0	9	74FU0	11
71FB0	10	74JA0	12
71FC0	11	74JC0	11
71FE0	9	74KA0	7
74EB0	12	74KC0	8
74FA0	14	74KE0	7
74FC0	16	75BB0	5
74FF0	14	75HE0	7
74FH0	16	75MA0	7
74FJ0	14	75MC0	5

Table E-II
Avionic Test Station Constraints

Avionic Test Station	Job Description	Constrained Quality
TSC	Analog/Digital Computer Test Station	2
TSD	Analog/Visual Computer Test Station	2
TSM	Microwave Frequency Test Station	2

VITA

George DeGovanni was born on 4 January 1947 in Philadelphia, Pennsylvania. He graduated from the United States Air Force Academy in June 1968 with a Bachelor of Science in Mathematics. He completed Undergraduate Pilot Training at Moody AFB, Georgia in August 1969. He then flew combat missions in Vietnam as an OV-10 Forward Air Controller attached to the 20th Tactical Air Support Squadron until April 1971. Upon return to the United States, DeGovanni was assigned to the 14th Pilot Training Wing, Columbus Air Force Base, Mississippi, as a T-38 Instructor Pilot/Flight Examiner. In May 1975, he entered the Air Force Institute of Technology.

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VITA

Donald Michael Douglas was born on 23 January, 1943 in Mt. Carmel, Illinois. After graduating from high school there in 1961, he attended the United States Air Force Academy from which he received the degree of Bachelor of Basic Science and a commission in the United States Air Force in 1965. He completed pilot training in September, 1966 and served as a KC-135 pilot with the 301st Air Refueling Wing, Lockbourne Air Force Base, Ohio. After completing rotary wing conversion training in May, 1969, he served with the 809th Combat Support Group, F. E. Warren Air Force Base, Wyoming as a UH-1F pilot. During 1970 and 1971 he flew as a UH-1P and UH-1N gunship flight examiner with the 20th Special Operations Squadron, RVN. He then served as an instructor pilot and Wing Chief of UH-1N Standardization in the 1550th Aircrew Training and Test Wing, Hill Air Force Base, Utah until entering the School of Engineering, Air Force Institute of Technology, in May 1975.

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